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COMPUTATION OF BREAST PTOSIS FROM 3D SCANS OF TORSO

A Thesis Presented to the Faculty of the Department of Electrical and Computer Engineering University of Houston

> In Partial Fulfillment of the Requirements for the Degree Master of Science in Electrical Engineering

> > by Danni Li August 2013

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Acknowledgements

First and foremost, I would like to express my deepest gratitude to my advisor, Dr. Fatima Merchant, for her excellent guidance and continual support during the course of my degree. Working with her was a wonderful experience and her wise knowledge, constructive advice, and constant encouragement that she shared during my stay at the University of Houston has been invaluable. She contributed signicantly to both my research and my professional development. I would also like to thank my thesis committee, Dr. Badrinath Roysam, Dr. Haluk Ogmen, and Dr. Gregory P. Reece, for their encouragement, insightful comments, valuable discussions, and accessibility.

During my graduate studies at the University of Houston, I have had the pleasure of meeting many students, who have helped me directly or indirectly in completing my studies and have made it a rewarding experience. I owe my thanks to them. In particular, I would like to thank my lab mates, Lijuan Zhao, Katrina Chan, and Johnny Andon. I appreciate all the helpful discussions that I had with them. I also thank my close friends, who have become an inseparable part of my life.

I am deeply indebted to my parents and my husband who have been a constant source of support and love throughout this degree and my life. Thank you for everything.

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Abstract

Ptosis is an important morphological parameter for characterizing breast aesthetics and is frequently used for assessing the outcome of breast surgery. It refers to the extent to which the nipple is lower than the terminus of the inframammary fold (the contour along which the inferior part of the breast attaches to the chest wall). Current clinical assessment of ptosis involves qualitative visualization by observers which is subject to inter- and intra-observer variability. Alternatively, ptosis can be measured anthropometrically from the patient or from clinical photographs, but these methods are error prone. As stereophotography is now finding its niche in clinical breast surgery, in this study we investigated and evaluated the utility of three-dimensional (3D) features such as surface curvature, coronal projection and surface normal for the assessment of breast ptosis using 3D scans of the torso. Experimental results suggest that 3D features are successful for objectively categorizing breast ptosis with high accuracy and precision.

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Chapter 1

Introduction

Approximately 232,000 new cases of breast cancer are expected to be diagnosed among women in 2013 according to the National Cancer Institute (NCI) [1]. Presently, advances in screening technology enable the detection of breast cancer at an early stage, when treatment is more effective, and the cure more likely. Breast reconstruction (BR) surgery plays an important role in the breast cancer treatment process. Contemporary goals of breast treatment are not only limited to the cure, but also include maximizing the quality of life. Thus, BR surgery is critical to treatment, as it not only rebuilds the breast tissue that has been removed, but also aims to create a breast that is aesthetically satisfactory to the patient.

Breast aesthetics refer to the physical characteristics of the breast, such as shape, volume, ptosis, and symmetry [2] to name a few. The assessment of the cosmetic result, as an approach to evaluate one of the aspects of treatment quality, has become an essential part of breast cancer treatment. Nowadays, measures characterizing breast aesthetics are determined by (1) qualitative subjective assessment by human observers, (2) direct physical measurements (anthropometry), (3) computer aided measurements on clinical photographs (photogrammetry), and (4) computer aided measurements using three-dimensional (3D) images (stereophotogrammetry).

Subjective assessment of breast aesthetics is highly influenced by the observers' experience and may be biased based on his/her visual perception of breast aesthetics. This assessment is typically based on vaguely defined rating scales that are inherently subjective and qualitative. Substantial studies have reported low intra- and inter- observer agreement and reliability, primarily due to the lack of consistency in the manual perception and interpretation of aesthetic outcomes [3–5].

Anthropometry is a measurement performed directly on the patient's body using a measuring tape. Although it is a useful tool in quantifying the aesthetic outcomes, there are several pragmatic limitations. First of all, it is not only time consuming but also inconvenient for patients, making

it impractical for routine use. More importantly, fundamental parameters such as breast projection is hard to evaluate because of the difficulty in making accurate measurements of curvature on the underlying chest wall, and the mobility of subcutaneous tissues. In addition, it is not feasible to make a large number of measurements on each subject. If a particular measurement does not prove valuable, one cannot retrospectively try a different one. To prove the validity of a specific measurement, studies across multiple institutions with multiple observers are needed, which are costly and labor intensive. Thus, direct anthropometry has limited utility in routine clinical practice and is not generally performed.

Photogrammetry is an alternative allowing indirect anthropometry on two-dimensional (2D) clinical photographs. In photogrammetry, digital images are typically displayed on a computer monitor, or conventional photographs are shown to observers for manually marking measurements. Photogrammetry is relatively more feasible and easy to implement since most medical institutions routinely take photographs for documentation purposes. However, photogrammetry has its drawbacks too. It cannot capture the 3D nature of the human torso. To get a complete view of the torso, a set of multiple photographs with the patient positioned at different angles have to be taken. Furthermore, accurate anatomic landmarks that are critical to obtaining reproducible assessment of aesthetic outcomes by photogrammetry may not be visible from 2D photographs, due to the lack of consistent guidelines for standard photography [6,7].

To address limitations of photogrammetry, stereophotogrammetry, which involves measurements on 3D scans of torso, is being evaluated as an alternative method to assess breast aesthetics. 3D digital photography systems are capable of non-invasively generating precise images at high speeds. A single 3D image yields more information on breast appearance than multiple conventional 2D photographs. One 3D scan of the torso can be viewed from several different angles, which is impossible in 2D photogrammetry. They also enable objective determination of properties such as contour distance, surface area, volume, and surface curvature, which are not available from 2D images [8–10]. Thus, 3D imaging has tremendous potential for analysis of breast appearance.

Features	2D Photograph3D Photograph	
Distance	Only straight-line distances can be measured from 2D pho- tographs.	Contour/geodesic distances that follow the surface contour can be measured.
Area	Available with limited precision.	Can be accurately measured from a 3D torso image.
Volume	Can only be indirectly approxi- mated with limited precision.	Can be accurately measured from a 3D torso image.
Surface curvature	2D radius of curvature measure- ments feasible.	3D surface curvature measure- ments available.
Surface normal	Planar surface normal measure- ments feasible.	3D surface normal available.

Table 1.1: A preliminary comparison of measurements feasible for 2D and 3D photographs.

Ptosis is a measurement used for characterizing breast morphology that estimates the amount of sagging or drooping of the breast. It refers to the extent by which the nipple is lower than the inframammary fold (IMF), i.e., the lower breast contour along which the inferior part of the breast attaches to the chest wall. Regnault [11] was the first to classify ptosis into a four-grade scale based on qualitative criteria. Later, LaTrenta and Hoffman [12] added a quantitative strategy for measuring different grades. LaTrenta and Hoffman's classification facilitates objective analysis based on distance measurements on the patient. Kim *et al.* [13] proposed a quantitative and objective measurement of breast ptosis on 2D lateral and oblique views of clinical photographs.

Previous studies on breast ptosis measurements were all based either on subjective ratings, direct anthropometry or 2D photogrammetry. As discussed above, the intrinsic properties of a 2D image limits our ability to quantify 3D features, thereby affecting the analysis that can be performed. A simple comparison of the features available from 2D photographs with those from 3D stereophotographs is shown in Table 1.1, from which it is apparent that 3D stereophotogrammetry offers more features that can be potentially explored for quantitative assessment.

However, simply employing the techniques widely used on 2D ptosis assessment (e.g., based on vertical distance measurement) onto 3D images is suboptimal and many important features of 3D images will be under utilized. One important issue in measuring breast ptosis is that traditional ptosis ratings involves identification of fiducial points (such as the nipple and the terminus of the inframammary fold) on patients during anthropometry, or on photographs during 2D photogrammetry. However, the terminus of inframammary fold is often difficult to identify because it is vaguely defined and hard to distinguish [14]. Thus, an approach of measuring ptosis that excludes the identification of the terminus of the inframammary fold would provide robust performance and accurate results.

In this thesis, we explored features that can be computed from 3D images for measuring breast ptosis without predefining the terminus of inframammary fold. To achieve this, we first investigated Gaussian surface curvature, coronal projection and surface normal and generated template histograms for each feature. Second, we conducted leave-one-out cross-validation (LOOCV) on our data set to test the performance of each feature for classification. We evaluated the following 3D features, (1) Gaussian curvature of the surface mesh, (2) distribution of 3D points along coronal planes, (3) the Y component of the surface normal and, (4) all the combinations of these three features. Test results were compared to the ground truth (assessment of breast ptosis by an experienced surgeon). Our results show that the singular use of each of the three features, Gaussian surface curvature, coronal projection, and the Y component of the surface normal have an overall accuracy of 73%, 72%, and 77%, respectively. Whereas the combination of the three features has an overall accuracy of 78%.

This thesis is organized as follows: Chapter 2 presents background material on 3D surface imaging and existing commercial systems for the same. It also includes a brief description of the 3D Torso Image Database housing the images used in our study. In Chapter 3, related work on current assessment of breast aesthetics and breast ptosis is discussed. In Chapter 4, an algorithm for measuring ptosis using 3D features is described, and Chapter 5 presents the experimental results and discussion. Conclusion and some ideas for future work are presented in Chapter 6.

Chapter 2

Background

2.1 Image Acquisition

3D image acquisition systems are popular for clinical use since they provide minimal invasiveness, high capture speeds, good accuracy, and safety. 3D imaging provides accurate geometrical information on the human torso in conjunction with a 2D texture map overlaid on the surface for realistic rendering. Typically, data from 3D imaging systems consists of a point cloud from sampling the surface of the torso as shown in Figure 2.1. Each point has a x, y, and z position corresponding to the position in space obtained from a triangulation method, applied to images from multiple cameras with known geometries.



Figure 2.1: (a) Point cloud of 3D surface scan. (b) Triangular surface mesh. (c) 2D texture mapped onto the 3D triangular surface mesh.

2.2 Image Database

We have a database of 3D torso scans of patients, maintained by the Biomedical Informatics Laboratory (BMIL) at the University of Texas at Austin, TX. Each 3D image was captured at the University of Texas M. D. Anderson Cancer Center (MDACC), Houston, TX. The database of images and related demographic information about each subject is hosted and managed by BMIL, and is accessible via a user-friendly web interface for data browsing, query and download. The number of images in the database is increasing as patients are enrolling into this study, and previously enrolled patients return for follow-up visits as the process of breast reconstruction procedure is implemented. An earlier model of the 3dMD imaging system, namely the DSP800; was used to capture the images of the first 40 patients, whereas the rest were acquired using the 3dMD Torso system (3dMD LLC, Atlanta, GA). The spatial resolution of scans from the DSP 800 is low (\sim 15,000) when compared to that of the 3dMDTorso system (\sim 75,000). The new system has improved geometrical accuracy and resolution.

2.3 Visualization Software

2.3.1 Commercial Software

Some of the popular commercial systems designed for plastic surgeons are Sulptor $3D^{TM}$ from Canfield Clinical Systems (Fairfield, NJ), 3dMD Breast AnalysisTM and 3dMDVultus TM from 3dMD, LCC. (Atlanta, GA), and 3D SurgeonTM from Genex Technologies Inc. (Kensington, MD). Most of these software packages enable a variety of surface path, angle, area and volume measurements.

2.3.2 University of Houston 3D Visualization Tool

Visualization is significant for image analysis, especially for quantitative analysis of 3D images, such as measurement of symmetry, ptosis, volume, etc. Various existing tools have been developed to perform different measurements. However, it is always beneficial to have a customized system according to our requirements and data. So we have developed a 3D visualization software for rendering, manipulation, alignment and analysis of 3D torso images. Our visualization tool i.e., BR software is shown in Figure 2.2.

The analysis modules allow computation of both distance (Euclidean and geodesic) and volume measurements. Currently the software supports the following features:



Figure 2.2: Screenshot of UH visualization tool.

- 3D image visualization and manipulation,
- Surface path measurements,
- Volume measurement,
- Curvature measurement,
- Recording and reporting of results,
- Connection to BMIL database of 3D Torso Images,
- 2D measurements.

The software was developed using Java, including JFC/Swing Application Program Interface (API) for dialogues, menus, and other basic user interface components. We have used XML configuration files for registration of functional code modules, which can be dynamically loaded by custom class loaders, yielding a very flexible plug-in capability. For 3D visualization we have used the Java 3D API, whereas the image representation and processing functionality is developed using the Java Advanced Imaging (JAI) API. Java 3D is a hierarchy of classes that serve as the interface to

a sophisticated 3D graphics and sound-rendering system. It provides high-level constructs to create and manipulate 3D geometry, and to build the structure used to render that geometry.

Chapter 3

Related Work

In this chapter, relevant techniques for assessing breast aesthetics, especially for ptosis classification and measurement are discussed. We start with the description of a normal breast, and then define ptosis, its classification, and existing techniques for measuring ptosis. Two approaches are currently used for measuring ptosis: subjective and objective methods. We discuss both advantages and limitations of various approaches, with a focus on evaluation using two-dimensional (2D) versus three-dimensional (3D) data.

3.1 Normal Breast

Normally, the human breast is located between the second intercostal space and the sixth rib. In the primary or non-augmented breast, the ideal aesthetic nipple lies above the inframammary fold (IMF) and is located at the center of the breast gland in young females [11]. The IMF is defined as the natural boundary of the breast from below, i.e., the place where the breast and the chest meet. IMF is an important aesthetic landmark of the female breast, and plays an essential role in breast surgery, such as in ptosis classification [15–17].

When the volume of the breast is small and well supported by the skin envelope, no IMF is formed. As the breast volume increases and the breast is not supported well, the IMF can be visualized as the lower boundary of the breast, along the intersection of the breast with the chest wall. Normally, the nipple, skin, and breast gland follow the influence of gravity together. The distance of nipple to the IMF increases very little while the distance of the nipple to the clavicle elongates more.

3.2 Importance of Ptosis for Breast Reconstruction

Contemporary goals of surgery during breast cancer treatment are not only limited to cure, but also include restoration of breast aesthetics, to help patients improve body image and quality of life. Although current literature shows that the breast cancer survival is becoming more and more common, the aesthetic results of breast cancer treatment are poor in up to 15% of the cases [18]. Consequently, objective measurements of breast morphology are important for both surgeons and patients in setting up appropriate plans for pre-treatment and for evaluation of post-treatment outcomes.

Grewal *et al.* [19] followed up to a total number of 134 patients who underwent revisionary breast surgery in a 15-year period from 1994 to 2009. Their results suggest that ptosis is the most frequent reason (40% of the patients) for patients seeking revisionary surgery. Webster [20] also studied the relationship between patients' ptosis and their satisfactions after immediate partial breast reconstruction with local flaps and symmetrization of the contralateral breast. Strong correlations indicated that satisfaction was observed in patients with higher degree of ptosis who may better benefit from the combined techniques of immediate reconstruction and contralateral mammaplasty.

Ptosis plays an important role for surgeons evaluating breast surgical outcomes [3, 21, 22]. Bajaj *et al.* [23] used ptosis as a metric to facilitate the assessment of breast aesthetic changes during breast conservation therapy. Hauben [24] reported the relationship between breast ptosis, volume and size using the value of breast-areola-nipple proportion. Such analysis is important to plastic surgeons in planning breast reduction, augmentation, and reconstruction.

Ptosis is also an important factor in planning strategies of breast reconstruction surgery. Roehl *et al.* [25] showed that patients with different levels of ptosis require distinct strategies of breast reconstruction. For instance, youthful patients with round-shaped breast (without ptosis or with minor ptosis) may benefit from implant-based reconstructions, while breast rearrangement is usually ideal for large-breasted women with significant breast ptosis and/or asymmetry.

3.3 Classification of Breast Ptosis

Ptosis is a characteristic of breast morphology, which is routinely used to assess surgical outcomes in a variety of breast surgeries. It provides a measure for understanding patient requirements, informing consultants, and training future surgeons. Plastic surgeons use a classification system to categorize the degree of breast sagging, or ptosis. This classification system also helps surgeons determine what treatment option is the best for an individual based on the level of her breast ptosis.

A variety of classifications exist for ptosis, including Regnault (1976) [11], Lewis (1983) [26], Brink (1990) [27] and (1993) [28], LaTrenta and Hoffman (1994) [12], Kirwan (2002) [29], and de la Torre and Vasconez (2007) [30]. The classification of ptosis helps determine the type of surgery for mastopexy. The determination of whether to augment a breast, perform mastopexy, or to do a combination of both involves the physician discussing the pros and cons of each procedure with the patient and deciding on the most feasible procedure [31].

3.3.1 Regnault's Classification

Ptosis is usually classified according to the relative position of the nipple with respect to the IMF. Abnormal ptosis is identified when the nipple and inferior pole of the breast descend lower than the level of the terminus of the IMF [2]. Regnault [11] subjectively classified the ptosis grades, as shown in Figure 3.1.

- **Grade 0** (**Normal breast**): A normal breast has the nipple and parenchyma (glandular tissue and fat which compose the breast) sitting above the crease or the terminus of IMF.
- Grade 1 (Minor ptosis): In first grade ptosis, the nipple lies at the level of the terminus of IMF and above the lowest contour of the breast.
- Grade 2 (Moderate ptosis): In grade two ptosis, the breast exhibits sagging in which the nipple lies below the level of the terminus of IMF but remains above the lowest contour of the breast.



Figure 3.1: Regnault's classification of ptosis.

• Grade 3 (Major ptosis): In grade three ptosis, the breast exhibits severe sagging in which the nipple lies well below the terminus of IMF and lies at the inferior contour of the breast.

In addition, Regnault also defined "Pseudoptosis" which is not true ptosis, or sagging, because the nipple lies above or at the level of the terminus of IMF. However, the majority of the breast parenchyma has descended below the level of the fold. Another condition is described as parenchymal maldistribution. The lower portion of the breast lacks fullness, and a higher terminus of the IMF is observed with a relatively short distance from the fold to the nipple. This is seen in conditions such as a tuberous breast. Pseudoptosis and parenchymal maldistribution are rare conditions and most clinical assessment systems typically only utilize the four-grade scale of ptosis (0-3).

3.3.2 Lewis's Classification

Lewis's [26] classification of breast ptosis is typically used for surgical classification as related to a pathological condition. It is defined as follows.

- Mildly ptotic breasts of adequate size, without hypertrophy.
- Mildly ptotic breast with atrophy.
- Mild to moderate ptosis with mild to moderate hypertrophy.

- Markedly ptotic breast with marked hypertrophy.
- Moderate or markedly ptotic breasts with adequate total breast bulk.
- Moderate or markedly ptotic breasts with inadequate total breast bulk.
- Mildly or moderately ptotic breasts with chronic cystic mastopathy.
- Breasts with marked ptosis or marked hypertrophy with cystic mastopathy.
- Asymmetry of the breasts (of significant degree).

3.3.3 Brink's Classification

Brink [27] classified ptosis similar to Regnault's classification as follows.

- **True ptosis**: The nipple-areola complex's relation to the IMF when the gland, skin, and nipple descend.
- **First-degree** (**minor**) **ptosis**: Nipple-areola complex at the IMF and above the breast contour (gland behind the nipple-areola complex).
- Second-degree (moderate) ptosis: Nipple-areola complex below the IMF but above the breast contour (gland behind the nipple-areola complex).
- **Third-degree** (**major**) **ptosis**: Nipple-areola complex below the IMF and below the breast contour (gland above the nipple-areola complex).

3.3.4 LaTrenta and Hoffman's Classification

In 1994, LaTrenta and Hoffman [12] presented a quantitative measurement on the vertical distance from the nipple to the terminus of IMF based on Regnault's classification. They quantified the classification using distance in centimeter metrics as follows.

• First degree or minor ptosis: nipple position lies within 1 cm of the level of the terminus of IMF.



Figure 3.2: Kirwan's classification of ptosis from stage A to stage F.

- Second degree or moderate ptosis: nipple position lies 1-3 cm below the terminus of IMF.
- Third degree or severe ptosis: nipple position lies greater than 3 cm below the level of terminus of IMF and below the lower contour of the breast and skin envelope.
- **Pseudoptosis**: nipple position lies at or above the level of terminus of IMF with a loose "saggy" skin envelope, giving the impression of true ptosis.

3.3.5 Kirwan's Classification

Since the Regnault's classification is qualitative and subjective, it is ineffective for planning surgical strategies for different stages of ptosis. Kirwan [29] proposed a quantitative measurement based on the Regnault's classification. In a new system, 6 stages of breast ptosis covering a 5 cm distance are defined. Stages A to E progress in 1 cm increments as follows (Figure 3.2):

- Stage A: nipple position 2 cm above the IMF,
- Stage B: nipple position 1 cm above the IMF,
- Stage C: nipple position even with IMF,
- Stage D: nipple position 1 cm below the IMF,
- Stage E: nipple position 2 cm below the IMF.
- Stage F: nipple position greater than 2 cm below the IMF.

3.4 Subjective Assessment of Ptosis

Currently, subjective ptosis assessments are performed mainly via either patients self-evaluation, or by a single observer or a panel composed of observers and physicians based on printed photographs, digital images, or directly viewing patients [3,4,32,33].

Although subjective ptosis assessment is still the most frequently used approach [34–36], it has been criticized for many limitations. First of all, the results are highly influenced by the observers' experience and may be biased based on his/her visual perception of breast aesthetics. Thus this approach has suffered from low reproducibility and variable internal and external consistency. For instance, Sneeuw *et al.* [5] reported higher intra-rater agreement between the nurse and the oncologist ($\kappa = 0.64$) but lower agreements between ratings by patients' and clinical observers' ratings ($\kappa < 0.10$) using the global 4-point scale. Sub-scales of the 4-point scale showed low to moderate reliability ($\kappa = 0.24 - 0.40$). In addition, Pezner *et al.* [3] also reported that experienced observers had higher agreements than novice observers. The scales showed low reliability ($\kappa = 0.31$). Consequently, data averaged from a panel rather than individual evaluator is often employed, but this approach is time and labor intensive. Oliveira *et al.* [37] reported this process can take months or even years when performed in a large number of patients with multiple observers.

Another major limitation of subjective ptosis assessment is that the lack of a standardized, explicit scale for analyzing cosmetic outcome also amortizes the precision of the process. A crude ordinal scale with four or five categories is imprecise for identifying individual aesthetic elements.

3.5 Objective Measurements of Ptosis

3.5.1 Anthropometry

As discussed before, anthropometry involves measurements made directly on the patient's body using a measuring tape. Penn's approach of defining nipple-to-sternal notch and mid-clavicle point distances based on 20 women with "aesthetically perfect" breasts has gained broad attention and has been adopted as normative [38]. Similarly, the distances between fiducial points were computed in 66 women in whom one-third had either breast hypertrophy, ptosis, or both [39]. Another study measured the symmetry of 40 patients by computing differences between the right and left breast and investigated the relationship between subjective rating and linear measurements [40]. A study of anthropometric breast measurement on 385 Turkish female students was also reported in [41].

"Aesthetically perfect breasts" was defined as a breast shape for which no aesthetic procedure would be indicated. The problem with this definition is that different surgeons have different notions when an aesthetic procedure is indicated. For example, in general, European Plastic Surgeons feel that what American Plastic Surgeons consider to be the "ideal breast" is really too large and they would recommend a breast reduction [42]. Typically, the outcomes of anthropometry analysis are highly correlated with other metrics of breasts. For instance, 22 linear measurements were designed and compared to the results of Penn [38] and Smith [39]. Nine of the measures were shown to have statistically significant correlation with breast volume [43]. Another study [24] computed the distances between the nipple and the border of the breast to calculate the nipple-areola-breast proportion and showed correlation of patient characteristics and breast proportions. Significant positive linear correlation between age and areola-breast proportion was reported and areola-nipple proportion was shown to be significantly larger in higher ptosis grades.

Furthermore, direct anthropometry is not only time consuming but inconvenient for patients, making it impractical for routine use. To prove the validity of a specific measurement, studies across multiple observers are needed, which are too costly. Also, the relationships between outcomes of anthropometry and subjective scales are unclear [44, 45]. For these reasons, anthropometry has limited utility in routine clinical practice.

3.5.2 2D Photogrammetry

Instead of direct measurement on a patient, 2D photogrammetry, wherein measures are made on a photograph (printed or digital), has shown great potential for quantifying breast ptosis. Photogrammetry is relatively more feasible and easy to implement since most medical institutions routinely take photographs for documentation purpose. In addition, it is also possible to make several measurements on the same photograph. Pezner *et al.* [3] reported an evaluation of a series of frontal views from 14 patients performed by 44 observers that challenged the value of subjective evaluations in terms of reproducibility. Prints produced from digital images, digital images displayed on a computer monitor, or conventional photographs are acceptable to observers for subjective assessment of breast aesthetics [46]. Furthermore, instead of obtaining subjective ratings based on photographs, several studies proposed objective measurements calculated on 2D photographs [13, 21, 47]. This approach has yielded encouraging results, but there are limitations to the reported studies.

Kim *et al.* [13] proposed an objective, quantitative measurement of breast ptosis based on the ratio of distances between fiducial points, such as nipple point, sternal notch, lateral terminus, and lowest visible point, manually identified in digitized/digital images of oblique and lateral clinical photographs (pre-operative). However, the automatic identification of fiducial points can be challenging to locate and manual interventions must be involved. Furthermore, outcomes of distance ratios which scale from 0 to 1 need to be accurately mapped on to the 4-point scale by Regnault to allow for easier interpretation of the outcome. The paper employed a simple linear regression approach to transform the distance ratios to subjective scales, based on two clinical groups of 52 patients and 10 patients, respectively. However, the distribution of the measurements in either group did not illustrate strong linear relationships between the 4-point Regnault's scale.

Lee *et al.* [48] proposed a novel quantitative measure of breast curvature based on catenary analysis. They compared the length, the area enclosed by the curve, and the curvature measure from the catenary curve to those from manual tracings of the breast contour. Likewise, the same procedure was applied to frontal photographs. This can be related with the difficulty of extracting robust features from lateral views. Studies [49] also showed that lateral and oblique views are difficult to standardize and the solution will be to move into 3D stereophotogrammetry. In our work, we employed curvature analysis to 3D photographs. since curvature is an intrinsic feature in 3D scans and is easy to extract and measure. Furthermore, another limitation of 2D photogrammetry is that some anatomic landmarks may not be visible from the 2D photographs and the measurements cannot be obtained following the contours of the patient's body. To address this issue, clinical photographs of patients undergoing breast reconstruction are usually taken from five different views: anterior-posterior, right and left lateral, and right and left oblique views. An anteriorposterior (AP) view includes clavicles and shoulders above, publis below, arms at side. An oblique view is taken with the patient turned 45 degree and with the distal arm back slightly. Lateral views are taken directly from the side such that only the proximal breast is visible [13]. Although there are lots of efforts on standardizing the procedure of the clinical photography [50–53], some studies continue to report substantial deviation for measurements on photographs, mainly due to the lack of consistency in the manual identification of anatomic landmarks [54]. Consistent guidelines for standard photography are critical to obtaining reproducible assessment of aesthetic outcomes by 2D photogrammetry.

3.5.3 3D Stereophotogrammetry

Compared with 2D photogrammetry, the advantage of 3D stereophotogrammetry is the ability to view the breast from a significant different number of angles in one photograph. Moreover, 3D images contain the geometric properties of the underlying surface, which enable objective quantitative measurements. Images obtained from 3D stereophotogrammetry techniques have more features such as surface area, volume and curvature, etc., which yield more information than traditional 2D photographs.

For breast surgery, 3D stereophotogrammetry is now being widely used in evaluation of differences in volume, surface area, shape, size, contour and symmetry [55–57]. Galdino *et al.* [57] investigated the use of clinical 3D imaging to determine quantitative information about the breast, such as volume or projection. They applied this approach to real cases, providing objective data on breast and surgical mammaplasty (especially augmentation mammaplasty). This helped surgeons better understand the factors that contribute to breast shape and influence surgical outcomes. A couple of limitations were also found, highlighted by patients with significant ptosis or suffering from obesity, which may introduce errors into the 3D data, making them unreliable.

Tepper *et al.* [58] used 3D images to enable an objective volumetric analysis of breasts prior to breast reconstruction. Surgeons are then capable of visualizing the size, shape, contour and symmetry of the breast with 3D breast models, as well as obtaining quantitative breast measurements and performing volumetric calculations. This application represents a significant advance from traditional approaches to aesthetic and reconstructive breast surgery.

Although 3D imaging has tremendous potentials for analysis of breast appearance, it does have limitations. High cost and the difficulty in using these methods on a daily basis prevents their widespread use. Additionally, it involves the long acquisition time needed to obtain the 3D model, which can result in time delay for the patient. During the period of acquisition any movement made by the patient can result in unreliable 3D models. Another important issue is related with automation of the existing commercial 3D software. Several features are still difficult to automatically identify thus manual interventions are needed. People still expect to have completely automated software with low cost, easily operated hardware and the public databases with which results can be compared.

Nevertheless, 3D stereophotogrammetry is evolving rapidly and may offer the most accurate way to quantify numerous elements of breast appearance and evaluate changes over time [59]. Further development of this technology might yield a variety of useful clinical tools to aid surgical planning, patient decision making, and outcomes analysis [60].
Chapter 4

Methodology

In this study, we first cropped the torso image into a single breast area as the region of interest (ROI), and then partitioned each breast into four quadrants according to the nipple position. We investigated a variety of 3D features and tested their feasibility for distinguishing the four-scale ptosis grades. 3D features including Gaussian surface curvature, distribution of points along coronal projection planes, and surface normal were evaluated and are discussed in detail in this chapter. We generated a histogram for each quadrant, and built template histograms for all the four grades for each feature to analyze their feasibility for classification. Finally, the Bhattacharyya distance for histogram matching was used to categorize the ptosis grade, followed by statistical measurements for analyzing the performance of the algorithm. Figure 4.1 shows the flowchart outlining the methods used to assess breast ptosis from 3D surface scans.

4.1 Image Cropping

As a first step, the torso data was cropped to remove the neck, arms, legs and belly, leaving only the upper portion of the torso encompassing the breast region as the ROI. The breast region was defined to enclose the whole breast area, as shown in Figure 4.2, with the height from sternal notch, which has the same level with mid-clavicle point, down to the lowest visible point of the breast. Horizontally, each breast was cropped individually from the mid-point of torso to the lateral point. The reason for cropping the torso image into individual breast regions is that the ptosis grade was determined individually for each breast, since a patient may either have asymmetric breasts, i.e., the two breasts may have different ptosis grades, or only one breast mount is intact due to whole or partial mastectomy.

Furthermore, each breast was divided into four quadrants with the nipple at the origin to capture any spatial morphological differences across four grades. The four quadrants were named



Figure 4.1: Flowchart of algorithm used to assess ptosis from 3D surface scans.

as *a*, *b*, *c*, and *d* clockwise as follows: the upper left quadrant *a*, the upper right quadrant *b*, the lower right quadrant *c*, and the lower left quadrant *d*. As ptosis grade increases, the nipple moves downward, and the shape of the breast within each quadrant as well as the distribution of points in each quadrant changes across the four grades.

4.2 Curvature Analysis

One major advantage of stereophotogrammetry is that it can represent the natural 3D morphology of the torso. Surface curvature measures how fast a curve is changing in direction for a given vertex in 3D space. Surface curvature analysis can be used to highlight the shape of the underlying 3D surface, thus it plays an important role in ptosis classification. We used a toolbox developed by Gabriel Peyre [61] based on the algorithms proposed by Cohen-Steiner et al. [62, 63]



Figure 4.2: A sample image with the neck and arms cropped, extending from the sternal notch to just below the IMF. (a) Cropped image with both breasts (b) Cropped image for right breast (c) Cropped image for left breast.

to calculate surface curvature, which can be calculated as

$$T(v) = \frac{1}{|B|} \sum_{edges \ e} \beta(e) |e \cap B| \bar{e} \bar{e}^t, \tag{4.1}$$

where v is an arbitrary vertex on the mesh, |B| is the surface area around v over which the tensor is estimated, $\beta(e)$ is the signed angle between the normals to the two oriented triangles incident to edge e (positive if convex, negative if concave), $|e \cap B|$ is the length of e within B (always between 0 and |e|), and \bar{e} is a unit vector in the same direction as e in Figure 4.3. The tensor is evaluated at every vertex location v, for a neighborhood B that approximates a geodesic disk around this vertex. The two principal eigenvalues, k_{min} and k_{max} calculated for this tensor vector, are the estimates of principal curvatures at v.

Generally curvature values are very small, and it is hard to visualize subtle differences in curvature. Thus, for visualization, we extend the range to enable a better partitioning of region depending on similar curvature values. In our curvature mapping, we linearly mapped the curvature value onto a color map.

In addition to principle curvatures $(k_{min} \text{ and } k_{max})$, Gaussian (K) curvature can be computed



Figure 4.3: Estimation of curvature tensor.

by

$$K = k_{min} \cdot k_{max}.\tag{4.2}$$

The regions with K>0 are 'elliptic', while those with K<0 are 'hyperbolic', and those with K=0 are either 'planar' or 'cylindrical'.

We partitioned each breast into four quadrants according to the nipple position as shown in Figure 4.4. Quadrants were named a, b, c, and d in the clockwise direction. The premise for using curvature analysis is that as the ptosis grade increases, the advanced drooping of the breast is reflected in the shape and consequently the curvature value of the surface. Differences in the curvature value are visually apparent on the superior and inferior parts of the breast, thus in this study our aim was to evaluate the feasibility of using curvature as a feature for distinguishing between different ptosis grades.

An ideal breast without ptosis is relatively symmetrical across the superior and inferior parts, whereas sagging of the breast gland with increasing ptosis results in a non-symmetric breast shape and consequent asymmetry in curvature is observed across the superior and inferior parts. When the ptosis grade increases, the underlying gland droops, leading to a larger area that is flatter (low curvature values) being observed within the regions of quadrant *a* and *b*. This indicates an increase in the number of points around curvature value equal to zero within these quadrants.

For inferior quadrants c and d, a reversal in the curvature value is observed. When the ptosis grade increases, the area of the lower two quadrants become smaller, and larger curvature values are



Figure 4.4: Breast divided into four quadrants: *a*, *b*, *c* and *d*.

apparent in the region below the IMF. Typically, a large portion of breast exhibits a convex shape, in other words positive curvature values, especially in the nipple-areola area, whereas below the IMF, the concave shape of the crease introduces negative curvature values. Thus over the inferior pole of the breast a smaller number of points with lower curvature values are observed. Figure 4.5 shows an example curvature map for both left and right breasts.



Figure 4.5: Gaussian curvature plot of the breasts exhibited in Figure 4.2.

In order to evaluate the feasibility of Gaussian curvature as a feature for classification, we generated histograms to visualize the distribution of curvature values in each of the 4 quadrants. Since the curvature values are very small and greater than 95% of the values are located within the range $[-6 \times 10^{-4}, 6 \times 10^{4}]$, we divided the range into 40 bins, with each bin holding a range of

 1.5×10^{-5} , except that the first bin and the last bin are holding Gaussian curvatures smaller than -6×10^{-4} and greater than 6×10^{-4} , respectively. In order to standardize the size of the breast, the total number of points in each bin was normalized with respect to the total number of points in the ROI. Histograms of four quadrants were generated and concatenated in the order of *a*, *b*, *c*, and *d*. Finally, a histogram template for every grade was generated by taking the average of the histograms for all breasts within the specific grade, as shown in Figure 4.6 and Figure 4.7.

Figure 4.6 and Figure 4.7 shows the Gaussian curvature histogram templates for grade 0, 1, 2, and 3, respectively. Quadrant a, b, c, and d cover bins 1 - 40, 41 - 80, 81 - 120, and 121 - 160, respectively as shown in Table 4.1. Compared with grade 0 and grade 1, it is clear that the number of points acquired around curvature value zero (bin 19-20 and 69-70) are larger, indicating a flatter area. For quadrants c and d, the higher ptosis grade includes more low curvature values because of the drooping of the breast.



Figure 4.6: Histogram templates of concatenated Gaussian curvature histograms including each of the four quadrants (a-d) for Grade 0 and Grade 1.



Figure 4.7: Histogram templates of concatenated Gaussian curvature histograms including each of the four quadrants (a-d) for Grade 2 and Grade 3.

Quadrant a	Quadrant b	Quadrant c	Quadrant d	Range of Values
1	41	81	121	$(-inf - 5.7 \times 10^4)$
2	42	82	122	$\left[-5.7 \times 10^{-4}, -5.4 \times 10^{4}\right)$
3	43	83	123	$\left[-5.4 \times 10^{-4}, -5.1 \times 10^{4}\right)$
4	44	84	124	$\left[-5.1 \times 10^{-4}, -4.8 \times 10^{4}\right)$
5	45	85	125	$\left[-4.8 \times 10^{-4}, -4.5 \times 10^{4}\right)$
6	46	86	126	$-4.5 \times 10^{-4}, -4.2 \times 10^{4})$
7	47	87	127	$\left[-4.2 \times 10^{-4}, -3.9 \times 10^{4}\right)$
8	48	88	128	$-3.9 \times 10^{-4}, -3.6 \times 10^{4})$
9	49	89	129	$\left[-3.6 \times 10^{-4}, -3.3 \times 10^{4}\right)$
10	50	90	130	$\left[-3.3 \times 10^{-4}, -3 \times 10^{4}\right)$
11	51	91	131	$\left[-3 \times 10^{-4}, -2.7 \times 10^{4}\right)$
12	52	92	132	$\left[-2.7 \times 10^{-4}, -2.4 \times 10^{4}\right)$
13	53	93	133	$\left[-2.4 \times 10^{-4}, -2.1 \times 10^{4}\right)$
14	54	94	134	$\left[-2.1 \times 10^{-4}, -1.8 \times 10^{4}\right)$
15	55	95	135	$\left[-1.8 \times 10^{-4}, -1.5 \times 10^{4}\right)$
16	56	96	136	$\left[-1.5 \times 10^{-4}, -1.2 \times 10^{4}\right)$
17	57	97	137	$\left[-1.2 \times 10^{-4}, -0.9 \times 10^{4}\right)$
18	58	98	138	$\left[-0.9 \times 10^{-4}, -0.6 \times 10^{4}\right)$
19	59	99	139	$\left[-0.6 \times 10^{-4}, -0.3 \times 10^{4}\right)$
20	60	100	140	$\left[-0.3 \times 10^{-4}, 0\right)$
21	61	101	141	$[0, 0.3 \times 10^4)$
22	62	102	142	$\left[0.3 \times 10^{-4}, 0.6 \times 10^{4}\right)$
23	63	103	143	$\left[0.6 imes 10^{-4}, 0.9 imes 10^{4} ight)$
24	64	104	144	$\left[0.9 \times 10^{-4}, 1.2 \times 10^{4} ight)$
25	65	105	145	$\left[1.2 \times 10^{-4}, 1.5 \times 10^{4}\right)$
26	66	106	146	$\left[1.5 \times 10^{-4}, 1.8 \times 10^{4}\right)$
27	67	107	147	$\left[1.8 \times 10^{-4}, 2.1 \times 10^{4}\right)$
28	68	108	148	$\left[2.1 \times 10^{-4}, 2.4 \times 10^{4}\right)$
29	69	109	149	$\left[2.4 \times 10^{-4}, 2.7 \times 10^{4}\right)$
30	70	110	150	$\left[2.7 \times 10^{-4}, 3 \times 10^{4}\right)$
31	71	111	151	$(3 \times 10^{-4}, 3.3 \times 10^{4})$
32	72	112	152	$(3.3 \times 10^{-4}, 3.6 \times 10^4)$
33	73	113	153	$(3.6 \times 10^{-4}, 3.9 \times 10^{4})$
34	74	114	154	$(3.9 \times 10^{-4}, 4.2 \times 10^{4})$
35	75	115	155	$(4.2 \times 10^{-4}, 4.5 \times 10^{4})$
36	76	116	156	$(4.5 \times 10^{-4}, 4.8 \times 10^{4})$
37	77	117	157	$(4.8 \times 10^{-4}, 5.1 \times 10^{4})$
38	78	118	158	$(5.1 \times 10^{-4}, 5.4 \times 10^{4})$
39	79	119	159	$(5.4 \times 10^{-4}, 5.7 \times 10^{4})$
40	80	120	160	$\left\lfloor 5.7 \times 10^{-4}, inf \right)$

Table 4.1: The relationship between quadrants, bins, and the range of values for each bin for Gaussian curvature.

4.3 Coronal Projection Analysis

Coronal projection analysis is another feature which was evaluated in order to incorporate the effect of breast shape on ptosis grade. A coronal plane is a vertical plane that divides the breast into front and back sections. Coronal projection analysis includes the computation of the total number of points located on the surface mesh, between every two subsequent coronal planes, as shown is Figure 4.8.



Figure 4.8: Coronal planes spaced at equal intervals placed depth-wise along the breast.

As mentioned before, each breast was divided into 4 quadrants according to the nipple position, the same set of coronal planes were applied on all the 4 quadrants. We put nine coronal planes spaced at equal intervals on the breast to cut it into ten vertical sections along the Z-axis. The depth of the breast was normalized along the Z-axis, such that the largest Z-coordinate is located at 1 and the smallest Z-coordinate is located at 0. Thus when we count the number of points within every two sequential coronal planes, each bin is collecting the same proportion of the whole breast for every breast. The number of points located on the surface mesh on or between every two sequential planes was counted and normalized by the total number of points in the ROI.

Because the point density for each subject is the same within ROI, we reasoned that the distribution of points on the torso represents the morphology of the breast. A coronal plane projection plot for each of the four grades is shown in Figure 4.9 to illustrate the idea. Contours shown in Figure 4.9 display points located on coronal planes with a interval of 6 mm. It is important to note



Figure 4.9: A simple coronal projection plot of Grade 0, 1, 2, and 3.

that nipple may or may not locate at the largest Z-value especially for highly ptotic breasts. For grade 0, which shows no ptosis, contours for superior and inferior part are circularly symmetric. With the ptosis grade increases, contours tend to be elliptical and non-symmetric.

Nine coronal planes cut the Z-axis into ten bins, with each bin representing a width of 0.1. Histograms for four quadrants were generated and concatenated in the order of a, b, c, and d. Histogram templates for each grade was generated by taking an average of all the breasts within each grade category.

Figure 4.10 and Figure 4.11 shows the coronal projection histogram templates of grade 0, 1, 2, and 3. Quadrant *a* covers bins 1 - 10, quadrant *b* covers bins 11 - 20, quadrant *c* covers bins 21 - 30, and quadrant *d* covers bins 31 - 40 as shown in Table 4.2. Within each quadrant, low bin numbers represent points closer to the chest, while higher bin numbers represent points closer to the nipple. With ptosis increases, nipple position moves downwards, the total number of point acquired in quadrants *a* and *b* increases, while that in quadrants *c* and *d* decreases.



Figure 4.10: Histogram templates for coronal plane analysis for grade 0 and grade 1. Four quadrants are concatenated in the order: a, b, c, and d.

Table 4.2: The relationship between quadrants	, bins, and the range	of values for each l	oin for coronal
projection.			

Quadrant a	Quadrant b	Quadrant c	Quadrant d	Range of Values
1	11	21	31	[0, 0.1)
2	12	22	32	[0.1, 0.2)
3	13	23	33	[0.2, 0.3)
4	14	24	34	[0.3, 0.4)
5	15	25	35	[0.4, 0.5)
6	16	26	36	[0.5, 0.6)
7	17	27	37	[0.6, 0.7)
8	18	28	38	[0.7, 0.8)
9	19	29	39	[0.8, 0.9)
10	20	30	40	[0.9, 1.0]



Figure 4.11: Histogram templates for coronal plane analysis for grade 2 and grade 3. Four quadrants are concatenated in the order: a, b, c, and d.

4.4 Surface Normal Analysis

The 3D torso image is composed of the underlying triangular mesh, as shown in Figure 4.12(b). We calculated the surface normal for each triangle within the surface mesh.



Figure 4.12: (a) Calculation of surface normal (b) Triangular surface mesh.

Surface normal is computed as the cross product of two edges from the triangle, say \vec{a} and \vec{b} , as shown in Figure 4.12(a). For each triangle, if \vec{a} and \vec{b} are two vectors denoting two sides of one triangle, the surface normal of this triangle is

$$\vec{n} = \vec{a} \cdot \vec{b},\tag{4.3}$$

where \vec{n} is the vector of surface normal including 3 components, n_x , n_y and n_z in the X, Y and Z directions, respectively. The surface normal is normalized so that the length is one, i.e., $|\vec{n}| = 1$.

 n_x , which is the X component of the surface normal, represents the expanse of the breasts along X direction. n_z is the Z component of the surface normal, and it represents the degree of projection of the breast from the chest wall. n_x and n_z do not include information pertinent to breast ptosis. Thus, we eliminated these two components of the surface normal from further analysis.

 n_y was estimated to be the most informative component among the three for the analysis of ptosis. It represents the orientation of a breast along the Y-axes, and hence indicates the amount of drooping of the breast. Since points on the superior part of the breast largely exhibit the positive values for n_y (corresponding to an upward orientation), while points on the inferior part are typically negative (downward orientation). The distribution of n_y can portray the orientation of the

breast. Histograms for all quadrants were generated and concatenated in the order of a, b, c, and d. Histogram templates for each grade was generated by taking the average of all the breasts within the grade category. Figure 4.13 and Figure 4.14 show the histogram templates of the Y component of the surface normal for grades 0, 1, 2, and 3. Each quadrant covers 10 bins, in other words, quadrant a, b, c, and d covers bins 1 - 10, 11 - 20, 21 30, and 31 - 40, respectively as shown in Table 4.3. The Y component of the surface normal has a range of [-1, 1] so each bin possesses a range of 0.2. Within quadrant, lower bins represent negative surface normal values, while higher bins represent positive surface normal value.

Other than the difference in the number of points acquired in each quadrant, the histogram templates depict a transitional change in quadrant c and d across four grades. For grade 0, quadrants c and d have peaks in bin 25 and bin 35 respectively, which represents the range [-0.2, 0]. They were introduced by points around nipple area that were pointing straight forward rather than downward. As ptosis increase, points acquired in the range [-0.2, 0] decrease because the nipple moves downward and the number of points acquired around nipple-areola area were pointing down, while lower negative y components becomes larger. For grade 3 patients, it is an extreme case with most of the points in quadrants c and d pointing downwards.

Quadrant a	Quadrant b	Quadrant c	Quadrant d	Range of Values
1	11	21	31	[-1.0, -0.8)
2	12	22	32	[-0.8, -0.6)
3	13	23	33	[-0.6, -0.4)
4	14	24	34	[-0.4, -0.2)
5	15	25	35	[-0.2, 0)
6	16	26	36	[0, 0.2)
7	17	27	37	[0.2, 0.4)
8	18	28	38	[0.4, 0.6)
9	19	29	39	[0.6, 0.8)
10	20	30	40	[0.8, 1.0]

Table 4.3: The relationship between quadrants, bins, and the range of values for each bin for the Y component of the surface normal.



Figure 4.13: Histogram templates for the Y component of the surface normal for grade 0 and grade 1. Four quadrants are concatenated in the order: a, b, c, and d.



Figure 4.14: Histogram templates for the Y component of the surface normal for grade 2 and grade 3. Four quadrants are concatenated in the order: a, b, c, and d.

4.5 Histogram Matching

The similarity of the histogram template and the test case was computed by measuring the Bhattacharyya distance [64]. The Bhattacharyya measure can be used to compare the similarity between two histograms as follows. H and R represent two normalized histograms such that

$$\sum_{i} H_i = 1, \tag{4.4}$$

and

$$\sum_{i} R_i = 1. \tag{4.5}$$

If we let H_i be the histogram value in bin *i*, and R_i the histogram value in the same bin. The Bhattacharyya distance can be computed using the following equation

$$d(H,R) = \sqrt{1 - \frac{1}{\sqrt{\bar{H}\bar{R}N^2}} \sum_{i} \sqrt{H_i \cdot R_i}},\tag{4.6}$$

where

$$\bar{H} = \frac{1}{N} \sum_{i} H_i, \tag{4.7}$$

and N is the total number of bins in the histogram.

Bhattacharyya distance has the result in the scale of [0, 1]. d(H, R) = 0 or closer to 0 means a better match, whereas d(H, R) = 1 or closer to 1 means less similar. The rule of prediction is that by computing the Bhattacharyya distance between the test case's histogram and four template histograms, the grade with the smallest distance is set to be the predicted ptosis grade.

4.6 Statistical Measurement of Performance

In general, the result of classification can be characterized into four kinds: true positive (TP), false positive (FP), true negative (TN) and false negative (FN). Taking grade 0 for example:

• True positive means breasts of grade 0 were correctly identified as grade 0.

- False positive means breasts of other grades (grade1, 2, and 3) that were incorrectly identified as grade 0.
- True negative means breasts of other grades (grade1, 2, and 3) that were correctly rejected as not grade 0.
- False negative means breasts of grade 0 that were incorrectly identified as other grades (grade1, 2, or 3).

Several statistical analyses are made based on the following formula

• Sensitivity is defined as the proportion of actual positives which are correctly identified, with the formula,

$$Sensitivity = \frac{TP}{TP + FN}.$$
(4.8)

• **Specificity** is defined as the proportion of negatives which are correctly identified, with the formula,

$$Specificity = \frac{TN}{TN + FP}.$$
(4.9)

• Accuracy measures the proportion of true result, with the formula,

$$Accuracy = \frac{TP + TN}{TP + FP + TN + FN}.$$
(4.10)

• **Precision or Positive Prediction Value (PPV)** is defined as the proportion of the true positives against all the positive results, with the formula,

$$Precision = \frac{TP}{TP + FP}.$$
(4.11)

• **F** score is a measure of accuracy and can be defined as the harmonic mean of precision and sensitivity, with the formula,

$$FScore = \frac{2 \times precision \times sensitivity}{precision + sensitivity}.$$
(4.12)

Chapter 5

Results

In this chapter we evaluated the potential of different 3D features for categorizing breast ptosis from 3D scans of female torso. The performance of our algorithm on predicting ptosis grade is compared with the performance of subjective rating and the the performance of 2D photogrammetric measurement. The inter-observer variability between two surgeons' rating is also assessed.

5.1 Experimental Setup

In this study, we used patient images captured using the 3dMD TorsoTM system from 3dMD LLC, Atlanta Georgia. 3D torso images were taken from female patients undergoing breast reconstruction surgery at The University of Texas M. D. Anderson Cancer Center, Houston, TX. For this study, we selected subjects with the breast mount intact and the nipple clearly visible, This criteria was established because a clearly visible nipple was necessary for subjective rating which is visually estimated based on the level of nipple with respect to the terminus of the IMF. The data included a total of 247 breasts, from 170 patients and 5 commissioned volunteers. The sample subject population is a reflection of the distribution of the various grades observed in general population. Table 5.1 shows the number of breast for each grade in our data set. All subjects were chosen to have a complete torso image without holes or other artifacts such as missing data on the surface mesh, specifically over the region of interest encompassing the breast gland.

5.2 Evaluation of Objective Measurements on 3D Images

Cross-validation is a validation technique typically used to estimate the performance of a predictive model. For each round of cross-validation, the data set is partitioned into two complementary subsets, a training set and a test set. The training set is used to perform the analysis, while the test set is used to validate the analysis. Usually multiple rounds of cross-validation are performed on

Grade	Left	Right	Total
Grade 0	44	43	87
Grade 1	39	52	91
Grade 2	28	18	46
Grade 3	12	11	23

Table 5.1: Distribution of the number of left and right breast for every grade.

different partitions of the data set and the validation result is averaged over rounds. In leave-one-out cross-validation (LOOCV), as its name suggests, the data set is partitioned into two subsets: one sample data in the test set and the remaining samples in the training set. It is repeated such that all samples are used once as a test set.

We performed LOOCV on 203 breasts randomly chosen from the 247 breasts as the data set, including 71 breasts of grade 0, 75 breast of grade 1, 35 breasts of grade 2 and 22 breasts of grade 3. For each test, we picked one breast out of the data set as the test case, and the remaining 202 breasts formed the training set. Template histograms were generated for each grade by taking average of all the individual histograms for each breast image in the training data set. The cross-validation analysis was repeated for 203 times so that each subject image in the data set was used once as the validation data.

5.2.1 Gaussian Curvature

We evaluated the performance of using Gaussian curvature as a feature by conducting LOOCV on the 203 breast images. Table 5.2 and Table 5.3 show the cumulative and averaged confusion matrix for the LOOCV result. We used an experienced surgeon's rating as the ground truth. Table 5.4 shows the statistical measurements of the performance of Gaussian curvature. The statistical measures include sensitivity, specificity, accuracy, precision, F score and PPV for each grade. An overall performance was computed by averaging the values over all grades. Figure 5.1 shows the measurements for all grades and the overall performance.

Gaussian curvature provided a high accuracy on grade 3 of 83%. The accuracy of grade 0, grade 1 and grade 2 were 75%, 60% and 76%, which leads to an overall accuracy of 73%. Grade 3

	Predicted Grade								
Ground Truth	0	1	2	3					
0	40	29	2	0					
1	17	34	11	13					
2	3	11	2	19					
3	0	1	2	19					

Table 5.2: Cumulative confusion matrix for the result of LOOCV using Gaussian curvature as a feature.

Table 5.3: Averaged confusion matrix for the result of LOOCV using Gaussian curvature as a feature.

	Predicted Grade									
Ground Truth	0	1	2	3						
0	0.1970	0.1429	0.0099	0.0000						
1	0.0837	0.1675	0.0542	0.0640						
2	0.0148	0.0542	0.0099	0.0936						
3	0.0000	0.0049	0.0099	0.0936						

Table 5.4: Statistical measurements for the performance of Gaussian curvature as a feature.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.6667	0.4533	0.1176	0.3725	0.4025
Specificity	0.7832	0.6797	0.8226	0.9803	0.8165
Accuracy	0.7488	0.5961	0.7635	0.8276	0.7345
Precision	0.5634	0.4533	0.0571	0.8636	0.4845
F score	0.6107	0.4533	0.0769	0.5205	0.4155
PPV	0.5634	0.4533	0.0571	0.8636	0.4845



Figure 5.1: Statistical measurements for the performance of Gaussian curvature as a feature.

also showed a high precision rate of 86%, indicating that the performance of Gaussian curvature for predicting grade 3 is relatively good.

5.2.2 Coronal Projection

We evaluated the performance of using coronal projection as a feature by conducting LOOCV on the same 203 breast images. Table 5.5 and Table 5.6 show the cumulative and averaged confusion matrix, respectively for the LOOCV result. We used an experienced surgeon's rating as the ground truth. Table 5.7 shows the statistical measurements of the performance of coronal projection. An overall performance was computed by averaging the values over all grades. Figure 5.2 shows the statistical measurements for all grades and the overall performance.

Table 5.5: Cumulative confusion matrix for the result of LOOCV using coronal projection as a feature.

	Predicted Grade									
Ground Truth	0	1	2	3						
0	25	23	23	0						
1	4	35	32	4						
2	1	7	19	8						
3	0	2	8	12						

Table 5.6: Averaged confusion matrix for the result of LOOCV using coronal projection as a feature.

	Predicted Grade								
Ground Truth	0	1	2	3					
0	0.1232	0.1133	0.1133	0.0000					
1	0.0197	0.1724	0.1576	0.0197					
2	0.0049	0.0345	0.0936	0.0394					
3	0.0000	0.0099	0.0394	0.0591					

Table 5.7: Statistical measurements for the performance of coronal projection as a feature.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.8333	0.5224	0.2317	0.5000	0.5219
Specificity	0.7341	0.7059	0.8678	0.9441	0.8130
Accuracy	0.7488	0.6453	0.6108	0.8916	0.7241
Precision	0.3521	0.4667	0.5429	0.5455	0.4768
F score	0.4950	0.4930	0.3248	0.5217	0.4586
PPV	0.3521	0.4667	0.5429	0.5455	0.4768

Coronal projection provided a high accuracy on grade 3 of 89% and precision rate of 55%, with the accuracy for other grades falling in the range of 60%-75%. The overall accuracy was determined to be 72% with a precision of 48%.



Figure 5.2: Statistical measurements for the performance of coronal projection as a feature.

5.2.3 Surface Normal

We evaluated the performance of using the Y component of the surface normal as a feature by conducting LOOCV on the same 203 breast images. Table 5.8 and Table 5.9 show the cumulative and averaged confusion matrix, respectively for the result. Table 5.10 shows the statistical measurements of the performance of the Y component of the surface normal. An overall performance was computed by averaging the values over all the grades. Figure 5.3 shows the statistical measurements for all grades and the overall performance.

Table 5.8:	Cumulated	confusion	matrix	for	the	result	of	LOOCV	using	the	Y	component	of	the
surface not	rmal as a fea	ture.							-			-		

	Predicted Grade						
Ground Truth	0	1	2	3			
0	57	9	5	0			
1	29	32	10	4			
2	2	18	6	9			
3	0	0	8	14			

Table 5.9:	Averaged	confusion	matrix	for	the	result	of	LOOCV	using	the	Y	component	of	the
surface nor	mal as a fe	ature.							-			-		

		Predicted Grade					
Ground Truth	0	1	2	3			
0	0.2808	0.0443	0.0246	0.0000			
1	0.1429	0.1576	0.0493	0.0197			
2	0.0099	0.0887	0.0296	0.0443			
3	0.0000	0.0000	0.0394	0.0690			

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.6477	0.5424	0.2069	0.5185	0.4789
Specificity	0.8783	0.7014	0.8333	0.9545	0.8419
Accuracy	0.7783	0.6552	0.7438	0.8966	0.7685
Precision	0.8028	0.4267	0.1714	0.6364	0.5093
F score	0.7170	0.4776	0.1875	0.5714	0.4884
PPV	0.8028	0.4267	0.1714	0.6364	0.5093

Table 5.10: Statistical measurements for the performance of the Y component of the surface normal as a feature.



Figure 5.3: Statistical measurements for the performance of the Y component of the surface normal as a feature.

The Y component of the surface normal provided a good accuracy of 77% on grade 0, 65% on grade 1, 74% on grade 2 and 90% on grade 3, and had an overall accuracy of 77%. Grade 0 and grade 3 also had a high precision rate of 80% and 64%. This suggests that the Y component of surface normal is a relatively strong feature for predicting grade 0 and 3.

5.2.4 Combination of Features

We next evaluated the potential of different combinations of features to determine which combination, if any, allows improved classification. Gaussian curvature, coronal projection, or surface normal, independently do not provide high accuracy and precision for all four grades, but have the potential of identify ptosis on specific grades, i.e. Gaussian curvature and the Y component of the surface normal have a good performance on predicting Grade 0 and grade 3, while coronal

projection provided the best performance on predicting grade 2. Thus, we evaluated the effect of combining features for prediction of the ptosis grade. Concatenation of individual templates was done to facilitate the evaluation of various combinations of features.

5.2.4.1 Gaussian Curvature and Coronal Projection

We evaluated the combination of Gaussian curvature and coronal projection as features. A normalized and concatenated template of Gaussian curvature and coronal projection was generated for each grade. LOOCV was performed on the same 203 breast images. Table 5.11 and Table 5.12 show the cumulative and average confusion matrix, respectively for the result. Table 5.13 shows the statistical measurements of the performance. An overall performance was computed by averaging all four grades. Figure 5.4 shows the statistical measurements for all grades and the overall performance.

Table 5.11: Cumulative confusion matrix for the result of LOOCV using Gaussian curvature and coronal projection as features.

		Predicted Grade					
Ground Truth	0	3					
0	33	22	16	0			
1	13	29	25	8			
2	2	7	16	10			
3	0	0	3	19			

Table 5.12: Averaged confusion matrix for the result of LOOCV using Gaussian curvature and coronal projection as features.

	Predicted Grade						
Ground Truth	0	1	2	3			
0	0.1626	0.1084	0.0788	0.0000			
1	0.0640	0.1429	0.1232	0.0394			
2	0.0099	0.0345	0.0788	0.0493			
3	0.0000	0.0000	0.0148	0.0936			

5.2.4.2 Gaussian Curvature and the Y Component of the Surface Normal

We evaluated the combination of Gaussian curvature and the Y component of surface normal as features. A normalized and concatenated template of Gaussian curvature and the Y component

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.6875	0.5000	0.2667	0.5135	0.4919
Specificity	0.7548	0.6828	0.8671	0.9819	0.8217
Accuracy	0.7389	0.6305	0.6897	0.8966	0.7389
Precision	0.4648	0.3867	0.4571	0.8636	0.5431
F score	0.5546	0.4361	0.3368	0.6441	0.4929
PPV	0.4648	0.3867	0.4571	0.8636	0.5431

Table 5.13: Statistical measurements for the performance of Gaussian curvature and Coronal projection as features.



Figure 5.4: Statistical measurements for the performance of Gaussian curvature and Coronal Projection as features.

of surface normal was generated for each grade. LOOCV was performed on the same 203 breast

images. Table 5.14 and Table 5.15 show the cumulative and averaged confusion matrix, respectively

for the result. The statistical measurements are presented in Table 5.16 and plotted in Figure 5.5.

Table 5.14: Cumulative confusion matrix for the result of LOOCV using Gaussian curvature and the Y component of the surface normal as features.

		Predicted Grade					
Ground Truth	0	1	2	3			
0	54	15	2	0			
1	21	36	11	7			
2	3	14	6	12			
3	0	0	7	15			

Table 5.15: Averaged confusion matrix for the result of LOOCV using Gaussian curvature and the Y component of the surface normal as features.

	Predicted Grade						
Ground Truth	0	0 1 2					
0	0.2660	0.0739	0.0099	0.0000			
1	0.1034	0.1773	0.0542	0.0345			
2	0.0148	0.0690	0.0296	0.0591			
3	0.0000	0.0000	0.0345	0.0739			

Table 5.16: Statistical measurements for the performance of Gaussian curvature and the Y component of the surface normal as features.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.6923	0.5538	0.2308	0.4412	0.4795
Specificity	0.8640	0.7174	0.8362	0.9586	0.8440
Accuracy	0.7980	0.6650	0.7586	0.8719	0.7734
Precision	0.7606	0.4800	0.1714	0.6818	0.5235
F score	0.7248	0.5143	0.1967	0.5357	0.4929
PPV	0.7606	0.4800	0.1714	0.6818	0.5235



Figure 5.5: Statistical measurements for the performance Gaussian curvature and the Y component of the surface normal as features.

5.2.4.3 Coronal Projection and the Y component of surface normal

We evaluated the combination of coronal projection and the Y component of the surface normal. A normalized and concatenated template of coronal projection and Y component of surface normal was generated for each grade. LOOCV was performed on the same 203 breast images. Table 5.17 and Table 5.18 show the cumulative and averaged confusion matrix, respectively for the result. The statistical measurements are presented in Table 5.19 and plotted in Figure 5.6.

Table 5.17: Cumulative confusion matrix for the result of LOOCV using coronal projection and the Y component of the surface normal as features.

		Predicted Grade						
Ground Truth	0	0 1 2 3						
0	49	14	8	0				
1	23	31	18	3				
2	2	11	14	8				
3	0	1	6	15				

Table 5.18: Averaged confusion matrix for the result of LOOCV using coronal projection and the Y component of the surface normal as features.

	Predicted Grade					
Ground Truth	0	1	2	3		
0	0.2414	0.0690	0.0394	0.0000		
1	0.1133	0.1527	0.0887	0.0148		
2	0.0099	0.0542	0.0690	0.0394		
3	0.0000	0.0049	0.0296	0.0739		

Table 5.19: Statistical measurements for the performance of coronal projection and the Y component of the surface normal as features.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.6622	0.5439	0.3043	0.5769	0.5218
Specificity	0.8295	0.6986	0.8662	0.9605	0.8387
Accuracy	0.7685	0.6552	0.7389	0.9113	0.7685
Precision	0.6901	0.4133	0.4000	0.6818	0.5463
F score	0.6759	0.4697	0.3457	0.6250	0.5291
PPV	0.6901	0.4133	0.4000	0.6818	0.5463



Figure 5.6: Statistical measurements for the performance of coronal projection and the Y component of the surface normal as features.

5.2.4.4 All Features Combined

Finally, we combined all the three features together, by concatenating and normalizing all three templates. We evaluated the template by conducting LOOCV on the same 203 breast images. Table 5.20 and Table 5.21 show the cumulative and averaged confusion matrix, respectively for the result. The statistical measurements are presented in Table 5.22 and plotted in Figure 5.7.

Table 5.20: Cumulative confusion matrix for the result of LOOCV using all the three 3D measures as features.

	Predicted Grade				
Ground Truth	0	1	2	3	
0	50	13	8	0	
1	16	36	20	3	
2	3	11	12	9	
3	0	0	5	17	

Table 5.21: Averaged confusion matrix for the result of LOOCV using all the three 3D measures as features.

	Predicted Grade				
Ground Truth	0	1	2	3	
0	0.2463	0.0640	0.0394	0.0000	
1	0.0788	0.1773	0.0985	0.0148	
2	0.0148	0.0542	0.0591	0.0443	
3	0.0000	0.0000	0.0246	0.0837	

Table 5.22: Statistical measurements for the performance of all the three 3D measures as features.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.7246	0.6000	0.2667	0.5862	0.5444
Specificity	0.8433	0.7273	0.8544	0.9713	0.8491
Accuracy	0.8030	0.6897	0.7241	0.9163	0.7833
Precision	0.7042	0.4800	0.3429	0.7727	0.5750
F score	0.7143	0.5333	0.3000	0.6667	0.5536
PPV	0.7042	0.4800	0.3429	0.7727	0.5750

5.3 Evaluation of Subjective Rating

We had a team of two surgeons with experience in breast reconstruction who subjectively rated the ptosis grade using the Regnault's classification scale for the 203 breasts randomly chosen



Figure 5.7: Statistical measurements for the performance of the combination of all the three 3D features.

from the 247 breasts. We used the rating of the experienced senior surgeon (in terms of number of years in clinical practice) as the golden standard (i.e., ground truth) in our study. All the results were evaluated based on this surgeon's rating as the ground truth to maintain consistency.

We evaluated the result of ptosis graded by the other surgeon by comparing with the result from the senior surgeon which we used as ground truth. Table 5.23 shows the confusion matrix for subjective rating. From the table, we can see that the most disagreement amongst the two surgeons exists for grade 1 and grade 2.

	Predicted Grade				
Ground Truth	0	1	2	3	
0	41	21	9	0	
1	4	19	47	5	
2	0	5	16	15	
3	0	0	0	22	

Table 5.23: Confusion matrix for subjective rating of ptosis.

Table 5.24 (Figure 5.8) shows the statistical measures on the performance of subjective rating. Subjective rating had an relatively high accuracy of 84% on grade 0, and 91% on grade 3, but low accuracy of 60% on grade1 and 63% on grade 2, leading to an overall average accuracy of 74%. Grade 3 had a high precision rate of 1.0. Because grade 3 ptosis is an extreme case of breast ptosis so visually it can be easily identified. Whereas grade 1 and 2 had a lower precision rate of 25% and 44%, respectively, leading to an averaged precision of 57%.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.9111	0.4222	0.2222	0.5238	0.5198
Specificity	0.8113	0.6478	0.8485	1.0000	0.8269
Accuracy	0.8374	0.6010	0.6305	0.9064	0.7438
Precision/PPV	0.5775	0.2533	0.4444	1.0000	0.5688
F score	0.7069	0.3167	0.2963	0.6875	0.5018

Table 5.24: Statistical measures of the performance of subjective rating of ptosis.



Figure 5.8: Statistical measurements for the performance of subjective rating of ptosis.

5.4 Evaluation of LaTrenta and Hoffman's Classification

We performed the LaTrenta and Hoffman's quantitative classification [12] on the same data set (203 breasts), by computing the distance of the nipple from the terminus of IMF using our customized BR software [14]. An observer manually recorded the height of nipple level and that of the terminus of the IMF, and computed the vertical distance between nipple and the terminus of IMF. Grading was assessed according to LaTrenta and Hoffman's quantitative classification scheme as described earlier in Section 3.3.4. Table 5.25 presents the confusion matrix of the result. The ground truth was the ptosis grade determined by the experienced senior surgeon. Predicted ptosis grade was the result using LaTrenta and Hoffman's classification.

Table 5.26 (Figure 5.9) shows the statistical measurements of the performance of LaTrenta

	Predicted Grade				
Ground Truth	0	1	2	3	
0	51	8	12	0	
1	37	3	33	2	
2	11	2	17	5	
3	2	5	7	8	

Table 5.25: Cumulative confusion matrix for LaTrenta and Hoffman's classification using photogrammetry.

and Hoffmans classification. Grade 3 holds a relatively high accuracy of 90%, while grade 0, 1, and 2 exhibit a relatively lower accuracy at 65%, 57% and 66%, respectively. Also grade 0 has a relatively high precision of 72%, while grade 1, 2, and 3 have a low precision of 4%, 49% and 36% respectively, leading to an average precision of 40%.

Table 5.26: Statistical measures for the performance of LaTrenta and Hoffman's classification.

	Grade 0	Grade 1	Grade 2	Grade 3	Average
Sensitivity	0.5050	0.1667	0.2464	0.5333	0.3628
Specificity	0.8039	0.6108	0.8657	0.9255	0.8015
Accuracy	0.6552	0.5714	0.6552	0.8966	0.6946
Precision	0.7183	0.0400	0.4857	0.3636	0.4019
F score	0.5930	0.0645	0.3269	0.4324	0.3542
PPV	0.7183	0.0400	0.4857	0.3636	0.4019



Figure 5.9: Statistical measurements for performance of LaTrenta and Hoffman's classification.

5.5 Evaluation of Kim's Distance Ratio Methods

We evaluated Kim's objective methods using distance ratios [13] for assessing ptosis on 3D images. We randomly picked 64 breasts, with 16 breasts per grade out of the 247 as the training data set and made simple linear regressions on both methods. We evaluated the performance of the linear regression by testing on the same 203 breasts. We computed two distance ratios: measure 1: (s-i)/(s-n), measure 2: (n-v)/(i-v), where s-i represents vertical distance between sternal notch and lateral terminus, s-n is the vertical distance between sternal notch and nipple, n-v is the vertical distance between nipple and the lowest visible point, i-v is the vertical distance between sternal between lateral terminus and the lowest visible point. Based on the ground truth, linear regressions between the two distance ratios and the ground truth were determined. Figure 5.10 shows the simple linear regressions.

Based on the linear regressions of the two measurements, we evaluated the test set by mapping the distance ratios into a scale of [0, 3]. We set the nearest integer as the predicted grade. Table 5.27 and Table 5.28 show the confusion matrices for the result using measure 1 and measure 2. Figure 5.11 shows the average performance of Kim's distance ratio methods. Measure 1 has an accuracy of 65%, 46%, 64% and 90% for grade 0, 1, 2, and 3 respectively, leading to an average accuracy of 66%. Measure 2 has an accuracy of 65%, 40%, 62% and 88% for grade0, 1, 2, and 3 respectively, leading to an average accuracy of 64%.

	Predicted Grade				
Ground Truth	0	1	2	3	
0	0	52	19	0	
1	0	38	35	2	
2	0	11	24	0	
3	0	9	9	4	

Table 5.27: Confusion matrix for the result using distance ratios (measure 1).



Figure 5.10: Linear regression of distance ratios with subjective scores. Table 5.28: Confusion matrix for the result using distance ratios (measure 2).

	Predicted Grade				
Ground Truth	0	1	2	3	
0	0	62	9	0	
1	0	34	41	0	
2	0	11	18	6	
3	0	7	11	4	



Figure 5.11: Statistical measurements for the performance of Kim's distance ratio method.

5.6 Discussion

So far, we evaluated the performance of our 3D measurements, as well as subjective rating, LaTrenta and Hoffman's classification and Kim's distance ratio methods based on the same 203 breast images. Figure 5.12 shows a comparison of statistical result over all the measurements on grade 0. In the following figures, LaTrenta and Hoffman's classification is abbreviated as LH, G represents Gaussian curvature, P represents coronal projection, and Ny indicates the Y component of the surface normal. According to Figure 5.12, subjective measurement provided the highest accuracy (84%) but relative low precision rate (58%). All the 3D features and their combinations provided higher accuracy over LaTrenta and Hoffman's classification and Kim's distance ratio measurements. The combination of all three features provided the highest accuracy of 80% and precision rate of 70% among all the 3D features. Moreover, Ny provided the highest precision rate of 80% as well as a high accuracy of 78%.

Figure 5.13 shows a comparison of statistical result over the subjective measurement, La-Trenta and Hoffman's classification, Kim's distance ratios, and all the 3D measurements on grade 1. As seen in Figure 5.13, the overall performance of 3D features is better than that of subjective measurement, and 2D photogrammetry (LaTrenta and Hoffman's classification, and Kim's measurements). The combination of all the three features provided the best performance on grade 1


Figure 5.12: A comparison of the performance of subjective measurement, 2D photogrammetry, and 3D stereophotogrammetry for assessing grade 0.

with the accuracy of 69% and precision rate of 48%.



Figure 5.13: A comparison of the performance of subjective measurement, 2D photogrammetry, and 3D stereophotogrammetry for assessing grade 1.

Figure 5.14 shows a comparison of the performance of subjective rating, photogrammetry and stereophotogrammetry for grade 2. According to Figure 5.14, all the 3D measurements provided a higher accuracy over the other methods. The combination of all three features provided the best performance by having an accuracy of 76% and precision rate of 34% among all the 3D features.

Figure 5.15 shows a comparison of the performance of statistical result all the measurements for grade 3. As seen in Figure 5.15, subjective rating provided the highest accuracy of 91% and precision rate of 100%. Because grade 3 is the extreme case of ptosis, it is easy to visually identify.



Figure 5.14: A comparison of the performance of subjective measurement, 2D photogrammetry, and 3D stereophotogrammetry for assessing grade 2.

All the 3D measurements provided a better performance than LaTrenta and Hoffman's classification and Kim's measurements by having higher precision rate. The best feature for identifying grade 3 is G+P, with an accuracy of 90% and precision rate of 86%.



Figure 5.15: A comparison of the performance of subjective measurement, 2D photogrammetry, and 3D stereophotogrammetry for assessing grade 3.

Table 5.29 and Figure 5.16 shows a comparison of the average performance over all the approaches evaluated. Subjective rating of breast ptosis provided a good performance with an accuracy of 74% and precision rate of 57%. LaTrenta and Hoffman's classification and Kim's distance ratio measurements provided a lower accuracy of around 60%-70% and precision rate of around 29%-40%. This indicated that the LaTrenta and Hoffman's classification and Kim's measurement used on

3D image were suboptimal. All the 3D measurements exhibited good performance with accuracy in the range of 73%-78% and precision rate of 48%-57%. The best feature for the overall performance was G+P+Ny, which was the combination of all three 3D features. It provided an accuracy of 78% and precision rate 57%.

Table 5.29: A comparison of the overall performance of subjective rating, 2D photogrammetry, and 3D stereophotogrammetry.

Average	Sub	LH	Kim_1	Kim_2	G	P	Ny	G+P	G+Ny	P+Ny	G+P+Ny
Sensitivity	0.52	0.36	0.32	0.23	0.40	0.52	0.48	0.49	0.48	0.52	0.54
Specificity	0.83	0.80	0.77	0.74	0.82	0.81	0.84	0.82	0.84	0.84	0.85
Accuracy	0.74	0.69	0.66	0.64	0.73	0.72	0.77	0.74	0.77	0.77	0.78
Precision	0.57	0.40	0.34	0.29	0.48	0.48	0.51	0.54	0.52	0.55	0.57
F score	0.50	0.35	0.27	0.23	0.42	0.46	0.49	0.49	0.49	0.53	0.55
PPV	0.57	0.40	0.34	0.29	0.48	0.48	0.51	0.54	0.52	0.55	0.57



Figure 5.16: A comparison of the overall performance of subjective measurement, 2D photogrammetry, and 3D stereophotogrammetry for assessing grades 0-3.

In conclusion, all the 3D features and their combinations provided a good performance compared to subjective measurement, LaTrenta and Hoffman's classification and Kim's distance ratio methods by having a higher accuracy and higher precision rate. The best feature is the combination of Gaussian curvature, the coronal projection and the Y component of surface normal since it provides the highest accuracy of 78% and precision rate of 57% on the average performance.

Chapter 6

Conclusion

Development of an objective and quantitative method for measuring ptosis from 3D images is an important yet challenging task. Prior work mainly focused on either subjective rating, anthropometry or 2D photogrammetry. In this study, we proposed a new approach for measuring breast ptosis using 3D torso scans. We explored unique 3D morphological features from stereophotogrammetry that surpass the need of predefining the terminus of IMF. We investigated Gaussian curvature, coronal projection and the Y component of surface normal as features and built a 3D ptosis classification model. The results demonstrate that our new approach on 3D images yielded better performance compared to both subjective measurements and 2D photogrammetry.

Currently we employ three feature sets in training the model. However, the margin of each decision boundary is relatively small, which results in a higher rate of false positives and negatives. In future work, we will explore additional 3D features. Furthermore, the current features we chose are linearly combined together and assumed to be mutually exclusive from each other for simplicity. In real world, however, features may be correlated. Thus a more sophisticated multi-variant discriminant model needs to be explored.

We used the native histogram estimator where the feature space is divided into equal-sized bins. In addition, we used the Bhattacharyya distance to calculate the distance between histograms. More powerful machine learning approaches can be employed in future work. For instance, the k-means clustering method can be used where images are partitioned into k clusters in which the ones with same grade belong to one cluster with the nearest mean distance.

Last but not least, an important direction of the future work is to automating the assessment procedure. Currently our method is semi-automated where the 3D images need to be manually cropped before the following processes can be adopted. However, it would be desirable to have a completely automated algorithm, that incorporates computerized cropping and fiducial point detec-

tion to achieve robust and speedy prediction of breast ptosis.

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Appendix A

Objective Measurements on 3D Images

A.1 LOOCV Results for Gaussian Curvature Analysis

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
1	003L	0	С	0.29916	0.30966	0.33343	0.36380
2	003R	0	С	0.29837	0.33013	0.35388	0.40316
3	005R	0	С	0.34447	0.34695	0.36428	0.37918
4	007L	0	1	0.41064	0.40211	0.41260	0.42019
5	007R	0	1	0.39904	0.39369	0.40562	0.41396
6	008R	0	С	0.29619	0.31656	0.34022	0.36932
7	009L	0	С	0.50018	0.51879	0.53310	0.57613
8	013R	0	С	0.35243	0.37436	0.39705	0.42723
9	016R	0	С	0.32645	0.36588	0.38100	0.41192
10	025L	0	С	0.34518	0.37850	0.39695	0.43935
11	029R	0	С	0.42413	0.44488	0.47157	0.50747
12	037L	0	С	0.32176	0.33129	0.33971	0.36786
13	037R	0	С	0.35342	0.37035	0.38490	0.41795
14	046L	0	1	0.25794	0.24753	0.25624	0.28043
15	046R	0	1	0.27530	0.27443	0.29077	0.32497
16	049L	0	С	0.24041	0.24499	0.27305	0.32016
17	053L	0	С	0.26496	0.30646	0.32768	0.37252
18	053R	0	С	0.29683	0.35471	0.35551	0.41694
19	055L	0	С	0.26636	0.30035	0.30336	0.33334
20	055R	0	С	0.34894	0.38657	0.40222	0.43085
21	067R	0	С	0.24930	0.28365	0.29883	0.34283
22	073R	0	С	0.25085	0.25655	0.27499	0.31292
23	076L	0	С	0.39989	0.45721	0.45437	0.51058
24	078L	0	С	0.33857	0.37666	0.39214	0.42931
25	079R	0	С	0.20375	0.24329	0.25791	0.31334
26	084L	0	1	0.29684	0.29151	0.29977	0.31840
27	084R	0	1	0.33204	0.32450	0.34066	0.36421
28	088R	0	С	0.32066	0.33705	0.35302	0.38812
29	089R	0	С	0.22995	0.24177	0.26390	0.28789
30	093L	Õ	Č	0.22275	0.26130	0.28456	0.33294
31	096L	0	C	0.23445	0.24607	0.26932	0.29406
32	113R	0	Č	0.22509	0.24068	0.25901	0.29031
33	131R	0	C	0.27729	0.33767	0.35432	0.39922
34	135R	0	C	0.29444	0.33829	0.36039	0.40229
35	154R	0	Č	0.21507	0.22758	0.25033	0.29832
36	160L	0	1	0.22495	0.21431	0.23679	0.24737
37	175L	0	С	0.27359	0.28841	0.28800	0.31690
38	183L	0	С	0.19472	0.21785	0.23683	0.29615
39	186R	0	C	0.29132	0.31311	0.32624	0.35287
40	188R	0	1	0.24266	0.21325	0.25583	0.26918
41	192L	0	С	0.24031	0.25993	0.27794	0.31176
42	200L	0	1	0.19849	0.17950	0.19749	0.21450
43	201R	0	С	0.21785	0.22491	0.23927	0.27714
44	203L	Ő	1	0.25131	0.23593	0.23633	0.25745
45	204L	Ő	2	0 24748	0.21771	0.20761	0 22039

Table A.1: LOOCV results for Gaussian curvature analysis.

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
46	205L	0	1	0.24795	0.24070	0.25027	0.27829
47	205R	Ő	1	0.22714	0.21550	0.23654	0.26209
48	211R	Õ	2	0.26831	0.25313	0.24484	0.24976
49	217L	Õ	1	0.21101	0.17106	0.17680	0.18720
50	220L	Õ	Ċ	0.20916	0.24558	0.24970	0.29677
51	220R	0	С	0.21727	0.25015	0.27103	0.30998
52	505L	0	С	0.27044	0.28260	0.29600	0.32372
53	505R	0	С	0.26951	0.29508	0.32407	0.36117
54	508R	0	1	0.26905	0.21762	0.23712	0.24505
55	511L	0	1	0.26962	0.21500	0.22143	0.23174
56	523L	0	1	0.24116	0.20208	0.21731	0.22837
57	528R	0	1	0.23989	0.20955	0.23061	0.24448
58	529L	0	С	0.29148	0.30523	0.31691	0.36334
59	529R	0	С	0.25475	0.28124	0.30025	0.33182
60	535L	0	1	0.22902	0.20396	0.21732	0.23475
61	535R	0	1	0.22214	0.18505	0.21078	0.22388
62	542L	0	1	0.23291	0.20876	0.22952	0.23117
63	542R	0	1	0.23852	0.23213	0.26225	0.28797
64	554L	0	1	0.26035	0.25611	0.26009	0.26899
65	554R	0	1	0.26895	0.25626	0.26216	0.26597
66	700R	0	1	0.25316	0.21445	0.24512	0.25391
67	702L	0	1	0.22831	0.21178	0.23742	0.25460
68	702R	0	1	0.23802	0.22403	0.24861	0.25554
69	704R	0	1	0.25220	0.22568	0.24084	0.25579
70	705L	0	1	0.25256	0.23403	0.24846	0.25877
71	710L	0	1	0.27012	0.20431	0.21937	0.21635
72	006L	1	0	0.32103	0.32679	0.33277	0.35696
73	012L	1	0	0.38616	0.39313	0.39304	0.41444
74	012R	1	0	0.36726	0.37457	0.38296	0.40062
75	018L	1	0	0.37260	0.39590	0.40486	0.44056
76	018R	1	0	0.37706	0.40441	0.42551	0.44663
77	022L	1	0	0.38783	0.40178	0.41946	0.44279
78	022R	1	0	0.37390	0.39463	0.41414	0.44612
79	023L	1	0	0.37297	0.38629	0.40350	0.43099
80	023R	1	0	0.35539	0.38735	0.40305	0.44875
81	027R	1	2	0.45790	0.46702	0.45000	0.45337
82	047L	1	С	0.21731	0.19808	0.20970	0.20947
83	047R	1	С	0.26153	0.24483	0.26020	0.29528
84	049R	1	0	0.24807	0.26242	0.28793	0.33605
85	056L	1	С	0.17169	0.14833	0.15126	0.18748
86	057R	1	2	0.20440	0.17803	0.17765	0.20383
87	060L	1	0	0.23225	0.24567	0.26492	0.28566
88	069R	1	0	0.22761	0.23166	0.24950	0.27541
89	070R	1	С	0.21216	0.18901	0.20218	0.22355
90	075R	1	0	0.20386	0.20693	0.22223	0.24496
91	082L	1	С	0.21128	0.19374	0.20778	0.23312
92	086L	1	С	0.20409	0.18749	0.19515	0.23358
93	094R	1	С	0.20081	0.19498	0.20603	0.24238
94	095R	1	С	0.26335	0.25114	0.25143	0.25119
95	098R	1	С	0.22892	0.21965	0.23785	0.25301
96	124R	1	0	0.27046	0.28082	0.29992	0.33704
97	133L	1	С	0.18721	0.15824	0.16626	0.17330
98	133R	1	С	0.21454	0.21259	0.22407	0.23102
99	163R	1	С	0.28373	0.27333	0.28247	0.30668
100	181L	1	0	0.26839	0.26900	0.28062	0.30897

Table A.1: LOOCV results for Gaussian curvature analysis (continuted).

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	101	184L	1	0	0.20083	0.20393	0.21584	0.26539
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	102	190L	1	0	0.22563	0.23387	0.25225	0.26470
	103	197R	1	С	0.26089	0.23241	0.23854	0.26278
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	104	199L	1	С	0.21452	0.19644	0.20661	0.23227
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	105	200R	1	С	0.21264	0.20235	0.20934	0.21785
	106	203R	1	С	0.21921	0.21821	0.23662	0.27411
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	107	204R	1	2	0.24475	0.21923	0.21651	0.21844
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	108	209R	1	3	0.23614	0.17771	0.16716	0.15713
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	109	210L	1	3	0.28592	0.23029	0.22262	0.19509
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	110	219L	1	С	0.25741	0.23562	0.23943	0.25347
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	111	507L	1	2	0.26660	0.21786	0.20407	0.20743
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	112	507R	1	3	0.28835	0.23264	0.23114	0.22162
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	113	509R	1	2	0.31547	0.26670	0.25052	0.25952
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	114	511R	1	С	0.26846	0.20740	0.21643	0.20750
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	115	512R	1	С	0.23671	0.20460	0.21384	0.23581
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	116	514L	1	С	0.27567	0.23471	0.23536	0.23971
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	117	515L	1	C	0.27760	0.23640	0.24738	0.24579
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	118	515R	1	C	0.29948	0.24953	0.25708	0.25015
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	119	516L	1	3	0.31091	0.25248	0.22728	0.20862
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	120	516R	1	2	0.31361	0.25966	0.25460	0.25463
122517R13 0.32320 0.26459 0.2514 0.25385 123521L1C 0.23155 0.20113 0.21127 0.23529 124522R1C 0.20801 0.18990 0.21135 0.19453 125523R13 0.27482 0.21409 0.21135 0.19453 126527L12 0.27619 0.24328 0.23756 0.25359 127527R1C 0.22115 0.19808 0.20690 0.22558 128534L13 0.26078 0.23058 0.21409 0.20520 129539R1C 0.22115 0.19390 0.21302 0.24065 130540L13 0.26006 0.21971 0.21338 0.19834 131541L13 0.27691 0.23305 0.22939 0.220492 132541R12 0.26347 0.22802 0.22314 134543R13 0.26347 0.22578 0.21913 136691L1C 0.25892 0.20628 0.20368 0.20420 138699R1C 0.2172 0.8771 0.23077 0.23744 140703R12 0.26728 0.22622 0.23077 0.23744 140703R12 0.26728 0.22622 0.23077 0.21168 139700L1C 0.258	121	517L	1	3	0.32959	0.27292	0.25139	0.23890
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	122	517R	1	3	0.32320	0.26459	0.25614	0.25385
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	123	521L	1	Č	0.23155	0.20113	0.21127	0.23529
125523R130.274820.214090.211350.19433126527L120.276190.243280.237560.25359127527R1C0.235160.198080.206900.22558128534L130.260780.230580.214090.20520129539R1C0.221150.193900.213020.24065130540L130.260060.219710.213380.19834131541L130.276910.233050.229390.24092133543L130.264430.230540.228720.22314134543R130.264430.230540.228020.22314135574R1C0.263470.245530.262810.29274136691L1C0.258920.206280.203680.20420138699R1C0.217720.189710.205270.2168139700L1C0.258950.225200.230930.2399141704L120.267280.226620.225210.23095144713L1C0.217720.186710.203090.21377143711L130.326380.275480.269250.26148144713L1C0.245670.228010.223990.23860142710R	124	522R	1	C	0.20801	0.18990	0.20318	0.21934
126527L120.276190.243280.237560.25359127527R1C0.235160.198080.206900.22558128534L130.268780.230580.214090.20520129539R1C0.221150.193900.213020.24065130540L130.260060.219710.213380.19834131541L130.260360.220890.22304132541R120.276910.233050.229390.24092133543L130.263290.220890.209340.19534134543R130.264430.230670.225780.21913136691L1C0.263470.245530.262810.29274137691R120.258920.206280.203680.20420138699R1C0.257670.211680.223990.23093141704L120.254670.228010.223990.23860142710R1C0.24770.189710.205270.21168143711L130.326380.275480.269250.26148144713L1C0.24670.228010.223990.23860142710R1C0.24670.245300.273170.21579143711L13<	125	523R	1	3	0.27482	0.21409	0.21135	0 19453
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	125	527L	1	2	0.27619	0.24328	0.23756	0.25359
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	120	527E	1	Ĉ	0.23516	0.19808	0.20690	0.22558
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	128	534L	1	3	0.26878	0.23058	0.21409	0.20520
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	120	539R	1	C C	0.20070	0.19390	0.21302	0.20520
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	130	540L	1	3	0.26006	0.21971	0.21338	0.19834
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	131	541L	1	3	0.20000	0.23380	0.23320	0.22304
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	132	541R	1	2	0.27691	0.23305	0.22939	0.22001
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	132	5431	1	3	0.26329	0.22089	0.22939	0.19534
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	134	543R	1	3	0.26443	0.23054	0.22802	0.22314
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	135	574R	1	Č	0.23680	0.20687	0.22578	0.21913
137 691R 1 2 0.25892 0.20628 0.20368 0.20420 138 699R 1 C 0.21772 0.18971 0.20527 0.21168 139 700L 1 C 0.25895 0.22252 0.23007 0.23744 140 703R 1 2 0.26728 0.22662 0.22399 0.23860 141 704L 1 2 0.25467 0.22801 0.22399 0.23860 142 710R 1 C 0.24942 0.19420 0.20814 0.21237 143 711L 1 3 0.32638 0.27548 0.26925 0.26148 144 713L 1 C 0.21475 0.17837 0.20000 0.22005 145 713R 1 C 0.22959 0.18613 0.20309 0.21170 146 717R 1 C 0.27264 0.24530 0.27317 0.27539 147 002L 2 0 0.40474 0.40955 0.41010 0.41360	136	691L	1	C	0.25300	0.24553	0.26281	0.29274
137 601R 1 C 0.21772 0.18971 0.20505 0.20185 138 699R 1 C 0.21772 0.18971 0.20527 0.21168 139 700L 1 C 0.25895 0.22252 0.23007 0.23744 140 703R 1 2 0.26728 0.22662 0.22399 0.23860 141 704L 1 2 0.25467 0.22801 0.22399 0.23860 142 710R 1 C 0.24942 0.19420 0.20814 0.21237 143 711L 1 3 0.32638 0.27548 0.26925 0.26148 144 713L 1 C 0.21475 0.17837 0.20000 0.22005 145 713R 1 C 0.22959 0.18613 0.20309 0.21170 146 717R 1 C 0.27264 0.24530 0.27317 0.27539 147 002L 2 0 0.40474 0.40955 0.41010 0.41360	137	691R	1	2	0.25892	0.20628	0.20201	0.2027
1301	138	699R	1	Ē	0.21772	0.18971	0.20527	0.21168
159 $100L$ 1 2 0.25053 0.22622 0.22521 0.23093 141 $703R$ 1 2 0.26728 0.22662 0.22521 0.23093 141 $704L$ 1 2 0.25467 0.22801 0.22399 0.23860 142 $710R$ 1 C 0.24942 0.19420 0.20814 0.21237 143 $711L$ 1 3 0.32638 0.27548 0.26925 0.26148 144 $713L$ 1 C 0.21475 0.17837 0.20000 0.22005 145 $713R$ 1 C 0.22959 0.18613 0.20309 0.21170 146 $717R$ 1 C 0.27264 0.24530 0.27317 0.27539 147 $002L$ 2 0 0.40474 0.40955 0.41010 0.41360 148 $010L$ 2 3 0.43068 0.43290 0.43238 0.41812 149 $026L$ 2 1 0.30743 0.30052 0.30827 0.30470 150 $029L$ 2 0 0.40198 0.45933 0.48630 0.54338 151 $065L$ 2 1 0.21395 0.20592 0.22059 0.24020 152 $066L$ 2 0 0.42383 0.43828 0.44287 0.45984 153 $189L$ 2 1 0.25435 0.24053 0.25728 0.25038 154 $208L$	130	7001	1	C	0.25895	0.22252	0.23007	0.23744
110 100 1 2 0.20120 0.22002 0.22391 0.22393 141 $704L$ 12 0.25467 0.22801 0.22399 0.23860 142 $710R$ 1C 0.24942 0.19420 0.20814 0.21237 143 $711L$ 13 0.32638 0.27548 0.26925 0.26148 144 $713L$ 1C 0.21475 0.17837 0.20000 0.22005 145 $713R$ 1C 0.22959 0.18613 0.20309 0.21170 146 $717R$ 1C 0.27264 0.24530 0.27317 0.27539 147 $002L$ 20 0.40474 0.40955 0.41010 0.41360 148 $010L$ 23 0.43068 0.43290 0.43238 0.41812 149 $026L$ 21 0.30743 0.30052 0.30827 0.30470 150 $029L$ 20 0.40198 0.45933 0.48630 0.54338 151 $065L$ 21 0.21395 0.20592 0.22059 0.24020 152 $066L$ 20 0.42383 0.43828 0.44287 0.45984 153 $189L$ 21 0.25435 0.24053 0.25728 0.25038 154 $208L$ 23 0.31454 0.24920 0.23135 0.18305 155 $214R$ 2C 0.24250 0.20494	140	703R	1	2	0.25075	0.22252	0.22521	0.23093
142 $710R$ 1 C 0.24942 0.19420 0.20814 0.21237 143 $711L$ 1 3 0.32638 0.27548 0.26925 0.26148 144 $713L$ 1 C 0.21475 0.17837 0.20000 0.22005 145 $713R$ 1 C 0.22959 0.18613 0.20309 0.21170 146 $717R$ 1 C 0.27264 0.24530 0.27317 0.27539 147 $002L$ 2 0 0.40474 0.40955 0.41010 0.41360 148 $010L$ 2 3 0.43068 0.43290 0.43238 0.41812 149 $026L$ 2 1 0.30743 0.30052 0.30827 0.30470 150 $029L$ 2 0 0.40198 0.45933 0.48630 0.54338 151 $065L$ 2 1 0.21395 0.20592 0.22059 0.24020 152 $066L$ 2 0 0.42383 0.43828 0.44287 0.45984 153 $189L$ 2 1 0.25435 0.24053 0.25728 0.25038 154 $208L$ 2 3 0.31454 0.24920 0.23135 0.18305 155 $214R$ 2 C 0.24250 0.20494 0.20058 0.21340	141	704L	1	2	0.25467	0.22801	0.22321	0.23860
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	142	710R	1	Ē	0.24942	0.19420	0.20814	0.21237
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	143	7111	1	3	0.32638	0.27548	0.26925	0.26148
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	144	713L	1	Č	0.21475	0.17837	0.20020	0.22005
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	145	713R	1	Č	0.22959	0.18613	0.20309	0.21170
147 002L 2 0 0.40474 0.40955 0.41010 0.41360 148 010L 2 3 0.43068 0.43290 0.43238 0.41812 149 026L 2 1 0.30743 0.30052 0.30827 0.30470 150 029L 2 0 0.40198 0.45933 0.48630 0.54338 151 065L 2 1 0.21395 0.20592 0.22059 0.24020 152 066L 2 0 0.42383 0.43828 0.44287 0.45984 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.2058 0.21340	146	717R	1	Č	0.22255	0.24530	0.27317	0.27539
117 0.02L 2 0 0.10111 0.10335 0.11010 0.11010 148 010L 2 3 0.43068 0.43290 0.43238 0.41812 149 026L 2 1 0.30743 0.30052 0.30827 0.30470 150 029L 2 0 0.40198 0.45933 0.48630 0.54338 151 065L 2 1 0.21395 0.20592 0.22059 0.24020 152 066L 2 0 0.42383 0.43828 0.44287 0.45984 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	147	0021	2	0	0 40474	0.40955	0.41010	0.41360
149 026L 2 1 0.30743 0.30052 0.30827 0.30470 150 029L 2 0 0.40198 0.45933 0.48630 0.54338 151 065L 2 1 0.21395 0.20592 0.22059 0.24020 152 066L 2 0 0.42383 0.43828 0.44287 0.45984 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	148	010L	2	3	0.43068	0.43290	0.43238	0.41812
150 029L 2 0 0.40198 0.45933 0.48630 0.54338 151 065L 2 1 0.21395 0.20592 0.22059 0.24020 152 066L 2 0 0.42383 0.43828 0.44287 0.45984 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	149	026L	2	1	0.30743	0.30052	0.30827	0.30470
150 0252 2 0 0.10176 0.10175 0.10555 0.10555 151 065L 2 1 0.21395 0.20592 0.22059 0.24020 152 066L 2 0 0.42383 0.43828 0.44287 0.45984 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	150	0201	2	0	0.40198	0.45933	0.48630	0.54338
151 0.000 2 1 0.000 0.000 0.000 0.000 0.000 152 066L 2 0 0.42383 0.43828 0.44287 0.45984 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	151	0651	2	1	0.21395	0.20592	0.22059	0.24020
152 0001 2 0 0.42505 0.45026 0.44267 0.45704 153 189L 2 1 0.25435 0.24053 0.25728 0.25038 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	152	0661	2	0	0.42383	0.43828	0.44287	0 45984
155 1052 2 1 0.25455 0.24055 0.25726 0.25056 154 208L 2 3 0.31454 0.24920 0.23135 0.18305 155 214R 2 C 0.24250 0.20494 0.20058 0.21340	152	1891	2	1	0 25435	0.24053	0 25728	0.25038
155 214R 2 C 0.24250 0.20494 0.20058 0.21340	154	2081	2	3	0 31454	0 24920	0.23135	0 18305
	155	214R	2	č	0.24250	0.20494	0.20058	0.21340

Table A.1: LOOCV results for Gaussian curvature analysis (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
156	216L	2	1	0.25352	0.23775	0.24587	0.27090
157	219R	2	1	0.22435	0.18489	0.19146	0.19079
158	506L	2	3	0.29393	0.24526	0.23690	0.22739
159	509L	2	3	0.32725	0.29854	0.29347	0.29334
160	518L	2	3	0.30804	0.26433	0.26413	0.26308
161	518R	2	3	0.28040	0.21581	0.19629	0.17232
162	520L	2	3	0.26525	0.22087	0.20796	0.19904
163	520R	2	С	0.27034	0.22333	0.22015	0.23021
164	522L	2	3	0.24657	0.20565	0.20988	0.19253
165	525L	2	3	0.32373	0.25450	0.23767	0.20165
166	526R	2	3	0.26309	0.21252	0.19573	0.18817
167	530R	2	3	0.26459	0.22802	0.21010	0.19419
168	532L	2	1	0.21792	0.16882	0.18083	0.19046
169	532R	2	3	0.31381	0.24645	0.23819	0.19971
170	533L	2	3	0.28737	0.22928	0.21295	0.20745
171	533R	2	3	0.31562	0.26557	0.25893	0.24981
172	536L	2	1	0.26479	0.23912	0.25175	0.26095
173	536R	2	3	0.29095	0.23886	0.24026	0.22283
174	537R	2	1	0.22582	0.18231	0.18721	0 19324
175	5391	2	1	0.24586	0.20693	0.20759	0.22180
176	546L	2	1	0.23657	0.21161	0.21945	0.23763
177	546R	2	1	0.22645	0 19158	0 19704	0.19668
178	689R	2	3	0.22013	0.23762	0.23850	0.20754
179	692L	2	3	0.29620	0.23762	0.22690	0.23191
180	694I	2	3	0.25620	0.22306	0.22549	0.22212
181	701R	2	3	0.30270	0.22300	0.22549	0.17443
182	177I	2	C S	0.25729	0.23371	0.18725	0.17570
183	177R	3	C	0.32818	0.26673	0.25909	0.20382
18/	206I	3	C C	0.32612	0.26053	0.23300	0.10633
185	200L 207R	3	2	0.27965	0.20000	0.22802	0.22893
186	207K 212I	3	Č	0.27905	0.24250	0.22802	0.18302
187	212L 215I	3	C	0.27519	0.24239	0.19303	0.15362
188	215E 215E	3	C C	0.27319	0.21115	0.17884	0.13302
180	513I	3	C C	0.20027	0.23768	0.17004	0.17753
109	513D	3	C	0.23927	0.23708	0.21212	0.17755
190	510I	3	2	0.33443	0.26437	0.23087	0.24472
191	510D	3	2	0.24047	0.22555	0.21939	0.22027
192	526I	2	ſ	0.20825	0.17987	0.16571	0.18941
195	520L	2	C	0.29132	0.24139	0.21300	0.10041
194	524D	2	C	0.27449	0.22402	0.20702	0.19080
195	5201	2	C	0.27033	0.22740	0.20558	0.10932
190	520D	2	C	0.27088	0.21258	0.19998	0.19880
197	530K	2	C	0.24470	0.17460	0.10/31	0.10/40
198	547L	2	C	0.30102	0.24496	0.23037	0.21473
199	54/K	3	C	0.50152	0.24089	0.211/3	0.17029
200	549K	3	C	0.23815	0.18249	0.10880	0.14300
201	02K	3	C	0.34331	0.29481	0.20841	0.21338
202	697L	3	C	0.40985	0.35370	0.32872	0.27043
203	712L	3	С	0.28228	0.22778	0.21265	0.19510

Table A.1: LOOCV results for Gaussian curvature analysis (continuted).

A.2 LOOCV Results for Coronal Projection Analysis

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1	003L	0	2	0.28086	0.28439	0.25920	0.32155
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	003R	0	1	0.33514	0.31113	0.34970	0.36781
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	005R	0	1	0.24242	0.21696	0.22325	0.22788
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4	007L	0	1	0.22502	0.21643	0.22076	0.25810
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5	007R	0	С	0.21799	0.22162	0.23072	0.25367
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6	008R	0	С	0.32382	0.32547	0.34115	0.38194
8 013R 0 1 0.22203 0.21448 0.24455 0.26029 9 016R 0 C 0.32814 0.34039 0.35061 0.37993 10 025L 0 C 0.3490 0.34688 0.34538 0.40852 11 029R 0 C 0.24596 0.26042 0.28721 0.32329 12 037R 0 1 0.35607 0.33013 0.35703 0.36682 14 046L 0 2 0.25394 0.26263 0.24311 0.29939 15 046R 0 1 0.26213 0.25521 0.28456 0.3333 16 049L 0 2 0.28726 0.29421 0.26560 0.33699 18 053R 0 C 0.24772 0.26949 0.26504 0.32110 20 055R 0 C 0.24783 0.26653 0.29939 0.34627 21 067R	7	009L	0	С	0.24479	0.27100	0.26864	0.31855
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	8	013R	0	1	0.22203	0.21448	0.24455	0.26029
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	9	016R	0	С	0.32814	0.34039	0.35061	0.37993
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	025L	0	С	0.31490	0.34688	0.34538	0.40852
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	029R	0	С	0.24596	0.26042	0.28721	0.32329
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	037L	0	2	0.31360	0.30858	0.27402	0.32656
14046L02 0.25394 0.26263 0.24311 0.29939 15046R01 0.26213 0.25521 0.28845 0.30333 16049L02 0.28726 0.29742 0.26956 0.33768 17053L0C 0.26766 0.30411 0.29630 0.36990 18053R0C 0.26989 0.30212 0.32394 0.37937 19055L0C 0.24572 0.26649 0.26504 0.32110 20055R0C 0.147836 0.19622 0.22319 0.27701 22073R01 0.44296 0.42542 0.45640 0.46221 23076L0C 0.29375 0.42060 0.42292 0.47830 24078L0C 0.29376 0.27539 0.31981 0.33398 26084L02 0.22150 0.23242 0.21114 0.26703 27084R01 0.19840 0.19524 0.21982 0.23212 28088R0C 0.24550 0.28162 0.27299 0.34955 31096L02 0.26533 0.27293 0.22728 0.32874 30093L0C 0.24550 0.28162 0.22729 0.34955 31096L02 0.25838 0.27293 0.22728 0.31636 33131R0 <td>13</td> <td>037R</td> <td>0</td> <td>1</td> <td>0.35607</td> <td>0.33013</td> <td>0.35703</td> <td>0.36682</td>	13	037R	0	1	0.35607	0.33013	0.35703	0.36682
15 $046R$ 01 0.26213 0.25521 0.28845 0.30333 16 $049L$ 02 0.28726 0.29742 0.26956 0.33768 17 $053L$ 0C 0.27676 0.30441 0.29630 0.37937 18 $053R$ 0C 0.24989 0.30212 0.32394 0.37937 19 $055L$ 0C 0.24572 0.26949 0.26504 0.32110 20 $055R$ 0C 0.24783 0.26653 0.29939 0.34627 21 $067R$ 0C 0.17856 0.19622 0.22319 0.77701 22 $073R$ 01 0.44296 0.42542 0.45640 0.46221 23 $076L$ 0C 0.29280 0.31764 0.31921 0.37313 25 $079R$ 01 0.29376 0.27539 0.31981 0.33398 26 $084L$ 02 0.22150 0.23242 0.21982 0.25266 28 $088R$ 0C 0.24550 0.28162 0.27299 0.34955 31 $096L$ 02 0.26523 0.27278 0.31603 32 $113R$ 01 0.23313 0.31859 0.36156 0.38452 34 $135R$ 01 0.27311 0.22465 0.24904 33 $131R$ 01 0.27311 0.22465 0.24904 34 $135R$ 01 0.27	14	046L	0	2	0.25394	0.26263	0.24311	0.29939
16049L020.287260.297420.269560.3376817053L0C0.276760.304410.296300.3699018033R0C0.269890.302120.323940.3793719055L0C0.245720.269490.265040.3211020055R0C0.247830.266530.299390.3462721067R0C0.178560.196220.223190.2770122073R010.442960.425420.456400.4622123076L0C0.292800.317640.319210.3731325079R010.293760.275390.319810.3339826084L020.221500.232420.211140.2670327084R010.198400.195240.219820.2526628088R0C0.241500.281620.272990.3495531096L020.265230.279230.257280.3160332113R010.302130.318590.361560.3845234135R010.317270.311180.355490.3798635154R010.2273110.262640.307300.3384136160L020.248380.244710.220510.2676237175L02 <td>15</td> <td>046R</td> <td>0</td> <td>1</td> <td>0.26213</td> <td>0.25521</td> <td>0.28845</td> <td>0.30333</td>	15	046R	0	1	0.26213	0.25521	0.28845	0.30333
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16	049L	0	2	0.28726	0.29742	0.26956	0.33768
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17	053L	0	С	0.27676	0.30441	0.29630	0.36990
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	053R	0	C	0.26989	0.30212	0.32394	0.37937
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	0551	Õ	Ċ	0.24572	0.26949	0.26504	0.32110
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	055R	Ő	C	0.24783	0.26653	0.29939	0.34627
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	067R	Ő	C	0.17856	0.19622	0.22319	0.27701
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	073R	Ő	1	0.44296	0.42542	0.45640	0.46221
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	23	0761	Ő	Ċ	0.39375	0.42060	0.42292	0.47830
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	23	0781	0	C	0.29280	0.31764	0.31921	0.37313
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	070E	0	1	0.29276	0.27539	0.31921	0.33398
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	0841	0	2	0.22150	0.23242	0.21114	0.26703
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	084R	0	1	0.19840	0.19524	0.21114	0.25766
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	27	0880	0	ſ	0.24116	0.24626	0.28521	0.32312
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	0800	0	1	0.33426	0.24020	0.34070	0.32874
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	30	0031	0	C I	0.24550	0.28162	0.27299	0.34955
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	31	0961	0	2	0.24530	0.27923	0.25728	0.31603
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32	113P	0	1	0.20525	0.10730	0.22465	0.24904
33 131R 0 1 0.32313 0.31033 0.30130 0.30130 34 135R 0 1 0.31727 0.31118 0.35549 0.37986 35 154R 0 1 0.27311 0.26224 0.30730 0.33841 36 160L 0 2 0.25838 0.24471 0.22051 0.26762 37 175L 0 2 0.24694 0.26594 0.24490 0.30665 38 183L 0 C 0.29717 0.32242 0.32054 0.38887 39 186R 0 C 0.20570 0.22666 0.25687 0.30085 40 188R 0 1 0.22134 0.19729 0.22972 0.23588 41 192L 0 C 0.24237 0.25799 0.24282 0.29337 42 200L 0 2 0.38789 0.39301 0.37638 0.42234 43 201R 0 1 0.43631 0.41716 0.43954 0.44326 44	32	131R	0	1	0.32313	0.19750	0.22405	0.38452
34 153R 0 1 0.31727 0.31116 0.35349 0.31780 35 154R 0 1 0.27311 0.26224 0.30730 0.33841 36 160L 0 2 0.25838 0.24471 0.22051 0.26762 37 175L 0 2 0.24694 0.26594 0.24490 0.30665 38 183L 0 C 0.29717 0.32242 0.32054 0.38887 39 186R 0 C 0.20570 0.22666 0.25687 0.30085 40 188R 0 1 0.22134 0.19729 0.22972 0.23588 41 192L 0 C 0.24237 0.25799 0.24282 0.29337 42 200L 0 2 0.38473 0.39224 0.37850 0.41708 43 201R 0 1 0.43631 0.41716 0.43954 0.44326 44 203L 0 2 0.24885 0.25013 0.22121 0.26180 45	34	135R	0	1	0.31727	0.31118	0.35549	0.37986
33 134k 0 1 0.27311 0.20224 0.3030 0.30441 36 160L 0 2 0.25838 0.24471 0.22051 0.26762 37 175L 0 2 0.24694 0.26594 0.24490 0.30665 38 183L 0 C 0.29717 0.32242 0.32054 0.38887 39 186R 0 C 0.20570 0.22666 0.25687 0.30085 40 188R 0 1 0.22134 0.19729 0.22972 0.23588 41 192L 0 C 0.24237 0.25799 0.24282 0.29337 42 200L 0 2 0.38473 0.39224 0.37850 0.41708 43 201R 0 1 0.43631 0.41716 0.43954 0.44326 44 203L 0 2 0.24885 0.25013 0.22121 0.26180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47<	35	154D	0	1	0.31727	0.26224	0.33349	0.37980
30 100L 0 2 0.23536 0.24471 0.22051 0.24072 37 175L 0 2 0.24694 0.26594 0.24490 0.30665 38 183L 0 C 0.29717 0.32242 0.32054 0.38887 39 186R 0 C 0.20570 0.22666 0.25687 0.30085 40 188R 0 1 0.22134 0.19729 0.22972 0.23588 41 192L 0 C 0.24237 0.25799 0.24282 0.29337 42 200L 0 2 0.38473 0.39224 0.37850 0.41708 43 201R 0 1 0.43631 0.41716 0.43954 0.44326 44 203L 0 2 0.38789 0.39301 0.37638 0.42234 45 204L 0 2 0.24885 0.25013 0.22121 0.26180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47	36	154K 160I	0	1	0.25838	0.20224	0.22051	0.26762
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	37	1751	0	2	0.23638	0.24471	0.22051	0.20702
38 183L 0 C 0.29717 0.32242 0.32034 0.38887 39 186R 0 C 0.20570 0.22666 0.25687 0.30085 40 188R 0 1 0.22134 0.19729 0.22972 0.23588 41 192L 0 C 0.24237 0.25799 0.24282 0.29337 42 200L 0 2 0.38473 0.39224 0.37850 0.41708 43 201R 0 1 0.43631 0.41716 0.43954 0.44326 44 203L 0 2 0.38789 0.39301 0.37638 0.42234 45 204L 0 2 0.24885 0.25013 0.22121 0.26180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47 205R 0 1 0.24846 0.22889 0.25989 0.28707 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	39	1831	0		0.24094	0.20394	0.24490	0.30005
39180R0C 0.20370 0.22000 0.23087 0.50085 40 188R01 0.22134 0.19729 0.22972 0.23588 41 192L0C 0.24237 0.25799 0.24282 0.29337 42 200L02 0.38473 0.39224 0.37850 0.41708 43 201R01 0.43631 0.41716 0.43954 0.44326 44 203L02 0.38789 0.39301 0.37638 0.42234 45 204L02 0.24885 0.25013 0.22121 0.26180 46 205L02 0.24300 0.25542 0.23767 0.30016 47 205R01 0.24846 0.22889 0.25989 0.28707 48 211R01 0.34600 0.31603 0.32949 0.33692	30	185L	0	C	0.29717	0.32242	0.32034	0.38887
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	39 40	100K	0		0.20370	0.22000	0.23087	0.30083
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	40	100K	0	ſ	0.22134	0.19729	0.22972	0.23388
42 200L 0 2 0.38473 0.39224 0.3730 0.41708 43 201R 0 1 0.43631 0.41716 0.43954 0.44326 44 203L 0 2 0.38789 0.39301 0.37638 0.42234 45 204L 0 2 0.24885 0.25013 0.22121 0.26180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47 205R 0 1 0.24846 0.22889 0.25989 0.28707 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	41	192L 2001	0	C 2	0.24257	0.23799	0.24282	0.29557
43 201K 0 1 0.43031 0.41710 0.43934 0.44320 44 203L 0 2 0.38789 0.39301 0.37638 0.42234 45 204L 0 2 0.24885 0.25013 0.22121 0.26180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47 205R 0 1 0.24846 0.22889 0.25989 0.28707 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	42	200L 201D	0	2	0.36473	0.39224	0.37830	0.41708
44 205L 0 2 0.38789 0.39501 0.57038 0.42234 45 204L 0 2 0.24885 0.25013 0.22121 0.26180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47 205R 0 1 0.24846 0.22889 0.25989 0.28707 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	43 44	201K 2021	0	1	0.43031	0.41/10	0.43934	0.44520
45 204L 0 2 0.24685 0.25015 0.22121 0.20180 46 205L 0 2 0.24300 0.25542 0.23767 0.30016 47 205R 0 1 0.24846 0.22889 0.25989 0.28707 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	44 15	203L 2041	0	2	0.30/09	0.39301	0.37038	0.42234
40 203L 0 2 0.24300 0.25542 0.25767 0.30016 47 205R 0 1 0.24846 0.22889 0.25989 0.28707 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	4J 46	204L	0	2	0.24000	0.23013	0.22121	0.20160
47 203K 0 1 0.24846 0.22889 0.25989 0.28/07 48 211R 0 1 0.34600 0.31603 0.32949 0.33692	40	205D	0	2 1	0.24300	0.23342	0.23/0/	0.30010
40 ZIIK U I U.34000 U.31003 U.32949 U.33692	4/	205K	0	1	0.24840	0.22889	0.23989	0.28/07
40 2171 0 2 0.22215 0.22010 0.20244 0.2207	48	211K	0	1	0.34600	0.31003	0.32949	0.33092
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	49	21/L	0	2 C	0.32315	0.32010	0.29344	0.33970
50 220L 0 C 0.25287 0.24105 0.24075 0.28240	50	220L	0		0.23287	0.24103	0.24075	0.28240

Table A.2: LOOCV results for coronal projection analysis.

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
52	505L	0	С	0.32317	0.33844	0.32506	0.38423
53	505R	0	С	0.21846	0.23640	0.27092	0.31477
54	508R	0	1	0.22887	0.19400	0.21724	0.21221
55	511L	0	2	0.27978	0.26842	0.23985	0.25410
56	523L	0	2	0.26159	0.26803	0.23495	0.30105
57	528R	0	С	0.24703	0.24897	0.25697	0.29199
58	529L	0	С	0.24719	0.27896	0.27012	0.34938
59	529R	0	С	0.20489	0.23472	0.25887	0.31725
60	535L	0	2	0.32675	0.32926	0.30070	0.35562
61	535R	0	1	0.24428	0.21377	0.23537	0.24278
62	542L	0	2	0.26189	0.26812	0.24027	0.28154
63	542R	0	С	0.22516	0.23048	0.22830	0.27530
64	554L	0	2	0.26319	0.26216	0.24876	0.29894
65	554R	0	1	0.20857	0.18984	0.21376	0.21292
66	700R	0	2	0.20695	0.18858	0.18463	0.20137
67	702L	0	2	0.24747	0.25772	0.23559	0.28825
68	702R	0	2	0.21681	0.21015	0.19978	0.22245
69	704R	0	1	0.20812	0.17519	0.20549	0.21471
70	705L	0	2	0.24122	0.21871	0.19146	0.21031
71	710L	0	2	0.23095	0.21500	0.18634	0.20098
72	006L	1	2	0.19745	0.20183	0.18682	0.24161
73	012L	1	2	0.24314	0.24130	0.21528	0.26197
74	012R	1	С	0.22559	0.20003	0.22728	0.23639
75	018L	1	2	0.34892	0.36863	0.34067	0.39808
76	018R	1	С	0.31824	0.31258	0.33773	0.35382
77	022L	1	2	0.34737	0.36318	0.34221	0.40541
78	022R	1	0	0.24860	0.26482	0.28890	0.33734
79	023L	1	2	0.36278	0.38352	0.35565	0.41839
80	023R	1	С	0.38418	0.37496	0.41095	0.42263
81	027R	1	3	0.30901	0.25967	0.26712	0.21245
82	047L	1	2	0.37979	0.37800	0.35963	0.38821
83	047R	1	С	0.33986	0.33188	0.36748	0.39257
84	049R	1	С	0.26801	0.26243	0.29819	0.31934
85	056L	1	2	0.20209	0.20482	0.18038	0.24056
86	057R	1	С	0.25413	0.21608	0.23854	0.23371
87	060L	1	2	0.21162	0.21451	0.19617	0.24128
88	069R	1	С	0.34921	0.33355	0.36413	0.37959
89	070R	1	С	0.24639	0.21802	0.25235	0.25381
90	075R	1	С	0.23346	0.20087	0.22644	0.22623
91	082L	1	0	0.19505	0.21276	0.19965	0.24446
92	086L	1	2	0.28036	0.28626	0.25660	0.30964
93	094R	1	С	0.25115	0.24128	0.27188	0.29533
94	095R	1	С	0.37234	0.34866	0.37549	0.35657
95	098R	1	С	0.29082	0.26533	0.29533	0.27846
96	124R	1	С	0.31915	0.31504	0.35795	0.37648
97	133L	1	2	0.30893	0.30580	0.26533	0.30999
98	133R	1	С	0.28301	0.26577	0.27610	0.28204
99	163R	1	C	0.31284	0.29222	0.32592	0.32287
100	181L	1	0	0.22179	0.24898	0.23639	0.28925
101	184L	1	0	0.20353	0.22887	0.22299	0.27715
102	190L	1	2	0.23679	0.23195	0.20770	0.23107
103	197R	1	C	0.22832	0.20445	0.23572	0.24149
104	199L	1	2	0.23241	0.23588	0.20756	0.24155
105	200R	1	C	0.24099	0.20771	0.21988	0.23136
106	203R	1	2	0.55883	0.55673	0.55258	0.57444

Table A.2: LOOCV results for coronal projection analysis (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
107	204R	1	С	0.27161	0.24118	0.25680	0.25940
108	209R	1	3	0.23929	0.20219	0.20694	0.18891
109	210L	1	2	0.26898	0.24140	0.19935	0.19971
110	219L	1	2	0.25004	0.25772	0.23339	0.25626
111	507L	1	2	0.23235	0.21175	0.17066	0.19654
112	507R	1	С	0.24234	0.20512	0.21999	0.21594
113	509R	1	С	0.25562	0.22636	0.24390	0.25356
114	511R	1	С	0.21763	0.17643	0.18393	0.18087
115	512R	1	С	0.19852	0.18380	0.21527	0.23104
116	514L	1	2	0.24297	0.24775	0.22584	0.28544
117	515L	1	2	0.18930	0.18156	0.15271	0.18831
118	515R	1	С	0.21811	0.18043	0.20271	0.18689
119	516L	1	2	0.29719	0.28651	0.24374	0.27136
120	516R	1	С	0.25784	0.22311	0.24297	0.24154
121	517L	1	2	0.32981	0.32642	0.29699	0.32648
122	517R	1	С	0.22423	0.18929	0.20083	0.20342
123	521L	1	2	0.27068	0.27385	0.24407	0.30153
124	522R	1	С	0.23089	0.19827	0.21322	0.22996
125	523R	1	3	0.23350	0.19193	0.19580	0.18148
126	527L	1	2	0.34200	0.34476	0.32551	0.36378
127	527R	1	С	0.24030	0.21627	0.23207	0.25688
128	534L	1	2	0.43163	0.42075	0.40211	0.41239
129	539R	1	С	0.25889	0.23688	0.26034	0.25645
130	540L	1	2	0.21779	0.20317	0.18427	0.19182
131	541L	1	2	0.40456	0.40632	0.37313	0.40555
132	541R	1	С	0.23000	0.20074	0.21694	0.22215
133	543L	1	2	0.21939	0.21194	0.17260	0.22193
134	543R	1	С	0.22622	0.19944	0.21432	0.21016
135	574R	1	3	0.24496	0.22940	0.23177	0.21476
136	691L	1	2	0.26837	0.28096	0.25662	0.32155
137	691R	1	2	0.22643	0.21899	0.21607	0.24683
138	699R	1	С	0.18119	0.15832	0.17204	0.17910
139	700L	1	2	0.21302	0.20543	0.17332	0.19520
140	703R	1	С	0.26571	0.22884	0.24952	0.24286
141	704L	1	2	0.25693	0.25751	0.21925	0.27642
142	710R	1	С	0.23030	0.20112	0.21922	0.22196
143	711L	1	2	0.26791	0.25516	0.22992	0.25516
144	713L	1	2	0.26600	0.26958	0.23724	0.29337
145	713R	1	С	0.27683	0.24063	0.26589	0.26204
146	717R	1	С	0.20446	0.19254	0.20303	0.22407
147	002L	2	С	0.32194	0.30172	0.26795	0.28798
148	010L	2	3	0.42424	0.40086	0.37986	0.37099
149	026L	2	С	0.37841	0.37131	0.36196	0.37781
150	029L	2	0	0.40317	0.44295	0.47490	0.52342
151	065L	2	С	0.27996	0.27294	0.25190	0.29140
152	066L	2	С	0.24080	0.24369	0.22503	0.27253
153	189L	2	С	0.23295	0.21134	0.20870	0.22220
154	208L	2	С	0.36664	0.34942	0.32248	0.33377
155	214R	2	1	0.24106	0.21255	0.24496	0.23640
156	216L	2	С	0.23993	0.23914	0.22565	0.27907
157	219R	2	3	0.26933	0.24391	0.26548	0.24217
158	506L	2	С	0.24925	0.24591	0.22117	0.26169
159	509L	2	С	0.23581	0.22883	0.20439	0.24114
160	518L	2	С	0.22911	0.22268	0.19729	0.21184
161	518R	2	3	0.22723	0.20267	0.18545	0.17703

Table A.2: LOOCV results for coronal projection analysis (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
162	520L	2	С	0.19537	0.18208	0.15387	0.18198
163	520R	2	1	0.24277	0.21660	0.22586	0.22856
164	522L	2	С	0.32899	0.31477	0.28734	0.31180
165	525L	2	3	0.29223	0.26556	0.23503	0.21834
166	526R	2	1	0.22360	0.17785	0.20423	0.18148
167	530R	2	1	0.31696	0.28700	0.30466	0.30091
168	532L	2	С	0.24446	0.23309	0.21162	0.22064
169	532R	2	3	0.29263	0.24451	0.24054	0.18731
170	533L	2	С	0.33257	0.31987	0.29529	0.32533
171	533R	2	3	0.27369	0.23694	0.25852	0.22984
172	536L	2	С	0.33485	0.33194	0.31178	0.35498
173	536R	2	1	0.27612	0.24001	0.25203	0.25520
174	537R	2	1	0.25468	0.21539	0.24321	0.24251
175	539L	2	С	0.21968	0.21581	0.18953	0.21732
176	546L	2	С	0.23064	0.23327	0.21240	0.25459
177	546R	2	1	0.22140	0.19761	0.21532	0.21955
178	689R	2	3	0.27471	0.23349	0.25797	0.23143
179	692L	2	С	0.38743	0.38623	0.38027	0.39683
180	694L	2	С	0.25253	0.24003	0.20935	0.21795
181	701R	2	3	0.34985	0.31102	0.32918	0.28647
182	177L	3	2	0.26895	0.24086	0.19675	0.21335
183	177R	3	С	0.36423	0.31984	0.31964	0.28488
184	206L	3	С	0.48563	0.46195	0.44714	0.44621
185	207R	3	1	0.29138	0.26867	0.28054	0.27936
186	212L	3	2	0.29769	0.26833	0.22672	0.23335
187	215L	3	2	0.29228	0.26047	0.21920	0.22737
188	215R	3	С	0.28942	0.23183	0.23340	0.18641
189	513L	3	2	0.27785	0.24903	0.21570	0.21809
190	513R	3	С	0.31024	0.26350	0.25735	0.22741
191	519L	3	2	0.25724	0.24101	0.21215	0.21871
192	519R	3	С	0.25903	0.21926	0.22186	0.20347
193	526L	3	2	0.25082	0.22155	0.18175	0.20186
194	52R	3	1	0.29574	0.26725	0.26729	0.27131
195	534R	3	С	0.27871	0.23297	0.23783	0.20117
196	538L	3	2	0.25154	0.22895	0.18967	0.19251
197	538R	3	С	0.21133	0.17354	0.17808	0.16782
198	547L	3	2	0.27061	0.25129	0.22003	0.23233
199	547R	3	С	0.35153	0.30134	0.30382	0.26768
200	549R	3	С	0.27608	0.23470	0.23291	0.19690
201	62R	3	С	0.44000	0.39975	0.39348	0.35983
202	697L	3	С	0.39748	0.35245	0.31675	0.27644
203	712L	3	С	0.28184	0.25145	0.21181	0.18948

Table A.2: LOOCV results for coronal projection analysis (continuted).

A.3 LOOCV Results for the Y Component of the Surface Normal Analysis

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
1	003L	0	С	0.16513	0.18213	0.23739	0.30616
2	003R	0	С	0.19166	0.21855	0.28977	0.34729
3	005R	0	1	0.21654	0.19892	0.26120	0.29890
4	007L	0	С	0.29267	0.31553	0.32867	0.34625
5	007R	0	С	0.22674	0.25396	0.28688	0.31262
6	008R	0	С	0.34969	0.39963	0.42292	0.45092
7	009L	0	С	0.22689	0.26704	0.29365	0.36929
8	013R	0	С	0.17925	0.20367	0.27009	0.32077
9	016R	0	С	0.38761	0.43259	0.45181	0.47000
10	025L	0	С	0.32556	0.38047	0.40980	0.45849
11	029R	0	С	0.35274	0.35279	0.38657	0.45510
12	037L	0	С	0.25551	0.25746	0.27665	0.32360
13	037R	0	С	0.25902	0.27911	0.31897	0.35121
14	046L	0	С	0.21209	0.22944	0.25437	0.30176
15	046R	0	С	0.18171	0.21991	0.28179	0.33002
16	049L	0	С	0.22899	0.25418	0.30300	0.36405
17	053L	0	С	0.27641	0.32409	0.36794	0.42697
18	053R	0	С	0.26289	0.32623	0.36647	0.41650
19	055L	0	С	0.21455	0.27056	0.30893	0.36829
20	055R	0	С	0.26546	0.32799	0.37505	0.41714
21	067R	0	С	0.21204	0.26200	0.31553	0.35916
22	073R	0	С	0.37273	0.41881	0.44350	0.46784
23	076L	0	Č	0.35515	0.38810	0.41985	0.49728
24	078L	0	C	0.35506	0.37553	0.40170	0.46980
25	079R	0	Č	0.21584	0.21904	0.27133	0.31473
26	084L	0	Ċ	0.24917	0.28892	0.33162	0.38287
27	084R	Õ	C	0.23525	0.26556	0.32269	0.38104
28	088R	Õ	C	0.24234	0.28178	0.35107	0.41088
29	089R	Õ	C	0.20436	0.20753	0.25923	0.30090
30	093L	0	Č	0.22647	0.26816	0.31556	0.38814
31	096L	0	Ċ	0.24560	0.24890	0.26914	0.32092
32	113R	Õ	C	0.20386	0.21217	0.27338	0.33210
33	131R	0	Č	0.22895	0.27323	0.32601	0.38513
34	135R	0	Č	0.28089	0.31320	0.38117	0.44001
35	154R	Õ	Č	0.19246	0.21487	0.28760	0 34928
36	160L	Õ	2	0.28753	0.26630	0.25374	0.31625
37	175L	Õ	Ē	0.17570	0.21647	0.24127	0.30740
38	183L	Õ	C	0.27301	0.32309	0.35571	0.40579
39	186R	Õ	C	0.16894	0.18342	0.22537	0.28337
40	188R	Õ	Č	0.22569	0.24715	0 29539	0 32409
41	192L	Ő	2	0.31481	0.31634	0.30914	0.36935
42	200L	Ő	Ē	0.29095	0.31575	0 31964	0.33986
43	200E	Ő	Č	0.23085	0.26917	0.30298	0.33406
44	2031	0	Č	0.30279	0.31516	0 32780	0 34993
45	2031	0	C	0 19353	0 20033	0.22175	0.26994
46	2051	0	C	0.25536	0.26920	0 31208	0.26727
40 47	205E 205R	0	C	0.223550	0.20920	0.31460	0.35403
48	2051	0	C	0.22450	0.27071	0.28855	0 32240
49	2171	0	2	0.26167	0.24072	0.20895	0.21864
• •			-	0.2010/	0.2.072	0.20000	0.21001

Table A.3: LOOCV results for surface normal analysis.

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
50	220L	0	1	0.36498	0.35531	0.37229	0.43640
51	220R	0	С	0.18457	0.21449	0.26814	0.33683
52	505L	0	С	0.25069	0.28536	0.31075	0.35446
53	505R	0	С	0.21581	0.24922	0.30193	0.36772
54	508R	0	1	0.23589	0.21097	0.27119	0.30735
55	511L	0	1	0.31294	0.29469	0.30726	0.35611
56	523L	0	С	0.21735	0.22497	0.26370	0.30850
57	528R	0	С	0.35993	0.37956	0.38292	0.38468
58	529L	0	С	0.22431	0.24340	0.29150	0.36399
59	529R	0	С	0.20706	0.22682	0.27657	0.32250
60	535L	0	С	0.22595	0.24799	0.27543	0.32396
61	535R	0	1	0.24781	0.23587	0.27964	0.32279
62	542L	0	С	0.29451	0.31842	0.32583	0.34248
63	542R	0	С	0.13243	0.15470	0.21575	0.27947
64	554L	0	2	0.22751	0.23250	0.21830	0.25704
65	554R	0	1	0.21261	0.20851	0.22237	0.27354
66	700R	0	1	0.20427	0.17955	0.23661	0.28741
67	702L	0	С	0.24081	0.26660	0.29051	0.32657
68	702R	0	С	0.21890	0.23493	0.29323	0.32854
69	704R	0	1	0.23472	0.22554	0.28661	0.33369
70	705L	0	1	0.22749	0.22189	0.25171	0.30142
71	710L	0	2	0.37262	0.34053	0.33244	0.37212
72	006L	1	0	0.22724	0.25010	0.27721	0.31163
73	012L	1	С	0.21190	0.18617	0.20418	0.25139
74	012R	1	С	0.21368	0.20735	0.26818	0.31052
75	018L	1	0	0.22895	0.26398	0.29601	0.34954
76	018R	1	0	0.32340	0.36965	0.38545	0.40548
77	022L	1	0	0.22554	0.26934	0.30996	0.36321
78	022R	1	0	0.26261	0.31457	0.36591	0.40104
79	023L	1	0	0.21353	0.25060	0.28420	0.33700
80	023R	1	0	0.23678	0.25579	0.31887	0.36004
81	027R	1	3	0.39302	0.32122	0.29790	0.26299
82	047L	1	2	0.35573	0.36904	0.34993	0.35224
83	047R	1	0	0.22581	0.26987	0.32019	0.36297
84	049R	1	0	0.25923	0.28873	0.35400	0.40059
85	056L	1	0	0.23281	0.26371	0.28813	0.31708
86	057R	1	С	0.20463	0.18671	0.21791	0.25843
87	060L	1	0	0.21165	0.21249	0.22662	0.29359
88	069R	1	0	0.19298	0.20286	0.25543	0.29171
89	070R	1	С	0.28980	0.24491	0.26308	0.30855
90	075R	1	С	0.27963	0.24645	0.25768	0.30193
91	082L	1	С	0.27977	0.26336	0.27498	0.32861
92	086L	1	0	0.25532	0.25995	0.25577	0.31214
93	094R	1	0	0.23047	0.27389	0.31379	0.34379
94	095R	1	0	0.40158	0.43194	0.42693	0.42683
95	098R	1	С	0.19806	0.18362	0.21778	0.25657
96	124R	1	0	0.22172	0.22684	0.28797	0.34530
97	133L	1	2	0.24257	0.23372	0.23187	0.24564
98	133R	1	3	0.36580	0.37615	0.37112	0.35846
99	163R	1	0	0.22457	0.24717	0.29367	0.33334
100	181L	1	0	0.19665	0.20689	0.24034	0.30718
101	184L	1	0	0.15934	0.18904	0.22393	0.28360
102	190L	1	2	0.19790	0.17040	0.15532	0.20400
103	197R	1	С	0.32918	0.27643	0.30359	0.33016
104	199L	1	С	0.23156	0.22100	0.23602	0.29230

Table A.3: LOOCV results for surface normal analysis (continuted).

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	105	200R	1	С	0.19930	0.18808	0.20231	0.23743
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	106	203R	1	С	0.24394	0.22550	0.26767	0.33240
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	107	204R	1	С	0.18589	0.18496	0.21525	0.24532
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	108	209R	1	2	0.43685	0.39841	0.37036	0.39507
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	109	210L	1	2	0.31027	0.26043	0.24187	0.24343
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	110	219L	1	С	0.22610	0.20849	0.22803	0.27443
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	111	507L	1	2	0.31593	0.28948	0.25502	0.29314
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	112	507R	1	С	0.30743	0.25605	0.25636	0.27107
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	113	509R	1	С	0.29451	0.25865	0.30144	0.31782
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	114	511R	1	С	0.22461	0.20105	0.24430	0.27554
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	115	512R	1	С	0.24566	0.21473	0.25931	0.31019
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	116	514L	1	0	0.22730	0.24864	0.26725	0.29750
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	117	515L	1	С	0.19426	0.18136	0.20634	0.25917
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	118	515R	1	С	0.21710	0.18298	0.22035	0.25273
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	119	516L	1	2	0.34341	0.31463	0.27928	0.30566
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	120	516R	1	С	0.31751	0.27860	0.29198	0.33049
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	121	517L	1	0	0.33086	0.33863	0.34036	0.34328
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	122	517R	1	Č	0.32181	0.27188	0.27930	0.31088
124522R1C0.196660.171120.197440.23187125523R1C0.317680.269030.270110.29624126527L100.331410.356560.359130.38275127527R1C0.219630.199520.246880.27702128534L130.363490.369480.354080.34748129539R1C0.291740.254600.291880.34401130540L130.352850.352420.340850.32920131541L100.307740.314350.313140.31900132541R1C0.328690.281200.284170.32126133543L120.278630.235860.213230.23267134543R120.317590.272310.270070.29543135574R100.255250.282520.304340.31718136691L1C0.236720.235710.254940.30870137691R100.290210.298090.318580.31795138699R1C0.170290.137270.161710.21322139700L1C0.185000.177310.188590.22741140703R1C0.254710.230300.260770.26960141704L <t< td=""><td>123</td><td>521L</td><td>1</td><td>C</td><td>0.24467</td><td>0.23904</td><td>0.25659</td><td>0.29645</td></t<>	123	521L	1	C	0.24467	0.23904	0.25659	0.29645
125523R1C0.317680.269030.270110.20624126527L100.331410.355660.359130.38275127527R1C0.219630.199520.246880.27702128534L130.363490.369480.354080.34748129539R1C0.291740.254600.291880.34401130540L130.352850.352420.340850.32920131541L100.007740.214350.213140.31900132541R1C0.328690.235860.213230.23267134543R120.278630.235860.213230.23267134543R120.236720.235710.270070.29543135574R100.255250.282520.304340.30870137691R100.290210.298090.318580.31795138699R1C0.170290.137270.161710.21332139700L1C0.254710.230330.260980.28169141704L100.252090.256340.286090.32782143711L120.272200.2663280.260700.26960144713R100.239870.246330.277790.31445145713R<	124	522R	1	Č	0.19666	0.17112	0 19744	0.23187
126527L100.331410.336560.130110.3227127527R1C0.219630.199520.246880.27702128534L130.363490.369480.354080.34748129539R1C0.291740.254600.291880.34401130540L130.352850.352420.340850.32920131541L100.307740.314350.313140.31900132541R120.278630.235860.284170.322671345438120.278630.235860.213230.232671345438120.236720.235710.274940.30870135574R100.255250.282520.304340.31718136691L1C0.170290.137270.161710.2132138699R1C0.170290.37770.161710.2132139700L1C0.25090.256340.28030.32770142710R1C0.35120.27180.26070.26960144713L100.225180.231980.282900.30583147002L230.461400.446070.445730.4236145713R100.225180.231980.262770.30583144717R1 <t< td=""><td>125</td><td>523R</td><td>1</td><td>Č</td><td>0.31768</td><td>0.26903</td><td>0.27011</td><td>0.29624</td></t<>	125	523R	1	Č	0.31768	0.26903	0.27011	0.29624
127527R1C0.219630.19330.021880.02702128534L130.363490.369480.354080.34748129539R1C0.291740.254600.291880.34401130540L130.352850.352420.340850.32920131541L100.307740.314350.313140.31900132541R1C0.328690.281200.284170.32126133543L120.278630.235860.213230.23267134543R120.317590.272310.270070.29543135574R100.255250.282520.304340.31718136691R1C0.236720.235710.254940.30870137691R100.290210.298090.318580.31795138699R1C0.170290.137270.161710.21332139700L1C0.254710.230300.260980.28169141704L100.252090.265340.286090.32770142710R1C0.315120.271260.286090.32782143711L120.271200.263280.262070.26960144703L100.239870.246930.225790.31445145713R <td< td=""><td>125</td><td>527L</td><td>1</td><td>0</td><td>0.33141</td><td>0.35656</td><td>0.35913</td><td>0.38275</td></td<>	125	527L	1	0	0.33141	0.35656	0.35913	0.38275
128534L13 0.36349 0.36948 0.35408 0.34748 129539R1C 0.29174 0.25460 0.29188 0.34401 130540L13 0.35285 0.35242 0.34085 0.32920 131541L10 0.30774 0.31435 0.31314 0.31900 132541R1C 0.32869 0.28120 0.28417 0.32126 133543L12 0.27863 0.23586 0.21323 0.23267 134543R12 0.31759 0.27231 0.27007 0.29543 135574R10 0.25525 0.28252 0.30434 0.31718 136691L1C 0.23672 0.23571 0.25494 0.30870 137691R10 0.29021 0.29809 0.31858 0.31795 138699R1C 0.17029 0.13727 0.16171 0.21332 139700L1C 0.25471 0.2303 0.26098 0.28169 141704L10 0.25209 0.26534 0.2809 0.32782 143711L12 0.27126 0.28609 0.32782 143711L12 0.27120 0.26328 0.26207 0.26960 144713R10 0.22518 0.23198 0.28290 0.30583 145713R1 <t< td=""><td>120</td><td>527E</td><td>1</td><td>Č</td><td>0.21963</td><td>0.19952</td><td>0.24688</td><td>0.27702</td></t<>	120	527E	1	Č	0.21963	0.19952	0.24688	0.27702
120539R1C0.291740.254600.291880.34401130540L130.352850.352420.340850.32920131541L100.307740.314350.313140.31900132541R1C0.328690.281200.284170.32126133543L120.278630.235860.213230.23267134543R120.317590.272310.270070.29543135574R100.255250.282520.304340.31718136691L1C0.236720.235710.254940.30870137691R100.290210.298090.318580.31795138699R1C0.170290.137270.161710.21332139700L1C0.185000.177310.188590.22741140703R1C0.252090.256340.288030.32770142710R1C0.315120.271260.286090.32782143711L120.272200.263280.262070.26960144713R100.239870.246930.275790.31445145713R100.225180.231980.282900.30593146717R100.195370.217810.267370.30583147002L <t< td=""><td>127</td><td>534L</td><td>1</td><td>3</td><td>0.36349</td><td>0.36948</td><td>0.35408</td><td>0.34748</td></t<>	127	534L	1	3	0.36349	0.36948	0.35408	0.34748
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	120	539R	1	Č	0.29174	0.25460	0.29188	0.34401
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	120	540I	1	3	0.35285	0.35242	0.34085	0.32920
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	131	541I	1	0	0.30774	0.31435	0.31314	0.31900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	132	541R	1	Č	0.32869	0.28120	0.28417	0.32126
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	132	5/3I	1	2	0.27863	0.23586	0.21323	0.23267
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	134	5/3R	1	2	0.31759	0.25580	0.21323	0.29543
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	135	574R	1	0	0.25525	0.28252	0.30434	0.31718
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	136	601I	1	Č	0.23525	0.23571	0 25494	0.30870
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	130	691R	1	0	0.29021	0.29809	0.31858	0.31795
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	138	600R	1	Č	0.17020	0.13727	0.16171	0.21332
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	130	700I	1	C	0.18500	0.17731	0.18859	0.21332
140 100 100 100 0.25209 0.25634 0.2803 0.32770 141 704 1 C 0.31512 0.27126 0.28609 0.32782 143 711 1 2 0.27220 0.26328 0.26207 0.26960 144 713 1 0 0.23987 0.24693 0.27579 0.31445 145 713 1 0 0.22518 0.23198 0.28290 0.30593 146 717 1 0 0.19537 0.21781 0.26737 0.30583 147 002 2 3 0.46140 0.44607 0.42444 0.37029 148 010 2 3 0.46140 0.44607 0.42444 0.37029 149 026 2 0 0.41846 0.43527 0.43304 0.42436 150 029 2 3 0.43981 0.45304 0.44573 0.24023 152 066 2 C 0.22606 0.20205 0.19730 0.24023 152 066 2 C 0.22808 0.23116 0.21735 0.21995 153 189 2 1 0.25979 0.21911 0.23716 0.26756 156 216 2 1 0.27100 0.24931 0.26025 0.31746 157 219 2 1 0.27100 0.24853 0.25065 0.25887 158 506 2	140	703R	1	C	0.16500	0.23303	0.26098	0.22741
141 $104L$ 1 0 0.25007 0.25007 0.25007 0.25007 0.25007 142 $710R$ 1 C 0.31512 0.27126 0.28609 0.32782 143 $711L$ 1 2 0.27220 0.26328 0.26207 0.26960 144 $713L$ 1 0 0.23987 0.24693 0.27579 0.31445 145 $713R$ 1 0 0.22518 0.23198 0.28290 0.30593 146 $717R$ 1 0 0.19537 0.21781 0.26737 0.30583 147 $002L$ 2 3 0.46140 0.44607 0.42444 0.37029 148 $010L$ 2 3 0.46140 0.44607 0.42444 0.37029 149 $026L$ 2 0 0.41846 0.43527 0.43304 0.42436 150 $029L$ 2 3 0.43981 0.45304 0.44573 0.42527 151 $065L$ 2 C 0.22606 0.20205 0.19730 0.24023 152 $066L$ 2 C 0.22808 0.23116 0.21735 0.21995 153 $189L$ 2 0 0.26676 0.26931 0.28009 0.28487 154 $208L$ 2 1 0.25979 0.21911 0.23716 0.26756 156 $216L$ 2 1 0.27100 0.24931 0.26025 0.31746	140	703K 704I	1	0	0.25209	0.25634	0.28803	0.32770
142 $110R$ 1 2 0.31312 0.27120 0.2200 0.26207 0.26960 144 $713L$ 1 0 0.23987 0.24693 0.27579 0.31445 145 $713R$ 1 0 0.22518 0.23198 0.28290 0.30593 146 $717R$ 1 0 0.19537 0.21781 0.26737 0.30583 147 $002L$ 2 3 0.46140 0.44607 0.42444 0.37029 148 $010L$ 2 3 0.46140 0.44607 0.42444 0.37029 149 $026L$ 2 0 0.41846 0.43527 0.43304 0.42436 150 $029L$ 2 3 0.43981 0.45304 0.44573 0.42527 151 $065L$ 2 C 0.22606 0.20205 0.19730 0.24023 152 $066L$ 2 C 0.22808 0.23116 0.21735 0.21995 153 $189L$ 2 0 0.26676 0.26931 0.28009 0.28487 154 $208L$ 2 3 0.43522 0.42527 0.41390 0.37992 155 $214R$ 2 1 0.25979 0.21911 0.26025 0.31746 157 $219R$ 2 1 0.27100 0.24931 0.26025 0.31746 158 $506L$ 2 1 0.272122 0.24853 0.25065 0.25887 159	142	710P	1	Č	0.31512	0.25054	0.28609	0.32782
143 1112 1 2 0.27220 0.2050 0.2050 0.2050 0.2050 144 $713L$ 1 0 0.23987 0.24693 0.27579 0.31445 145 $713R$ 1 0 0.22518 0.23198 0.28290 0.30593 146 $717R$ 1 0 0.19537 0.21781 0.26737 0.30583 147 $002L$ 2 3 0.34668 0.30930 0.29590 0.27668 148 $010L$ 2 3 0.46140 0.44607 0.42444 0.37029 149 $026L$ 2 0 0.41846 0.43527 0.43304 0.42436 150 $029L$ 2 3 0.43981 0.45304 0.44573 0.42527 151 $065L$ 2 C 0.22606 0.20205 0.19730 0.24023 152 $066L$ 2 C 0.22808 0.23116 0.21735 0.21995 153 $189L$ 2 0 0.26676 0.26931 0.28009 0.28487 154 $208L$ 2 3 0.43522 0.42527 0.41390 0.37992 155 $214R$ 2 1 0.25979 0.21911 0.26025 0.31746 156 $216L$ 2 1 0.27100 0.24931 0.26025 0.31746 157 $219R$ 2 1 0.272100 0.24853 0.25065 0.25887 159 <td>142</td> <td>711I</td> <td>1</td> <td>2</td> <td>0.27220</td> <td>0.26328</td> <td>0.26207</td> <td>0.26960</td>	142	711I	1	2	0.27220	0.26328	0.26207	0.26960
144 $112L$ 1 0 0.22518 0.24013 0.21517 0.51445 145 $713R$ 1 0 0.22518 0.23198 0.28290 0.30593 146 $717R$ 1 0 0.19537 0.21781 0.26737 0.30583 147 $002L$ 2 3 0.34668 0.30930 0.29590 0.27668 148 $010L$ 2 3 0.46140 0.44607 0.42444 0.37029 149 $026L$ 2 0 0.41846 0.43527 0.43304 0.42436 150 $029L$ 2 3 0.43981 0.45304 0.44573 0.42527 151 $065L$ 2 C 0.22606 0.20205 0.19730 0.24023 152 $066L$ 2 C 0.22808 0.23116 0.21735 0.21995 153 $189L$ 2 0 0.26676 0.26931 0.28009 0.28487 154 $208L$ 2 3 0.43522 0.42527 0.41390 0.37992 155 $214R$ 2 1 0.25979 0.21911 0.23716 0.26756 156 $216L$ 2 1 0.27100 0.24931 0.26025 0.31746 157 $219R$ 2 1 0.27232 0.24853 0.25065 0.25887 159 $509L$ 2 1 0.28348 0.26522 0.26959 0.31286	144	7131	1	0	0.23987	0.24693	0.27579	0.31445
115 115 115 115 0.2216 0.2216 0.2216 0.22736 0.20737 0.30583 146 $717R$ 10 0.19537 0.21781 0.26737 0.30583 147 $002L$ 23 0.34668 0.30930 0.29590 0.27668 148 $010L$ 23 0.46140 0.44607 0.42444 0.37029 149 $026L$ 20 0.41846 0.43527 0.43304 0.42436 150 $029L$ 23 0.43981 0.45304 0.44573 0.42527 151 $065L$ 2C 0.22606 0.20205 0.19730 0.24023 152 $066L$ 2C 0.22808 0.23116 0.21735 0.21995 153 $189L$ 20 0.26676 0.26931 0.28009 0.28487 154 $208L$ 23 0.43522 0.42527 0.41390 0.37992 155 $214R$ 21 0.25979 0.21911 0.23716 0.26756 156 $216L$ 21 0.27100 0.24931 0.26025 0.31746 157 $219R$ 21 0.27232 0.24853 0.25065 0.25887 159 $509L$ 21 0.28348 0.26522 0.26959 0.31286	145	713R	1	0	0.22518	0.23198	0.28290	0.30593
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	146	717R	1	0	0.19537	0.21781	0.26737	0.30583
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	147	0021	2	3	0.34668	0.30930	0.20797	0.27668
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	147	0101	2	3	0.46140	0.44607	0.42444	0.37029
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	140	0261	2	0	0.41846	0.43527	0.43304	0.42436
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	150	0201	2	3	0.43981	0.45304	0.44573	0.42527
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	151	0651	2	Č	0.22606	0.20205	0.19730	0.24023
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	151	0661	2	C	0.22808	0.23116	0.21735	0.21995
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	152	1891	2	0	0.26676	0.26931	0.28009	0 28487
151 2001 2 3 0.43322 0.42327 0.41350 0.37992 155 214R 2 1 0.25979 0.21911 0.23716 0.26756 156 216L 2 1 0.27100 0.24931 0.26025 0.31746 157 219R 2 1 0.22419 0.17387 0.18408 0.20470 158 506L 2 1 0.27322 0.24853 0.25065 0.25887 159 509L 2 1 0.28348 0.26522 0.26959 0.31286	154	2081	2	3	0.43522	0.42527	0.41390	0.37992
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	154	200L 214P	2	1	0.75070	0.72327	0.71390	0.27992
150 210L 2 1 0.27100 0.24951 0.20025 0.51740 157 219R 2 1 0.22419 0.17387 0.18408 0.20470 158 506L 2 1 0.27232 0.24853 0.25065 0.25887 159 509L 2 1 0.28348 0.26522 0.26959 0.31286	155	214K 216I	2	1	0.23919	0.21911	0.25710	0.20750
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	150	2100	2	1	0.27100	0.2+931	0.20025	0.31740
150 5001 2 1 0.27252 0.24055 0.25005 0.25087 0.2	159	219K 506I	2	1	0.22419	0.17507	0.10400	0.20470
	159	509L	2	1	0.28348	0.26522	0.26959	0.31286

Table A.3: LOOCV results for surface normal analysis (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
160	518L	2	С	0.31588	0.29451	0.27946	0.30709
161	518R	2	3	0.32623	0.29753	0.30660	0.27269
162	520L	2	С	0.28414	0.24948	0.21839	0.24602
163	520R	2	1	0.42482	0.40716	0.41035	0.43707
164	522L	2	3	0.29816	0.27672	0.26814	0.25401
165	525L	2	1	0.30593	0.29116	0.29798	0.29228
166	526R	2	1	0.29990	0.24010	0.24510	0.25851
167	530R	2	3	0.28159	0.26224	0.26100	0.23648
168	532L	2	1	0.26065	0.22257	0.22829	0.27163
169	532R	2	С	0.37564	0.31993	0.30711	0.30823
170	533L	2	1	0.30165	0.27385	0.27645	0.29151
171	533R	2	1	0.34448	0.28787	0.30716	0.32864
172	536L	2	1	0.26038	0.23078	0.23336	0.27561
173	536R	2	1	0.34739	0.29067	0.29340	0.31087
174	537R	2	1	0.29847	0.24342	0.26257	0.28096
175	539L	2	1	0.25653	0.25639	0.27812	0.29839
176	546L	2	1	0.25338	0.24007	0.24418	0.28975
177	546R	2	1	0.25586	0.21015	0.21774	0.23484
178	689R	2	1	0.29855	0.29085	0.31506	0.30234
179	692L	2	3	0.48266	0.50043	0.49347	0.47367
180	694L	2	С	0.37864	0.35419	0.35012	0.38352
181	701R	2	3	0.38112	0.36509	0.36593	0.32607
182	177L	3	С	0.29588	0.27484	0.25052	0.23883
183	177R	3	С	0.44442	0.42541	0.39742	0.36443
184	206L	3	С	0.54345	0.54103	0.50861	0.49511
185	207R	3	2	0.37147	0.31391	0.30669	0.32743
186	212L	3	С	0.33260	0.27229	0.22748	0.21436
187	215L	3	С	0.33385	0.27523	0.23398	0.22549
188	215R	3	С	0.35322	0.27999	0.26382	0.23526
189	513L	3	С	0.32337	0.28781	0.26817	0.25626
190	513R	3	С	0.37008	0.30803	0.28564	0.26307
191	519L	3	2	0.31689	0.26019	0.21046	0.23389
192	519R	3	2	0.26206	0.20736	0.20268	0.21409
193	526L	3	С	0.32739	0.28320	0.26015	0.25289
194	52R	3	С	0.49796	0.50636	0.48740	0.48076
195	534R	3	2	0.38819	0.33095	0.29952	0.31019
196	538L	3	2	0.31359	0.27808	0.24492	0.29099
197	538R	3	2	0.23454	0.19667	0.19133	0.21487
198	547L	3	2	0.40032	0.35836	0.30405	0.32853
199	547R	3	С	0.38193	0.32082	0.28983	0.23856
200	549R	3	С	0.29303	0.26794	0.27773	0.26646
201	62R	3	С	0.52379	0.50693	0.46756	0.42939
202	697L	3	С	0.43968	0.37383	0.32703	0.27987
203	712L	3	2	0.25560	0.21262	0.19672	0.20964

Table A.3: LOOCV results for surface normal analysis (continuted).

A.4 LOOCV Results for Combination of Gaussian Curvature and Coronal Projection

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
1	003L	0	С	0.2901	0.2973	0.2986	0.3433
2	003R	0	С	0.3173	0.3208	0.3518	0.3859
3	005R	0	1	0.2978	0.2893	0.3021	0.3128
4	007L	0	1	0.3311	0.3229	0.3309	0.3487
5	007R	0	1	0.3215	0.3195	0.3300	0.3433
6	008R	0	С	0.3103	0.3210	0.3407	0.3757
7	009L	0	С	0.3937	0.4139	0.4221	0.4655
8	013R	0	С	0.2945	0.3051	0.3297	0.3537
9	016R	0	С	0.3273	0.3534	0.3661	0.3962
10	025L	0	С	0.3304	0.3630	0.3721	0.4242
11	029R	0	С	0.3467	0.3645	0.3904	0.4255
12	037L	0	2	0.3177	0.3201	0.3086	0.3478
13	037R	0	1	0.3548	0.3508	0.3712	0.3932
14	046L	0	2	0.2559	0.2552	0.2498	0.2901
15	046R	0	1	0.2688	0.2650	0.2896	0.3143
16	049L	0	С	0.2649	0.2725	0.2713	0.3290
17	053L	0	С	0.2709	0.3054	0.3124	0.3712
18	053R	0	С	0.2837	0.3295	0.3401	0.3986
19	055L	0	С	0.2562	0.2853	0.2848	0.3273
20	055R	0	С	0.3026	0.3320	0.3546	0.3909
21	067R	0	С	0.2168	0.2439	0.2637	0.3117
22	073R	0	1	0.3600	0.3513	0.3768	0.3947
23	076L	0	С	0.3968	0.4393	0.4389	0.4947
24	078L	0	С	0.3165	0.3484	0.3575	0.4022
25	079R	0	C	0.2528	0.2598	0.2905	0.3238
26	084L	0	2	0.2619	0.2636	0.2593	0.2938
27	084R	0	1	0.2735	0.2678	0.2867	0.3134
28	088R	0	С	0.2837	0.2952	0.3209	0.3571
29	089R	0	1	0.2869	0.2775	0.3048	0.3090
30	093L	0	С	0.2344	0.2717	0.2788	0.3413
31	096L	0	С	0.2503	0.2632	0.2634	0.3052
32	113R	0	С	0.2161	0.2201	0.2424	0.2705
33	131R	0	С	0.3011	0.3283	0.3580	0.3919
34	135R	0	С	0.3061	0.3250	0.3579	0.3912
35	154R	0	1	0.2458	0.2455	0.2803	0.3190
36	160L	0	2	0.2422	0.2300	0.2288	0.2577
37	175L	0	С	0.2606	0.2774	0.2673	0.3118
38	183L	0	С	0.2512	0.2752	0.2818	0.3456
39	186R	0	С	0.2522	0.2733	0.2936	0.3279
40	188R	0	1	0.2322	0.2054	0.2431	0.2531
41	192L	0	С	0.2413	0.2590	0.2610	0.3027
42	200L	0	2	0.3061	0.3050	0.3019	0.3316
43	201R	0	1	0.3448	0.3351	0.3539	0.3697
44	203L	0	2	0.3268	0.3241	0.3143	0.3498
45	204L	0	2	0.2482	0.2345	0.2145	0.2420
46	205L	0	2	0.2455	0.2482	0.2441	0.2894
47	205R	0	1	0.2380	0.2223	0.2485	0.2749
48	211R	0	1	0.3096	0.2863	0.2903	0.2966
49	217L	0	2	0.2729	0.2566	0.2422	0.2743
50	220L	0	С	0.2213	0.2433	0.2453	0.2897

Table A.4: LOOCV results for Gaussian curvature and coronal projection.

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
51	220R	0	С	0.2982	0.3064	0.3348	0.3709
52	505L	0	C	0.2980	0.3118	0.3109	0.3553
53	505R	0	C	0.2453	0.2674	0.2987	0.3388
54	508R	Ő	1	0.2498	0.2061	0.2274	0.2292
55	511L	Ő	2	0.2747	0.2432	0.2308	0.2432
56	523L	0	2	0.2516	0.2374	0.2263	0.2672
57	529D	0	1	0.2310	0.2374	0.2203	0.2603
59	520K	0	ſ	0.2433	0.2301	0.2441	0.2095
50	529L	0	C	0.2702	0.2924	0.2944	0.3304
59	529K	0	C	0.2512	0.2390	0.2805	0.5240
60	535L 525D	0	2	0.2821	0.2759	0.2025	0.3015
01	535K	0	1	0.2335	0.1999	0.2234	0.2335
62	542L	0	2	0.2478	0.2403	0.2350	0.2576
63	542R	0	1	0.2319	0.2313	0.2459	0.2817
64	554L	0	2	0.2618	0.2592	0.2545	0.2844
65	554R	0	1	0.2407	0.2255	0.2392	0.2409
66	700R	0	1	0.2312	0.2019	0.2170	0.2291
67	702L	0	1	0.2381	0.2359	0.2365	0.2719
68	702R	0	1	0.2277	0.2172	0.2255	0.2396
69	704R	0	1	0.2312	0.2020	0.2239	0.2361
70	705L	0	2	0.2470	0.2265	0.2218	0.2358
71	710L	0	2	0.2513	0.2097	0.2035	0.2088
72	006L	1	0	0.2665	0.2716	0.2698	0.3048
73	012L	1	2	0.3227	0.3262	0.3169	0.3467
74	012R	1	С	0.3048	0.3003	0.3149	0.3289
75	018L	1	0	0.3609	0.3825	0.3741	0.4199
76	018R	1	0	0.3489	0.3614	0.3841	0.4029
77	022L	1	0	0.3682	0.3830	0.3828	0.4245
78	022R	1	0	0.3175	0.3360	0.3570	0.3955
79	0231	1	0	0.3679	0 3849	0 3803	0 4247
80	023E	1	Ő	0.3701	0.3812	0.4070	0.4359
81	023R	1	3	0.3906	0.3778	0.4070	0.3540
82	047I	1	2	0.3004	0.3018	0.3700	0.3110
82	047L 047D	1	Ć	0.3032	0.3016	0.2944	0.3473
03	04/K	1	C	0.3032	0.2910	0.3164	0.3473
04 05	049K	1	0	0.2382	0.2024	0.2951	0.5278
8J 97	050L	1	2	0.1873	0.1788	0.1003	0.2137
80	05/K	1	C	0.2306	0.1980	0.2103	0.2193
8/	UGUL	1	U	0.2222	0.2306	0.2331	0.2644
88	069R	1	C	0.2948	0.2872	0.3121	0.3316
89	070R	1	C	0.2299	0.2040	0.2286	0.2392
90	07/5R	1	C	0.2192	0.2039	0.2243	0.2358
91	082L	1	0	0.2033	0.2035	0.2038	0.2389
92	086L	1	2	0.2452	0.2420	0.2280	0.2743
93	094R	1	С	0.2274	0.2194	0.2412	0.2702
94	095R	1	С	0.3225	0.3038	0.3195	0.3084
95	098R	1	С	0.2617	0.2436	0.2681	0.2660
96	124R	1	0	0.2958	0.2984	0.3302	0.3573
97	133L	1	2	0.2554	0.2435	0.2214	0.2511
98	133R	1	С	0.2511	0.2407	0.2514	0.2578
99	163R	1	С	0.2986	0.2829	0.3050	0.3149
100	181L	1	0	0.2462	0.2592	0.2595	0.2993
101	184L	1	0	0.2022	0.2168	0.2194	0.2713
102	190L	1	2	0.2313	0.2329	0.2311	0.2485
103	197R	1	Ē	0.2451	0.2189	0.2371	0.2524
104	1991	1	2	0.2236	0 2171	0 2071	0.2370
101	1//1	1	-	0.2250	0.21/1	0.2071	0.2070

Table A.4: LOOCV results for Gaussian curvature and coronal projection (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
106	203R	1	С	0.4245	0.4228	0.4251	0.4501
107	204R	1	С	0.2585	0.2305	0.2375	0.2398
108	209R	1	3	0.2377	0.1903	0.1881	0.1738
109	210L	1	3	0.2776	0.2359	0.2113	0.1974
110	219L	1	2	0.2538	0.2469	0.2364	0.2549
111	507L	1	2	0.2501	0.2148	0.1881	0.2021
112	507R	1	3	0.2663	0.2193	0.2256	0.2188
113	509R	1	2	0.2871	0.2474	0.2472	0.2566
114	511R	1	С	0.2444	0.1925	0.2008	0.1946
115	512R	1	С	0.2185	0.1945	0.2146	0.2334
116	514L	1	2	0.2598	0.2413	0.2307	0.2636
117	515L	1	2	0.2376	0.2108	0.2056	0.2189
118	515R	1	С	0.2620	0.2177	0.2315	0.2208
119	516L	1	2	0.3041	0.2700	0.2357	0.2420
120	516R	1	С	0.2871	0.2421	0.2489	0.2482
121	517L	1	2	0.3297	0.3009	0.2751	0.2861
122	517R	1	3	0.2782	0.2300	0.2302	0.2300
123	521L	1	2	0.2519	0.2403	0.2283	0.2704
124	522R	1	С	0.2197	0.1941	0.2083	0.2247
125	523R	1	3	0.2550	0.2033	0.2037	0.1881
126	527L	1	2	0.3108	0.2984	0.2849	0.3136
127	527R	1	С	0.2377	0.2074	0.2198	0.2417
128	534L	1	2	0.3596	0.3393	0.3221	0.3257
129	539R	1	С	0.2408	0.2165	0.2379	0.2487
130	540L	1	3	0.2399	0.2116	0.1994	0.1951
131	541L	1	2	0.3446	0.3315	0.3111	0.3273
132	541R	1	С	0.2545	0.2175	0.2233	0.2317
133	543L	1	2	0.2423	0.2165	0.1919	0.2091
134	543R	1	С	0.2461	0.2156	0.2213	0.2167
135	574R	1	3	0.2409	0.2184	0.2288	0.2170
136	691L	1	2	0.2659	0.2638	0.2597	0.3075
137	691R	1	2	0.2432	0.2127	0.2100	0.2265
138	699R	1	С	0.2003	0.1747	0.1894	0.1961
139	700L	1	2	0.2371	0.2141	0.2037	0.2173
140	703R	1	С	0.2665	0.2277	0.2377	0.2370
141	704L	1	2	0.2558	0.2432	0.2216	0.2582
142	710R	1	С	0.2400	0.1977	0.2138	0.2172
143	711L	1	2	0.2986	0.2655	0.2504	0.2583
144	713L	1	2	0.2417	0.2286	0.2194	0.2593
145	713R	1	С	0.2543	0.2151	0.2366	0.2382
146	717R	1	C	0.2410	0.2205	0.2407	0.2510
147	002L	2	С	0.3657	0.3597	0.3464	0.3564
148	010L	2	3	0.4275	0.4172	0.4070	0.3953
149	026L	2	С	0.3448	0.3378	0.3362	0.3432
150	029L	2	0	0.4026	0.4512	0.4806	0.5335
151	065L	2	С	0.2492	0.2418	0.2368	0.2670
152	066L	2	0	0.3447	0.3546	0.3513	0.3780
153	189L	2	1	0.2439	0.2264	0.2343	0.2367
154	208L	2	3	0.3416	0.3035	0.2806	0.2692
155	214R	2	1	0.2418	0.2088	0.2239	0.2252
156	216L	2	C	0.2468	0.2384	0.2360	0.2750
157	219R	2	1	0.2479	0.2164	0.2314	0.2180
158	506L	2	C	0.2725	0.2456	0.2292	0.2451
159	509L	2	C	0.2852	0.2660	0.2529	0.2685
160	518L	2	С	0.2715	0.2444	0.2331	0.2388

Table A.4: LOOCV results for Gaussian curvature and coronal projection (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
161	518R	2	3	0.2552	0.2093	0.1909	0.1747
162	520L	2	С	0.2329	0.2024	0.1829	0.1907
163	520R	2	1	0.2569	0.2200	0.2230	0.2294
164	522L	2	С	0.2907	0.2659	0.2516	0.2591
165	525L	2	3	0.3084	0.2601	0.2364	0.2102
166	526R	2	3	0.2441	0.1960	0.2000	0.1849
167	530R	2	3	0.2919	0.2592	0.2617	0.2532
168	532L	2	С	0.2316	0.2035	0.1968	0.2061
169	532R	2	3	0.3034	0.2455	0.2394	0.1936
170	533L	2	С	0.3108	0.2783	0.2574	0.2728
171	533R	2	3	0.2954	0.2517	0.2587	0.2400
172	536L	2	С	0.3019	0.2893	0.2834	0.3115
173	536R	2	1	0.2836	0.2394	0.2462	0.2396
174	537R	2	1	0.2407	0.1995	0.2170	0.2193
175	539L	2	С	0.2331	0.2114	0.1988	0.2196
176	546L	2	С	0.2336	0.2227	0.2160	0.2463
177	546R	2	1	0.2239	0.1946	0.2064	0.2084
178	689R	2	3	0.2827	0.2356	0.2484	0.2198
179	692L	2	С	0.3449	0.3229	0.3206	0.3250
180	694L	2	С	0.2589	0.2317	0.2176	0.2200
181	701R	2	3	0.3271	0.2751	0.2781	0.2372
182	177L	3	2	0.2632	0.2270	0.1921	0.1954
183	177R	3	С	0.3467	0.2945	0.2909	0.2477
184	206L	3	С	0.4136	0.3782	0.3569	0.3447
185	207R	3	С	0.2856	0.2559	0.2556	0.2554
186	212L	3	С	0.3001	0.2558	0.2229	0.2101
187	215L	3	С	0.2839	0.2390	0.2065	0.1940
188	215R	3	С	0.2821	0.2217	0.2079	0.1661
189	513L	3	С	0.2888	0.2434	0.2139	0.1988
190	513R	3	С	0.3226	0.2742	0.2571	0.2362
191	519L	3	2	0.2490	0.2333	0.2159	0.2195
192	519R	3	С	0.2350	0.2005	0.2037	0.1946
193	526L	3	С	0.2718	0.2318	0.1994	0.1953
194	52R	3	С	0.2853	0.2469	0.2393	0.2345
195	534R	3	С	0.2785	0.2302	0.2222	0.1954
196	538L	3	2	0.2614	0.2208	0.1949	0.1957
197	538R	3	С	0.2286	0.1742	0.1729	0.1676
198	547L	3	С	0.2862	0.2481	0.2253	0.2237
199	547R	3	С	0.3275	0.2728	0.2619	0.2243
200	549R	3	С	0.2673	0.2102	0.2034	0.1723
201	62R	3	С	0.3946	0.3512	0.3368	0.2958
202	697L	3	С	0.4037	0.3531	0.3228	0.2735
203	712L	3	С	0.2821	0.2399	0.2122	0.1923

Table A.4: LOOCV results for Gaussian curvature and coronal projection (continuted).

A.5 LOOCV Results for Combination of Gaussian Curvature and the Y Component of the Surface Normal

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
1	003L	0	С	0.24162	0.25403	0.28942	0.33622
2	003R	0	С	0.25076	0.27996	0.32342	0.37627
3	005R	0	1	0.28771	0.28279	0.31696	0.34141
4	007L	0	С	0.35657	0.36142	0.37300	0.38500
5	007R	0	С	0.32453	0.33128	0.35130	0.36681
6	008R	0	С	0.32404	0.36049	0.38380	0.41215
7	009L	0	С	0.38837	0.41258	0.43036	0.48389
8	013R	0	С	0.27959	0.30135	0.33956	0.37777
9	016R	0	С	0.35834	0.40062	0.41791	0.44192
10	025L	0	С	0.33551	0.37949	0.40343	0.44902
11	029R	0	С	0.39008	0.40149	0.43117	0.48200
12	037L	0	С	0.29053	0.29668	0.30979	0.34644
13	037R	0	С	0.30984	0.32792	0.35348	0.38602
14	046L	0	С	0.23613	0.23865	0.25531	0.29129
15	046R	0	С	0.23325	0.24867	0.28631	0.32750
16	049L	0	С	0.23477	0.24963	0.28841	0.34281
17	053L	0	С	0.27075	0.31540	0.34839	0.40067
18	053R	0	С	0.28038	0.34077	0.36103	0.41672
19	055L	0	С	0.24185	0.28584	0.30616	0.35125
20	055R	0	С	0.31002	0.35848	0.38887	0.42405
21	067R	0	С	0.23142	0.27304	0.30729	0.35109
22	073R	0	С	0.31769	0.34729	0.36899	0.39799
23	076L	0	С	0.37818	0.42406	0.43745	0.50398
24	078L	0	С	0.34691	0.37609	0.39695	0.45001
25	079R	0	С	0.20988	0.23148	0.26471	0.31404
26	084L	0	С	0.27405	0.29022	0.31610	0.35211
27	084R	0	С	0.28774	0.29650	0.33179	0.37272
28	088R	0	С	0.28421	0.31064	0.35205	0.39966
29	089R	0	С	0.21754	0.22530	0.26157	0.29446
30	093L	0	С	0.22462	0.26475	0.30046	0.36159
31	096L	0	С	0.24009	0.24749	0.26923	0.30778
32	113R	0	С	0.21474	0.22687	0.26629	0.31191
33	131R	0	С	0.25427	0.30714	0.34046	0.39224
34	135R	0	С	0.28774	0.32598	0.37092	0.42158
35	154R	0	С	0.20408	0.22132	0.26961	0.32480
36	160L	0	1	0.25814	0.24171	0.24541	0.28391
37	175L	0	С	0.22992	0.25499	0.26566	0.31219
38	183L	0	С	0.23712	0.27554	0.30217	0.35522
39	186R	0	С	0.23813	0.25659	0.28038	0.32002
40	188R	0	1	0.23433	0.23082	0.27632	0.29790
41	192L	0	С	0.28005	0.28951	0.29395	0.34177
42	200L	0	С	0.24905	0.25683	0.26568	0.28418
43	201R	0	С	0.22444	0.24803	0.27299	0.30693
44	203L	0	С	0.27824	0.27838	0.28574	0.30719
45	204L	0	1	0.22215	0.20920	0.21480	0.24641
46	205L	0	С	0.25168	0.25535	0.28287	0.32583
47	205R	0	С	0.22586	0.23215	0.27832	0.31147
48	211R	0	1	0.26423	0.26207	0.26759	0.28843
49	217L	0	2	0.23769	0.20881	0.19354	0.20353
50	220L	0	С	0.29745	0.30542	0.31698	0.37317

Table A.5: LOOCV results for Gaussian curvature and surface normal.

51 52 53 54 55 56 57 58 59 60 61 62 63	220R 505L 505R 508R 511L 523L 523L 529R 535L 535R 542L 542R 554L 554R 700R	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	C C C 1 1 1 C C C 1 1 C C	0.20159 0.26075 0.24414 0.25301 0.29208 0.22956 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.23300 0.28398 0.27311 0.21432 0.25794 0.21384 0.30658 0.27605 0.25548 0.22705 0.21199	0.26959 0.30347 0.31320 0.25472 0.26781 0.24162 0.31608 0.30447 0.28865 0.24808	0.32368 0.33944 0.36446 0.27795 0.30043 0.27141 0.32230 0.36367 0.32720 0.28289
52 53 54 55 56 57 58 59 60 61 62 63	505L 505R 505R 508R 511L 523L 523L 529L 529R 535L 535R 542L 542R 554L 554R 700R		C C 1 1 1 C C C 1 1 C C	0.26175 0.26075 0.24414 0.25301 0.29208 0.22956 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	$\begin{array}{c} 0.28398\\ 0.27311\\ 0.21432\\ 0.25794\\ 0.21384\\ 0.30658\\ 0.27605\\ 0.25548\\ 0.22705\\ 0.21199\end{array}$	0.30347 0.31320 0.25472 0.26781 0.24162 0.31608 0.30447 0.28865 0.24808	0.33944 0.36446 0.27795 0.30043 0.27141 0.32230 0.36367 0.32720 0.28289
53 54 55 56 57 58 59 60 61 62 63	505R 505R 508R 511L 523L 528R 529L 529R 535L 535R 542L 542R 554L 554R 700R		C 1 1 1 C C C 1 1 1 C C	0.24414 0.25301 0.29208 0.22956 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.27311 0.21432 0.25794 0.21384 0.30658 0.27605 0.25548 0.22705 0.21199	0.31320 0.25472 0.26781 0.24162 0.31608 0.30447 0.28865 0.24808	0.36446 0.27795 0.30043 0.27141 0.32230 0.36367 0.32720 0.28289
54 55 56 57 58 59 60 61 62 63	508R 508R 511L 523L 528R 529L 529R 535L 535R 542L 542R 554L 554R 700R		1 1 1 C C C 1 1 1 C	0.25301 0.29208 0.22956 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.21432 0.25794 0.21384 0.30658 0.27605 0.25548 0.22705 0.21199	0.25472 0.26781 0.24162 0.31608 0.30447 0.28865 0.24808	0.27795 0.30043 0.27141 0.32230 0.36367 0.32720 0.28289
55 56 57 58 59 60 61 62 63	50000 5111 5231 5232 5292 5292 5351 5352 5352 5421 5422 5542 5542 5542 5542 7008		1 1 C C C 1 1 C C	0.29208 0.22956 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.25794 0.21384 0.30658 0.27605 0.25548 0.22705 0.21199	0.26781 0.24162 0.31608 0.30447 0.28865 0.24808	0.30043 0.27141 0.32230 0.36367 0.32720 0.28289
56 57 58 59 60 61 62 63	511L 523L 528R 529L 529R 535L 535R 542L 542R 554L 554R 700R		1 C C C 1 1 C C	0.22956 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.21384 0.30658 0.27605 0.25548 0.22705 0.21199	0.20781 0.24162 0.31608 0.30447 0.28865 0.24808	0.30045 0.27141 0.32230 0.36367 0.32720 0.28289
57 58 59 60 61 62 63	523L 528R 529L 529R 535L 535R 542L 542R 554L 554R 700R		C C C 1 1 C C	0.22930 0.30586 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.21384 0.30658 0.27605 0.25548 0.22705 0.21199	0.24102 0.31608 0.30447 0.28865 0.24808	0.32230 0.36367 0.32720 0.28289
57 58 59 60 61 62 63	528R 529L 529R 535L 535R 542L 542R 554L 554R 700R	0 0 0 0 0 0 0 0	C C 1 1 C C	0.30386 0.26008 0.23213 0.22749 0.23532 0.26550 0.19291	0.27605 0.25548 0.22705 0.21199	0.30447 0.28865 0.24808	0.32230 0.36367 0.32720 0.28289
58 59 60 61 62 63	529L 529R 535L 535R 542L 542R 554L 554R 700R	0 0 0 0 0 0 0	C 1 1 C C	0.23213 0.22749 0.23532 0.26550 0.19291	0.27603 0.25548 0.22705 0.21199	0.28865 0.24808	0.32720 0.28289
60 61 62 63	529R 535L 535R 542L 542R 554L 554L 554R 700R	0 0 0 0 0 0	1 1 C C	0.23213 0.22749 0.23532 0.26550 0.19291	0.22705 0.21199	0.28865	0.32720 0.28289
60 61 62 63	535L 535R 542L 542R 554L 554R 700R	0 0 0 0 0	1 C C	0.22749 0.23532 0.26550 0.19291	0.22703	0.24808	0.28289
61 62 63	535R 542L 542R 554L 554R 700R	0 0 0 0	C C	0.23532 0.26550 0.19291	0.21199		0 077777
62 63	542L 542R 554L 554R 700R	0 0 0	C	0.26550	0 0 0 0 0 0 0	0.24762	0.27777
63	542R 554L 554R 700R	0 0 0	С	0.19291	0.26923	0.28182	0.29218
~ •	554L 554R 700R	0		0.1/1/0	0.19725	0.24013	0.28375
64	554R 700R	0	2	0.24449	0.24459	0.24010	0.26308
65	700R	0	1	0.24242	0.23361	0.24308	0.26978
66		0	1	0.23002	0.19777	0.24090	0.27118
67	702L	0	С	0.23465	0.24076	0.26529	0.29280
68	702R	0	С	0.22866	0.22955	0.27184	0.29431
69	704R	0	1	0.24361	0.22561	0.26472	0.29730
70	705L	0	1	0.24036	0.22804	0.25009	0.28090
71	710L	0	1	0.32543	0.28081	0.28164	0.30437
72	006L	1	0	0.27812	0.29099	0.30626	0.33507
73	012L	1	С	0.31146	0.30758	0.31319	0.34275
74	012R	1	0	0.30045	0.30273	0.33059	0.35841
75	018L	1	0	0.30923	0.33647	0.35464	0.39767
76	018R	1	0	0.35126	0.38742	0.40598	0.42655
77	022L	1	0	0.31724	0.34203	0.36880	0.40496
78	022R	1	Ő	0.32308	0.35686	0.39077	0.42417
79	0231	1	Ő	0.30389	0.32559	0.34899	0.38686
80	023E	1	0	0.30197	0.32823	0.36340	0.40682
81	023K 027P	1	3	0.30197	0.32823	0.30340	0.40082
82	027K 047I	1	2	0.42070	0.40080	0.28846	0.28078
82	047L	1	0	0.29470	0.29010	0.28840	0.20978
03	04/K	1	0	0.24432	0.23703	0.29174	0.33080
84	049K	1	0	0.25371	0.27589	0.32200	0.36973
85	056L	1	0	0.20455	0.21394	0.23011	0.26047
86	05/R	1	C	0.20452	0.18242	0.19880	0.23274
87	060L	1	0	0.22219	0.22968	0.24652	0.28965
88	069R	1	0	0.21101	0.21774	0.25248	0.28368
89	070R	1	С	0.25396	0.21875	0.23462	0.26942
90	075R	1	С	0.24470	0.22755	0.24061	0.27492
91	082L	1	С	0.24790	0.23118	0.24371	0.28490
92	086L	1	С	0.23113	0.22664	0.22749	0.27567
93	094R	1	0	0.21615	0.23773	0.26544	0.29744
94	095R	1	0	0.33958	0.35330	0.35035	0.35020
95	098R	1	С	0.21404	0.20244	0.22804	0.25480
96	124R	1	0	0.24729	0.25526	0.29400	0.34119
97	133L	1	С	0.21667	0.19958	0.20175	0.21257
98	133R	1	0	0.29987	0.30552	0.30654	0.30155
99	163R	1	0	0.25587	0.26058	0.28812	0.32029
100	181L	1	Ő	0.23527	0.23996	0.26126	0.30808
101	184L	1	Ő	0.18128	0.19662	0.21992	0.27464
102	1901	1	Č	0.21222	0.20461	0.200/7	0.27404
102	107D	1	C	0.21222	0.20401	0.20947	0.23031
103	19/K 1001	1		0.29700	0.23337	0.27301	0.29030
104	177L	1	C	0.22321	0.20908	0.22100	0.20399

Table A.5: LOOCV results for Gaussian curvature and surface normal (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
106	203R	1	С	0.23190	0.22189	0.25262	0.30465
107	204R	1	С	0.21732	0.20282	0.21588	0.23227
108	209R	1	2	0.35114	0.30848	0.28732	0.30064
109	210L	1	3	0.29835	0.24582	0.23244	0.22059
110	219L	1	С	0.24226	0.22247	0.23380	0.26416
111	507L	1	2	0.29231	0.25619	0.23096	0.25392
112	507R	1	2	0.29804	0.24463	0.24408	0.24758
113	509R	1	С	0.30517	0.26270	0.27715	0.29014
114	511R	1	С	0.24751	0.20425	0.23078	0.24390
115	512R	1	С	0.24123	0.20973	0.23766	0.27553
116	514L	1	С	0.25264	0.24177	0.25181	0.27015
117	515L	1	С	0.23958	0.21068	0.22779	0.25257
118	515R	1	С	0.26155	0.21880	0.23942	0.25144
119	516L	1	2	0.32757	0.28526	0.25461	0.26168
120	516R	1	С	0.31557	0.26930	0.27392	0.29501
121	517L	1	3	0.33023	0.30754	0.29920	0.29573
122	517R	1	2	0.32251	0.26826	0.26797	0.28380
123	521L	1	С	0.23820	0.22090	0.23502	0.26762
124	522R	1	С	0.20241	0.18075	0.20033	0.22569
125	523R	1	2	0.29702	0.24312	0.24252	0.25060
126	527L	1	2	0.30505	0.30522	0.30448	0.32466
127	527R	1	С	0.22753	0.19880	0.22777	0.25261
128	534L	1	3	0.31966	0.30796	0.29258	0.28535
129	539R	1	С	0.25886	0.22630	0.25551	0.29686
130	540L	1	3	0.30995	0.29366	0.28435	0.27176
131	541L	1	3	0.29025	0.27702	0.27608	0.27523
132	541R	1	2	0.30390	0.25825	0.25824	0.28395
133	543L	1	2	0.27107	0.22850	0.21129	0.21482
134	543R	1	2	0.29222	0.25229	0.24993	0.26179
135	574R	1	0	0.24620	0.24760	0.26795	0.27260
136	691L	1	С	0.25045	0.24067	0.25891	0.30082
137	691R	1	С	0.27501	0.25633	0.26737	0.26720
138	699R	1	С	0.19545	0.16558	0.18478	0.21250
139	700L	1	С	0.22504	0.20119	0.21035	0.23248
140	703R	1	С	0.26107	0.22985	0.24375	0.25756
141	704L	1	С	0.25338	0.24259	0.25800	0.28663
142	710R	1	С	0.28417	0.23589	0.25017	0.27620
143	711L	1	3	0.30052	0.26945	0.26568	0.26557
144	713L	1	С	0.22765	0.21539	0.24089	0.27139
145	713R	1	С	0.22740	0.21031	0.24625	0.26307
146	717R	1	С	0.23717	0.23197	0.27029	0.29101
147	002L	2	3	0.37683	0.36290	0.35759	0.35186
148	010L	2	3	0.44630	0.43954	0.42843	0.39493
149	026L	2	0	0.36717	0.37401	0.37587	0.36941
150	029L	2	0	0.42132	0.45620	0.46645	0.48792
151	065L	2	1	0.22009	0.20400	0.20927	0.24021
152	066L	2	0	0.34034	0.35038	0.34885	0.36045
153	189L	2	1	0.26063	0.25533	0.26893	0.26818
154	208L	2	3	0.37971	0.34854	0.33529	0.29820
155	214R	2	1	0.25129	0.21215	0.21964	0.24200
156	216L	2	1	0.26240	0.24360	0.25316	0.29510
157	219R	2	1	0.22427	0.17946	0.18781	0.19787
158	506L	2	3	0.28333	0.24690	0.24387	0.24364
159	509L	2	С	0.30615	0.28237	0.28178	0.30326
160	518L	2	С	0.31198	0.27983	0.27190	0.28593

Table A.5: LOOCV results for Gaussian curvature and surface normal (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
161	518R	2	3	0.30418	0.25990	0.25742	0.22810
162	520L	2	С	0.27485	0.23561	0.21324	0.22377
163	520R	2	1	0.35606	0.32838	0.32928	0.34931
164	522L	2	3	0.27358	0.24379	0.24078	0.22538
165	525L	2	3	0.31496	0.27345	0.26952	0.25109
166	526R	2	С	0.28210	0.22673	0.22179	0.22609
167	530R	2	3	0.27322	0.24573	0.23692	0.21637
168	532L	2	1	0.24024	0.19753	0.20593	0.23458
169	532R	2	3	0.34610	0.28556	0.27482	0.25970
170	533L	2	С	0.29460	0.25255	0.24675	0.25299
171	533R	2	1	0.33037	0.27694	0.28407	0.29190
172	536L	2	1	0.26260	0.23499	0.24273	0.26838
173	536R	2	1	0.32041	0.26603	0.26815	0.27045
174	537R	2	1	0.26465	0.21505	0.22803	0.24112
175	539L	2	1	0.25125	0.23298	0.24540	0.26290
176	546L	2	1	0.24512	0.22629	0.23214	0.26497
177	546R	2	1	0.24160	0.20108	0.20765	0.21660
178	689R	2	3	0.29452	0.26557	0.27941	0.25931
179	692L	2	3	0.40043	0.39356	0.39018	0.37292
180	694L	2	С	0.32688	0.29598	0.29447	0.31339
181	701R	2	3	0.34415	0.30652	0.30015	0.26148
182	177L	3	С	0.27726	0.24556	0.22116	0.20965
183	177R	3	С	0.39065	0.35505	0.33546	0.29525
184	206L	3	С	0.44816	0.42741	0.39588	0.37662
185	207R	3	2	0.32878	0.28048	0.27023	0.28251
186	212L	3	С	0.31793	0.25787	0.22330	0.19972
187	215L	3	С	0.30593	0.24715	0.21448	0.19293
188	215R	3	С	0.31639	0.24797	0.22537	0.19462
189	513L	3	С	0.31155	0.26394	0.24177	0.22044
190	513R	3	С	0.35271	0.29653	0.27164	0.25406
191	519L	3	2	0.28129	0.24338	0.21507	0.22718
192	519R	3	2	0.23669	0.19410	0.19342	0.20018
193	526L	3	С	0.30988	0.26322	0.23892	0.22299
194	52R	3	С	0.40206	0.39170	0.37461	0.36574
195	534R	3	2	0.33776	0.28396	0.25680	0.25704
196	538L	3	2	0.29301	0.24742	0.22358	0.24919
197	538R	3	2	0.23967	0.18606	0.17982	0.19260
198	547L	3	2	0.35416	0.30694	0.26973	0.27753
199	547R	3	С	0.34408	0.28369	0.25381	0.20726
200	549R	3	С	0.27614	0.22923	0.22984	0.21405
201	62R	3	С	0.44284	0.41466	0.38122	0.33905
202	697L	3	С	0.42503	0.36390	0.32787	0.27519
203	712L	3	С	0.26927	0.22033	0.20484	0.20250

Table A.5: LOOCV results for Gaussian curvature and surface normal (continuted).

A.6 LOOCV Results for Combination of Coronal Projection and the Y Component of the Surface Normal

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
1	003L	0	С	0.2304	0.2388	0.2485	0.3140
2	003R	0	1	0.2730	0.2689	0.3211	0.3577
3	005R	0	1	0.2298	0.2081	0.2430	0.2658
4	007L	0	С	0.2610	0.2706	0.2800	0.3054
5	007R	0	С	0.2224	0.2383	0.2603	0.2847
6	008R	0	С	0.3370	0.3644	0.3842	0.4179
7	009L	0	С	0.2360	0.2690	0.2814	0.3448
8	013R	0	С	0.2018	0.2091	0.2576	0.2921
9	016R	0	С	0.3591	0.3892	0.4044	0.4273
10	025L	0	С	0.3203	0.3641	0.3790	0.4342
11	029R	0	С	0.3041	0.3100	0.3405	0.3947
12	037L	0	2	0.2860	0.2842	0.2753	0.3251
13	037R	0	1	0.3114	0.3057	0.3385	0.3591
14	046L	Õ	Ċ	0.2340	0.2466	0.2488	0.3006
15	046R	Ő	C	0.2255	0.2382	0.2851	0.3170
16	0491	Ő	C	0.2598	0.2766	0.2868	0.3511
17	053L	Ő	Č	0.2766	0.3144	0 3340	0 3995
18	053R	Ő	Č	0.2664	0.3144	0 3459	0.3984
19	0551	Ő	Č	0.2307	0.2700	0.2878	0.3455
20	055E	Ő	Č	0.2568	0.2988	0 3393	0.3833
20	067R	0	C	0.1960	0.2315	0.2733	0.3207
21	073R	0	C	0.4094	0.4221	0.2799	0.3207
22	0761	0	C	0.4094	0.4047	0.4300	0.4879
23	0781	0	C	0.3749	0.3478	0.3628	0.4372
25	070E	0	1	0.3234	0.2488	0.3020	0.3245
25	09/1	0	ſ	0.2370	0.2400	0.2780	0.3245
20	084L	0	C	0.2337	0.2022	0.2780	0.3301
27	004K	0	C	0.2170	0.2551	0.2701	0.3233
20	0800	0	1	0.2417	0.2040	0.3138	0.3090
29	0031	0	ſ	0.2770	0.2033	0.3028	0.3131
21	0951	0	C	0.2502	0.2750	0.2930	0.3093
22	112D	0	C 1	0.2350	0.2043	0.2055	0.3165
32 22	113K 121D	0		0.2033	0.2049	0.2302	0.2955
33 24	131K 125D	0	C	0.2800	0.2968	0.3442	0.3848
54 25	153K	0	C	0.2990	0.3122	0.3080	0.4110
35	154K	0	C	0.2303	0.2397	0.2976	0.3439
30 27	100L	0	2	0.2755	0.2557	0.2377	0.2929
37	1/3L	0	C	0.2143	0.2425	0.2451	0.3070
38	183L	0	C	0.2853	0.3228	0.3386	0.3974
39	180K	0	C	0.1882	0.2062	0.2416	0.2922
40	188R	0	С	0.2235	0.2236	0.2646	0.2834
41	192L	0	2	0.2809	0.2886	0.2780	0.3335
42	200L	0	С	0.3411	0.3561	0.3503	0.3804
43	201R	0	C	0.3490	0.3511	0.3775	0.3925
44	203L	0	C	0.3480	0.3562	0.3529	0.3878
45	204L	0	2	0.2229	0.2266	0.2215	0.2659
46	205L	0	С	0.2493	0.2624	0.2774	0.3354
47	205R	0	С	0.2368	0.2385	0.2885	0.3223
48	211R	0	1	0.3061	0.2942	0.3097	0.3298
49	217L	0	2	0.2940	0.2832	0.2547	0.2857

Table A.6: LOOCV results for coronal projection and surface normal.

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
50	220L	0	1	0.3061	0.3036	0.3135	0.3676
51	220R	0	С	0.2870	0.2926	0.3336	0.3824
52	505L	0	С	0.2892	0.3130	0.3180	0.3696
53	505R	0	С	0.2171	0.2429	0.2868	0.3423
54	508R	0	1	0.2324	0.2027	0.2457	0.2641
55	511L	0	2	0.2968	0.2819	0.2756	0.3093
56	523L	Õ	Ē	0.2405	0 2474	0 2497	0 3048
57	528R	Ő	Č	0.3087	0.3210	0.3261	0.3415
58	5201	0	C	0.360	0.3210	0.3201	0.3568
50	529R	0	C	0.2560	0.2010	0.2679	0.3199
60	525I	0	C	0.2000	0.2900	0.2883	0.3402
61	535D	0	1	0.2007	0.2251	0.2585	0.2856
62	540I	0	ſ	0.2401	0.2231	0.2363	0.2850
62	542L	0	C	0.2787	0.2943	0.2803	0.3133
05	J42K	0	C	0.1847	0.1905	0.2221	0.2774
04	334L	U	2	0.2460	0.2478	0.2340	0.2788
65	554K	0	1	0.2106	0.1994	0.2181	0.2451
66	700R	0	l	0.2056	0.1841	0.2122	0.2481
67	702L	0	C	0.2442	0.2622	0.2645	0.3080
68	702R	0	С	0.2179	0.2229	0.2509	0.2806
69	704R	0	1	0.2218	0.2019	0.2494	0.2806
70	705L	0	1	0.2345	0.2203	0.2236	0.2599
71	710L	0	2	0.3100	0.2848	0.2695	0.2991
72	006L	1	0	0.2129	0.2272	0.2364	0.2788
73	012L	1	2	0.2281	0.2155	0.2098	0.2567
74	012R	1	С	0.2197	0.2037	0.2486	0.2760
75	018L	1	0	0.2951	0.3206	0.3191	0.3746
76	018R	1	0	0.3208	0.3423	0.3624	0.3805
77	022L	1	0	0.2929	0.3197	0.3265	0.3849
78	022R	1	0	0.2557	0.2908	0.3297	0.3706
79	023L	1	0	0.2977	0.3240	0.3219	0.3799
80	023R	1	Õ	0.3191	0.3210	0.3678	0.3926
81	027R	1	3	0.3535	0.2921	0.2829	0.2391
82	0471	1	2	0.3680	0.3735	0.3548	0.3707
83	047P	1	0	0.2885	0.3735	0.3316	0.3781
84	047R	1	0	0.2605	0.3023	0.3773	0.3623
0 4 95	049K 056I	1	0	0.2037	0.2759	0.3273	0.3023
0J 86	050L	1	C	0.2100	0.2301	0.2404	0.2014
00 07	03/K	1		0.2307	0.2019	0.2203	0.2404
ð/ 00	UOUL	1	U C	0.2110	0.2133	0.2119	0.2087
88	009K	1	C	0.2821	0.2760	0.3145	0.3385
89	070R	1	C	0.2690	0.2319	0.2578	0.2825
90	075R	1	C	0.2576	0.2248	0.2426	0.2668
91	082L	1	С	0.2412	0.2394	0.2403	0.2896
92	086L	1	2	0.2681	0.2734	0.2562	0.3109
93	094R	1	0	0.2410	0.2581	0.2936	0.3205
94	095R	1	0	0.3872	0.3925	0.4020	0.3933
95	098R	1	С	0.2488	0.2282	0.2595	0.2677
96	124R	1	С	0.2748	0.2745	0.3249	0.3612
97	133L	1	2	0.2777	0.2722	0.2492	0.2797
98	133R	1	3	0.3270	0.3257	0.3271	0.3225
99	163R	1	С	0.2723	0.2706	0.3102	0.3281
100	181L	1	0	0.2096	0.2289	0.2384	0.2984
101	184L	1	0	0.1828	0.2099	0.2235	0.2804
102	190L	1	2	0.2182	0.2035	0.1834	0.2180
103	197R	1	С	0.2833	0.2431	0.2718	0.2892
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Table A.6: LOOCV results for coronal projection and surface normal (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
105	200R	1	С	0.2211	0.1981	0.2113	0.2344
105	200R	1	C	0.4312	0.4247	0.4342	0.4693
100	203R 204R	1	C	0.4312	0.7247	0.7360	0.4025
107	204K 200P	1	2	0.2527	0.2149	0.2309	0.2525
100	209K 210I	1	2	0.3322	0.3139	0.3000	0.3090
109	210L 210L	1	2	0.2904	0.2311	0.2210	0.2220
110	219L 507I	1	2	0.2384	0.2544	0.2507	0.2033
111	507L	1	2	0.2775	0.2550	0.2170	0.2496
112	50/K	1	C	0.2768	0.2320	0.2389	0.2451
113	509R	1	C	0.2758	0.2430	0.2742	0.2875
114	SIIK	1	C	0.2211	0.1891	0.2162	0.2331
115	512R	1	С	0.2233	0.1999	0.2383	0.2735
116	514L	1	0	0.2353	0.2482	0.2474	0.2915
117	515L	1	С	0.1918	0.1815	0.1815	0.2265
118	515R	1	С	0.2176	0.1817	0.2117	0.2223
119	516L	1	2	0.3211	0.3009	0.2621	0.2890
120	516R	1	С	0.2892	0.2524	0.2686	0.2895
121	517L	1	2	0.3303	0.3326	0.3194	0.3350
122	517R	1	С	0.2773	0.2343	0.2433	0.2627
123	521L	1	2	0.2580	0.2570	0.2504	0.2990
124	522R	1	С	0.2145	0.1852	0.2055	0.2309
125	523R	1	С	0.2788	0.2337	0.2359	0.2457
126	527L	1	0	0.3367	0.3507	0.3427	0.3734
127	527R	1	С	0.2302	0.2081	0.2396	0.2671
128	534L	1	2	0.3990	0.3959	0.3789	0.3813
129	539R	1	Ē	0 2758	0 2459	0.2766	0 3034
130	5401	1	3	0.2932	0.2876	0.2740	0.2694
131	541L	1	2	0.3594	0.3633	0.3444	0.3649
132	5/1P	1	Č	0.2837	0.2443	0.2528	0.3042
132	542I	1	2	0.2657	0.2443	0.2328	0.2702
133	543L	1		0.2508	0.2242	0.1940	0.2274
134	545K	1	C	0.2757	0.2387	0.2438	0.2364
135	5/4K	1	0	0.2502	0.2575	0.2705	0.2709
130	691L	1	0	0.2530	0.2593	0.2558	0.3152
13/	691R	1	0	0.2603	0.2615	0.2722	0.2846
138	699R	1	С	0.1758	0.1482	0.1670	0.1970
139	700L	1	2	0.1995	0.1919	0.1811	0.2119
140	703R	1	С	0.2603	0.2309	0.2553	0.2630
141	704L	1	0	0.2545	0.2569	0.2560	0.3031
142	710R	1	С	0.2760	0.2388	0.2549	0.2799
143	711L	1	2	0.2701	0.2593	0.2465	0.2625
144	713L	1	0	0.2533	0.2585	0.2572	0.3041
145	713R	1	С	0.2523	0.2363	0.2745	0.2848
146	717R	1	0	0.2000	0.2056	0.2374	0.2681
147	002L	2	С	0.3345	0.3055	0.2823	0.2824
148	010L	2	3	0.4432	0.4241	0.4028	0.3706
149	026L	2	0	0.3989	0.4046	0.3991	0.4018
150	029L	2	0	0.4219	0.4480	0.4605	0.4769
151	065L	2	С	0.2544	0.2401	0.2263	0.2670
152	066L	2	C	0.2345	0.2375	0.2212	0.2476
153	189L	2	1	0.2504	0.2421	0.2470	0.2555
154	2081	2	3	0 4024	0 3892	0 3710	0.3576
155	214R	2	1	0.2506	0.2159	0 2411	0.2525
155	21 4 1 2161	2	ſ	0.2550	0.2139	0.2411	0.2323
150	210L 210D	2	1	0.2339	0.2445	0.2430	0.2909
150	219K 5061	2		0.2478	0.2118	0.2264	0.2242
150	500L	2	C	0.2010	0.2472	0.2304	0.2003
159	209L	2	C	0.2607	0.2477	0.2392	0.2793

Table A.6: LOOCV results for coronal projection and surface normal (continuted).
Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
160	518L	2	С	0.2759	0.2611	0.2419	0.2638
161	518R	2	3	0.2811	0.2546	0.2534	0.2299
162	520L	2	С	0.2438	0.2184	0.1889	0.2164
163	520R	2	1	0.3460	0.3261	0.3312	0.3488
164	522L	2	С	0.3140	0.2964	0.2779	0.2844
165	525L	2	3	0.2992	0.2787	0.2684	0.2580
166	526R	2	1	0.2645	0.2113	0.2256	0.2233
167	530R	2	3	0.2998	0.2749	0.2837	0.2706
168	532L	2	С	0.2527	0.2279	0.2201	0.2475
169	532R	2	3	0.3367	0.2847	0.2758	0.2550
170	533L	2	С	0.3175	0.2978	0.2860	0.3089
171	533R	2	1	0.3111	0.2636	0.2839	0.2836
172	536L	2	С	0.2999	0.2859	0.2754	0.3178
173	536R	2	1	0.3138	0.2665	0.2735	0.2844
174	537R	2	1	0.2774	0.2298	0.2531	0.2624
175	539L	2	1	0.2388	0.2370	0.2380	0.2610
176	546L	2	С	0.2423	0.2367	0.2288	0.2727
177	546R	2	1	0.2393	0.2040	0.2165	0.2273
178	689R	2	1	0.2869	0.2637	0.2879	0.2692
179	692L	2	3	0.4376	0.4470	0.4405	0.4369
180	694L	2	С	0.3218	0.3025	0.2885	0.3119
181	701R	2	3	0.3658	0.3391	0.3480	0.3069
182	177L	3	2	0.2827	0.2584	0.2252	0.2264
183	177R	3	С	0.4063	0.3763	0.3606	0.3271
184	206L	3	С	0.5153	0.5030	0.4789	0.4713
185	207R	3	1	0.3338	0.2922	0.2939	0.3043
186	212L	3	С	0.3156	0.2703	0.2271	0.2241
187	215L	3	С	0.3138	0.2680	0.2267	0.2264
188	215R	3	С	0.3229	0.2570	0.2491	0.2122
189	513L	3	С	0.3015	0.2691	0.2433	0.2379
190	513R	3	С	0.3415	0.2866	0.2719	0.2459
191	519L	3	2	0.2886	0.2508	0.2113	0.2264
192	519R	3	С	0.2605	0.2134	0.2125	0.2089
193	526L	3	2	0.2916	0.2542	0.2244	0.2288
194	52R	3	С	0.4095	0.4049	0.3931	0.3903
195	534R	3	С	0.3379	0.2862	0.2704	0.2614
196	538L	3	2	0.2843	0.2547	0.2190	0.2467
197	538R	3	2	0.2232	0.1855	0.1848	0.1928
198	547L	3	2	0.3417	0.3095	0.2654	0.2845
199	547R	3	С	0.3670	0.3112	0.2969	0.2535
200	549R	3	С	0.2847	0.2519	0.2563	0.2343
201	62R	3	С	0.4837	0.4565	0.4321	0.3961
202	697L	3	С	0.4191	0.3633	0.3219	0.2782
203	712L	3	С	0.2690	0.2328	0.2044	0.1998

Table A.6: LOOCV results for coronal projection and surface normal (continuted).

Table A.6: LOOCV Results for combination of coronal projection and surface normal analysis

A.7 LOOCV Results for Combination of All the Three 3D Features

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Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
1	003L	0	С	0.25537	0.26454	0.27971	0.33140
2	003R	0	С	0.28171	0.29073	0.33241	0.37347
3	005R	0	1	0.27345	0.26268	0.28911	0.30824
4	007L	0	С	0.31880	0.32046	0.33014	0.34788
5	007R	0	С	0.29334	0.29922	0.31625	0.33338
6	008R	0	С	0.32397	0.34921	0.37013	0.40233
7	009L	0	С	0.34716	0.37143	0.38409	0.43580
8	013R	0	С	0.26181	0.27545	0.31113	0.34310
9	016R	0	С	0.34856	0.38160	0.39674	0.42226
10	025L	0	С	0.32879	0.36894	0.38505	0.43594
11	029R	0	С	0.34871	0.36064	0.38914	0.43556
12	037L	0	2	0.29842	0.30070	0.29834	0.33994
13	037R	0	С	0.32598	0.32866	0.35466	0.37973
14	046L	0	С	0.24221	0.24690	0.25131	0.29401
15	046R	0	С	0.24326	0.25087	0.28703	0.31965
16	049L	0	С	0.25348	0.26651	0.28227	0.34111
17	053L	0	С	0.27277	0.31178	0.33194	0.39068
18	053R	0	С	0.27692	0.32839	0.34910	0.40465
19	055L	0	С	0.24315	0.28050	0.29309	0.34150
20	055R	0	С	0.29077	0.33068	0.36151	0.39981
21	067R	0	С	0.21525	0.25007	0.28206	0.32826
22	073R	0	С	0.36427	0.37515	0.40025	0.42049
23	076L	0	С	0.38344	0.42291	0.43266	0.49557
24	078L	0	С	0.32986	0.35767	0.37284	0.42593
25	079R	0	С	0.24111	0.24699	0.28426	0.32082
26	084L	0	С	0.25772	0.27232	0.28543	0.32623
27	084R	0	С	0.26137	0.26705	0.29916	0.33748
28	088R	0	С	0.27062	0.29077	0.33127	0.37588
29	089R	0	1	0.26228	0.25633	0.29039	0.30631
30	093L	0	С	0.23179	0.27049	0.29159	0.35762
31	096L	0	С	0.24875	0.25851	0.26531	0.31056
32	113R	0	С	0.21210	0.21746	0.25317	0.29246
33	131R	0	С	0.27912	0.31101	0.34763	0.38968
34	135R	0	С	0.29791	0.32113	0.36585	0.40814
35	154R	0	С	0.22941	0.23575	0.28273	0.32940
36	160L	0	2	0.25822	0.24271	0.23740	0.27858
37	175L	0	С	0.23573	0.25869	0.25893	0.31035
38	183L	0	С	0.25869	0.29201	0.30842	0.36678
39	186R	0	С	0.22783	0.24702	0.27277	0.31376
40	188R	0	1	0.23008	0.22021	0.26171	0.27877
41	192L	0	С	0.26808	0.27940	0.27795	0.32643
42	200L	0	С	0.30115	0.30864	0.30792	0.33440
43	201R	0	С	0.31151	0.31468	0.33776	0.35819
44	203L	0	2	0.31901	0.32117	0.31883	0.34981
45	204L	0	2	0.23139	0.22368	0.21696	0.25165
46	205L	0	С	0.24882	0.25537	0.26865	0.31750
47	205R	0	1	0.23364	0.23107	0.27232	0.30355
48	211R	0	1	0.29403	0.28121	0.28970	0.30545
49	217L	0	2	0.26921	0.25145	0.23168	0.25709
50	220L	0	С	0.27760	0.28557	0.29377	0.34557
51	220R	0	С	0.26581	0.27917	0.31412	0.35987
52	505L	0	С	0.28309	0.30322	0.31083	0.35500

Table A.7: LOOCV results for combination of all the three 3D features.

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
53	505R	0	С	0.23589	0.26145	0.29977	0.34868
54	508R	0	1	0.24523	0.20777	0.24287	0.25790
55	511L	0	2	0.28804	0.26148	0.25882	0.28582
56	523L	0	1	0.24071	0.23330	0.23942	0.28164
57	528R	0	С	0.28759	0.28865	0.29768	0.31252
58	529L	0	С	0.25585	0.27702	0.29347	0.35897
59	529R	0	С	0.22342	0.24875	0.27908	0.32392
60	535L	0	С	0.26475	0.26553	0.26678	0.30904
61	535R	0	1	0.23835	0.21258	0.24360	0.26662
62	542L	0	С	0.26430	0.26886	0.26868	0.28867
63	542R	0	С	0.20423	0.20892	0.23625	0.28096
64	554L	0	2	0.25088	0.25059	0.24303	0.27556
65	554R	0	1	0.23169	0.21999	0.23372	0.25225
66	700R	0	1	0.22259	0.19476	0.22372	0.25008
67	702L	0	С	0.23900	0.24654	0.25578	0.29129
68	702R	0	1	0.22478	0.22327	0.25013	0.27247
69	704R	0	1	0.23239	0.21015	0.24656	0.27256
70	705L	0	1	0.24065	0.22497	0.23219	0.25951
71	710L	0	2	0.29729	0.26072	0.25388	0.27427
72	006L	1	0	0.25409	0.26462	0.27232	0.30709
73	012L	1	2	0.29048	0.28719	0.28432	0.31811
74	012R	1	С	0.27774	0.27282	0.30012	0.32290
75	018L	1	0	0.32300	0.34752	0.35004	0.39781
76	018R	1	0	0.34061	0.36418	0.38457	0.40376
77	022L	1	0	0.32759	0.34922	0.36015	0.40511
78	022R	1	0	0.30031	0.32904	0.36002	0.39734
79	023L	1	0	0.32472	0.34598	0.35123	0.39765
80	023R	1	0	0.33165	0.34451	0.37992	0.41216
81	027R	1	3	0.39141	0.35995	0.34765	0.32651
82	047L	1	2	0.32558	0.32574	0.31399	0.32591
83	047R	1	0	0.27982	0.28456	0.31899	0.35263
84	049R	1	0	0.25857	0.27148	0.31472	0.35373
85	056L	1	0	0.20373	0.21095	0.21481	0.25401
86	057R	1	С	0.22229	0.19429	0.21287	0.23306
87	060L	1	0	0.21872	0.22474	0.23096	0.27448
88	069R	1	С	0.26521	0.26209	0.29444	0.31887
89	070R	1	С	0.25147	0.21851	0.24067	0.26432
90	075R	1	С	0.24101	0.21902	0.23598	0.25971
91	082L	1	С	0.23163	0.22521	0.22996	0.27209
92	086L	1	2	0.24863	0.24811	0.23759	0.28744
93	094R	1	0	0.22842	0.23892	0.26760	0.29674
94	095R	1	0	0.35084	0.35176	0.35892	0.35234
95	098R	1	С	0.24235	0.22536	0.25247	0.26292
96	124R	1	0	0.27335	0.27663	0.31676	0.35335
97	133L	1	2	0.25122	0.24026	0.22495	0.24931
98	133R	1	С	0.29435	0.29287	0.29674	0.29519
99	163R	1	С	0.27617	0.27154	0.30125	0.32115
100	181L	1	0	0.23086	0.24301	0.25324	0.30193
101	184L	1	0	0.18899	0.20793	0.22095	0.27548
102	190L	1	2	0.22072	0.21411	0.20888	0.23458
103	197R	1	С	0.27601	0.23960	0.26117	0.28070
104	199L	1	2	0.22631	0.21838	0.21716	0.25673
105	200R	1	С	0.21833	0.19955	0.21063	0.22902
106	203R	1	С	0.37411	0.36898	0.37991	0.41458
107	204R	1	С	0.23681	0.21636	0.23033	0.24165

Table A.7: LOOCV results for combination of all the three 3D features (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
108	209R	1	2	0.31825	0.27760	0.26327	0.26861
109	210L	1	3	0.28889	0.24436	0.22196	0.21385
110	219L	1	2	0.24488	0.23481	0.23367	0.26155
111	507L	1	2	0.27378	0.24228	0.21276	0.23635
112	507R	1	С	0.28071	0.23221	0.23632	0.23750
113	509R	1	С	0.28960	0.25117	0.26653	0.27848
114	511R	1	С	0.23797	0.19542	0.21629	0.22486
115	512R	1	С	0.22788	0.20145	0.23044	0.26154
116	514L	1	2	0.24946	0.24378	0.24346	0.27534
117	515L	1	С	0.22408	0.20145	0.20583	0.23312
118	515R	1	С	0.24792	0.20680	0.22784	0.23193
119	516L	1	2	0.31776	0.28567	0.25104	0.26494
120	516R	1	С	0.29757	0.25483	0.26401	0.27833
121	517L	1	2	0.33009	0.31396	0.29846	0.30633
122	517R	1	С	0.29343	0.24478	0.24762	0.25979
123	521L	1	2	0.24950	0.23985	0.23808	0.27938
124	522R	1	С	0.21233	0.18678	0.20472	0.22713
125	523R	1	С	0.27747	0.22734	0.22801	0.22988
126	527L	1	2	0.31785	0.31894	0.31165	0.33820
127	527R	1	С	0.23186	0.20479	0.22921	0.25404
128	534L	1	2	0.36087	0.34963	0.33312	0.33313
129	539R	1	С	0.25887	0.22988	0.25713	0.28403
130	540L	1	3	0.28258	0.26692	0.25538	0.24799
131	541L	1	2	0.33275	0.32587	0.31181	0.32454
132	541R	1	С	0.28143	0.24061	0.24524	0.26495
133	543L	1	2	0.25500	0.22312	0.19923	0.21721
134	543R	1	С	0.27201	0.23600	0.23865	0.24579
135	574R	1	С	0.24579	0.24169	0.25646	0.25478
136	691L	1	С	0.25656	0.25481	0.25814	0.30789
137	691R	1	С	0.25983	0.24451	0.25143	0.26058
138	699R	1	С	0.19081	0.16319	0.18063	0.20198
139	700L	1	2	0.22110	0.20261	0.19877	0.22075
140	703R	1	С	0.26263	0.22951	0.24569	0.25276
141	704L	1	2	0.25457	0.24766	0.24576	0.28327
142	710R	1	С	0.26742	0.22490	0.24030	0.25938
143	711L	1	2	0.29006	0.26477	0.25432	0.26215
144	713L	1	С	0.24112	0.23485	0.23968	0.27891
145	713R	1	С	0.24499	0.22088	0.25297	0.26273
146	717R	1	С	0.22679	0.21961	0.24989	0.27054
147	002L	2	С	0.35946	0.34372	0.33042	0.33194
148	010L	2	3	0.43907	0.42703	0.41287	0.38712
149	026L	2	0	0.37095	0.37311	0.37129	0.37223
150	029L	2	0	0.41536	0.45183	0.46929	0.50003
151	065L	2	С	0.24170	0.22929	0.22438	0.25840
152	066L	2	0	0.31072	0.31880	0.31306	0.33372
153	189L	2	1	0.25174	0.24156	0.25047	0.25378
154	208L	2	3	0.37540	0.34883	0.33107	0.31051
155	214R	2	1	0.24793	0.21228	0.22839	0.24014
156	216L	2	1	0.25513	0.24212	0.24434	0.28985
157	219R	2	1	0.24023	0.20323	0.21681	0.21366
158	506L	2	С	0.27245	0.24657	0.23655	0.24980
159	509L	2	С	0.28464	0.26572	0.25857	0.28406
160	518L	2	С	0.28703	0.26216	0.24952	0.26356
161	518R	2	3	0.28088	0.24233	0.23589	0.21244
162	520L	2	С	0.25117	0.21923	0.19546	0.21076

Table A.7: LOOCV results for combination of all the three 3D features (continuted).

Subjects	Patient	Truth	Predicted	Distance G0	Distance G1	Distance G2	Distance G3
163	520R	2	1	0.32274	0.29584	0.29881	0.31425
164	522L	2	С	0.29322	0.26954	0.25724	0.25743
165	525L	2	3	0.30757	0.27084	0.25853	0.24067
166	526R	2	1	0.26404	0.21169	0.21610	0.21227
167	530R	2	3	0.28854	0.26022	0.26146	0.24778
168	532L	2	С	0.24165	0.21006	0.20784	0.23003
169	532R	2	3	0.32924	0.27257	0.26389	0.23803
170	533L	2	С	0.30778	0.27682	0.26392	0.27920
171	533R	2	1	0.31262	0.26428	0.27582	0.27278
172	536L	2	С	0.28870	0.27118	0.26774	0.30004
173	536R	2	1	0.30636	0.25765	0.26289	0.26547
174	537R	2	1	0.26137	0.21516	0.23320	0.24159
175	539L	2	1	0.24119	0.22740	0.22830	0.24863
176	546L	2	С	0.24039	0.22864	0.22575	0.26156
177	546R	2	1	0.23506	0.19993	0.21024	0.21759
178	689R	2	3	0.28806	0.25533	0.27245	0.25036
179	692L	2	3	0.39615	0.39113	0.38691	0.38106
180	694L	2	С	0.30412	0.27858	0.26911	0.28514
181	701R	2	3	0.34606	0.30803	0.31013	0.27007
182	177L	3	С	0.27452	0.24400	0.21333	0.21089
183	177R	3	С	0.38204	0.34372	0.33027	0.29184
184	206L	3	С	0.46099	0.43923	0.41367	0.40116
185	207R	3	2	0.31680	0.27660	0.27371	0.28146
186	212L	3	С	0.31133	0.26140	0.22445	0.21152
187	215L	3	С	0.30145	0.25167	0.21607	0.20506
188	215R	3	С	0.30766	0.24271	0.22808	0.19192
189	513L	3	С	0.30074	0.25907	0.23340	0.21966
190	513R	3	С	0.33915	0.28594	0.26696	0.24550
191	519L	3	2	0.27351	0.24259	0.21410	0.22439
192	519R	3	С	0.24436	0.20284	0.20335	0.20129
193	526L	3	С	0.29152	0.25010	0.22151	0.21618
194	52R	3	С	0.37003	0.35510	0.34259	0.33722
195	534R	3	С	0.31929	0.26804	0.25064	0.23986
196	538L	3	2	0.27987	0.24142	0.21288	0.23184
197	538R	3	2	0.23061	0.18198	0.17924	0.18471
198	547L	3	2	0.32868	0.28958	0.25425	0.26333
199	547R	3	С	0.34658	0.28969	0.27150	0.22917
200	549R	3	С	0.27612	0.23107	0.23087	0.20849
201	62R	3	С	0.44190	0.40975	0.38535	0.34611
202	697L	3	С	0.41605	0.36013	0.32421	0.27561
203	712L	3	С	0.27352	0.23117	0.20719	0.19826

Table A.7: LOOCV results for combination of all the three 3D features (continuted).

Appendix B

Subjective Rating

B.1 Subjective Rating for Grade 0

Patient No.	Surgeon 1	Surgeon 2	Patient No.	Surgeon 1	Surgeon 2
003L	0	0	175L	0	0
003R	0	0	183L	0	1
005R	0	1	186R	0	2
007L	0	0	188R	0	1
007R	0	0	192L	0	2
008R	0	1	200L	0	0
009L	0	0	201R	0	0
013R	0	0	203L	0	2
016R	0	0	204L	0	0
025L	0	0	205L	0	1
029R	0	0	205R	0	1
037L	0	0	211R	0	1
037R	0	0	217L	0	1
046L	0	1	220L	0	2
046R	0	1	220R	0	2
049L	0	1	505L	0	0
053L	0	0	505R	0	0
053R	0	0	508R	0	1
055L	0	0	511L	0	1
055R	0	0	523L	0	1
067R	0	0	528R	0	1
073R	0	0	529L	0	0
076L	0	0	529R	0	0
078L	0	0	535L	0	0
079R	0	2	535R	0	0
084L	0	0	542L	0	0
084R	0	0	542R	0	0
088R	0	1	554L	0	0
089R	0	1	554R	0	0
093L	0	1	700R	0	1
096L	0	2	702L	0	0
113R	0	0	702R	0	0
131R	0	0	704R	0	1
135R	0	0	705L	0	0
154R	0	1	710L	0	2
160L	0	2			

Table B.1: Subjective rating for grade 0

B.2 Subjective Rating for Grade 1

Patient No.	Surgeon 1	Surgeon 2	Patient No.	Surgeon 1	Surgeon 2
006L	1	1	219L	1	1
012L	1	1	507L	1	2
012R	1	1	507R	1	2
018L	1	0	509R	1	3
018R	1	1	511R	1	1
022L	1	1	512R	1	2
022R	1	1	514L	1	2
023L	1	2	515L	1	1
023R	1	2	515R	1	1
027R	1	2	516L	1	3
047L	1	2	516R	1	3
047R	1	2	517L	1	2
049R	1	1	517R	1	2
056L	1	2	521L	1	2
057R	1	2	522R	1	2
060L	1	1	523R	1	2
069R	1	2	527L	1	2
070R	1	2	527R	1	2
075R	1	2	534L	1	2
082L	1	2	539R	1	2
086L	1	2	540L	1	2
094R	1	2	541L	1	2
095R	1	0	541R	1	3
098R	1	3	543L	1	2
124R	1	2	543R	1	2
133L	1	2	574R	1	1
133R	1	2	691L	1	2
163R	1	2	691R	1	2
181L	1	2	699R	1	2
184L	1	2	700L	1	1
190L	1	2	703R	1	2
197R	1	2	704L	1	1
199L	1	1	710R	1	2
200R	1	0	711L	1	2
203R	1	2	713L	1	1
204R	1	0	713R	1	1
209R	1	2	717R	1	1
210L	1	2			

Table B.2: Subjective rating for grade 1.

B.3 Subjective Rating for Grade 2

Patient No.	Surgeon 1	Surgeon 2	Patient No.	Surgeon 1	Surgeon 2
002L	2	1	525L	2	3
010L	2	1	526R	2	2
026L	2	2	530R	2	3
029L	2	1	532L	2	2
065L	2	3	532R	2	3
066L	2	3	533L	2	3
189L	2	3	533R	2	3
208L	2	3	536L	2	2
214R	2	2	536R	2	3
216L	2	2	537R	2	2
219R	2	2	539L	2	2
506L	2	2	546L	2	2
509L	2	3	546R	2	2
518L	2	2	689R	2	3
518R	2	2	692L	2	2
520L	2	3	694L	2	1
520R	2	3	701R	2	3
522L	2	2			

Table B.3: Subjective rating for grade 2.

B.4 Subjective Rating for Grade 3

Patient No.	Surgeon 1	Surgeon 2	Patient No.	Surgeon 1	Surgeon 2
177R	3	3	52R	3	3
206L	3	3	534R	3	3
207R	3	3	538L	3	3
212L	3	3	538R	3	3
215L	3	3	547L	3	3
215R	3	3	547R	3	3
513L	3	3	549R	3	3
513R	3	3	62R	3	3
519L	3	3	697L	3	3
519R	3	3	712L	3	3

Table B.4: Subjective rating for grade 3.

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Table C.1: Distance measurements on Grade 0.

2 n-i p3	1 4.179 0	2.191 0	3.338 0	91 0	0 6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-	0	0	0	1	1	-
2 n-i	1 4.179	2.191	3.338	91	6																					
~	-		0.1	2.9	3.15	5.085	7.304	8.04	3.492	2.371	4.392	0.002	1.921	1.733	3.62	1.608	2.003	-1.182	-1.487	-0.888	-1.328	-1.267	-1.536	-0.848	-0.933	-0.994
ď-		-	-	-	-	-	-	-	-	1	-	-	1	1	-	-	-	-	0	0	-	0	0	-	-	-
M-2 0.0521	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	1.4878	2.0496	1.6563	1.4973	1.6014	1.7685	1.4211	1.4994	1.4708
r2 1 0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	0.8641	0.7212	0.8212	0.8617	0.8352	0.7927	0.8810	0.8611	0.8684
v-i/v-u 7 6207	2.6292	1.4944	2.4551	2.2228	1.6015	2.1900	3.3761	5.1572	2.5779	1.4797	2.2771	1.0005	1.4223	1.3131	1.9536	1.3817	1.5867	0.8641	0.7212	0.8212	0.8617	0.8352	0.7927	0.8810	0.8611	0.8684
i-v 75.65	25.65	44.32	22.94	24.46	52.52	42.73	30.74	19.34	22.13	49.43	34.39	37.62	45.49	55.35	37.96	42.13	34.14	86.95	53.34	49.67	95.99	76.87	74.09	71.27	67.17	75.52
л-и У-и	67.44	66.23	56.32	54.37	84.11	93.58	103.78	99.74	57.05	73.14	78.31	37.64	64.7	72.68	74.16	58.21	54.17	75.13	38.47	40.79	82.71	64.2	58.73	62.79	57.84	65.58
p1	-	1	1	-	1	-	-	-	1	1	-	-	1	1	-	-	-	0	0	0	0	0	0	0	0	0
M-1	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.5871	1.7907	1.5632	1.5599	1.8361	1.9390	1.5119	1.6123	1.5619
round	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	0.9410	0.9186	0.9437	0.9440	0.9136	0.9023	0.9493	0.9382	0.9438
s-i/s-n	1.2258	1.1139	1.1821	1.1886	1.1713	1.2919	1.6016	1.6400	1.1972	1.1419	1.2011	1.0001	1.1274	1.1258	1.2626	1.0984	1.1136	0.9410	0.9186	0.9437	0.9440	0.9136	0.9023	0.9493	0.9382	0.9438
S-n 195.04	185.04	192.33	183.29	158.57	184.45	174.2	121.4	125.62	177.09	167.1	218.38	190.25	150.78	137.73	137.86	163.4	176.31	200.39	182.71	157.59	237.19	146.66	157.19	167.23	151.08	176.85
s-i 276 82	226.83	214.24	216.67	188.48	216.04	225.05	194.44	206.02	212.01	190.81	262.3	190.27	169.99	155.06	174.06	179.48	196.34	188.57	167.84	148.71	223.91	133.99	141.83	158.75	141.75	166.91
50 9L	c0.0/-	-82.13	-15.28	15.89	-69.3	-68.52	-57.85	-58.03	29.57	152.88	-99.67	-31.39	-4.43	0.64	111.45	101.86	42.58	-2.46	-138.29	-115.49	2.34	83.12	78.06	-38.7	-15.46	42.36
S 176.42	176.43	176.43	224.33	228.83	199.26	199.26	167.33	167.33	263.71	393.12	197.02	196.5	211.05	211.05	323.47	323.47	273.06	273.06	82.89	82.89	322.24	293.98	293.98	191.32	193.46	284.79
I 50.4	-50.4	-37.81	7.66	40.35	-16.78	-25.79	-27.11	-38.69	51.7	202.31	-65.28	6.23	41.06	55.99	149.41	143.99	76.72	84.49	-84.95	-65.82	98.33	159.99	152.15	32.57	51.71	117.88
N N	-8.61	-15.9	41.04	70.26	14.81	25.06	45.93	41.71	86.62	226.02	-21.36	6.25	60.27	73.32	185.61	160.07	96.75	72.67	-99.82	-74.7	85.05	147.32	136.79	24.09	42.38	107.94
Patient	205L	205R	211R	217L	220L	220R	505L	505R	508R	511L	523L	528R	529L	529R	535L	535R	542L	542R	554L	554R	700R	702L	702R	704R	705L	710L

p3	-	0	0	0	0	0	0	0	0	0	0	0	0	С	0	0	1	0	0	0	0	ŝ	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
n-i	-0.912	2.239	2.258	2.079	1.652	-1.011	4.526	-1.111	4.526	-1.552	-1.351	-1.096	1.436	4	-2.597	-1.469	-0.965	-1.914	-1.745	-1.448	-1.498	-3.573	-1.001	-1.043	4.955	-1.186	-1.226	1.668	3.233	-1.134	-1.003	2.489	-1.251	-1.195	-1.813	1.709	-1.263	-1.073
p2	0	-	-	-	-	0	-	0	-	0	0	0	-	0	0	0	0	0	0	0	0	0	0	0	-	0	0	0	-	0	0	-	0	0	0	-	0	0
M-2	1.5546	0.9531	0.9531	0.9531	0.9531	1.5528	0.9531	1.6121	0.9531	2.3013	1.8013	1.5122	0.9531	2.4861	2.4161	1.8499	1.5343	2.1366	2.0488	1.8704	1.8438	2.3347	1.7317	1.5544	0.9531	1.8359	1.8131	1.9323	0.9531	1.5214	1.6710	0.9531	1.7996	1.7518	1.8790	0.9531	1.6959	1.7994
r2	0.8471	1.0000	1.0000	1.0000	1.0000	0.8475	1.0000	0.8325	1.0000	0.6572	0.7844	0.8578	1.0000	0.6103	0.6280	0.7720	0.8522	0.6991	0.7214	0.7668	0.7735	0.6487	0.8021	0.8471	1.0000	0.7755	0.7813	0.7510	1.0000	0.8555	0.8175	1.0000	0.7848	0.7969	0.7646	1.0000	0.8112	0.7848
n-v/i-v	0.8471	1.9302	1.7649	1.4565	1.3365	0.8475	4.4869	0.8325	4.4869	0.6572	0.7844	0.8578	1.3765	0.6103	0.6280	0.7720	0.8522	0.6991	0.7214	0.7668	0.7735	0.6487	0.8021	0.8471	2.6544	0.7755	0.7813	0.7510	1.8776	0.8555	0.8175	1.8347	0.7848	0.7969	0.7646	1.3514	0.8112	0.7848
i-v	59.64	24.07	29.52	45.54	49.1	66.31	12.98	66.31	12.98	45.28	62.65	77.1	38.14	102.63	69.82	64.43	65.31	63.61	62.64	62.09	66.15	101.72	50.57	68.23	29.95	52.84	56.07	-67	36.84	78.49	54.95	29.82	58.13	58.85	77.02	48.64	66.88	49.87
n-v	50.52	46.46	52.1	66.33	65.62	56.2	58.24	55.2	58.24	29.76	49.14	66.14	52.5	62.63	43.85	49.74	55.66	44.47	45.19	47.61	51.17	65.99	40.56	57.8	79.5	40.98	43.81	-50.32	69.17	67.15	44.92	54.71	45.62	46.9	58.89	65.73	54.25	39.14
p1	0	-	1	-	-	0	1	0	-	0	0	0	-	ŝ	0	0	0	0	0	0	0	ŝ	0	0	-	0	0	1	-	0	0	-	0	0	0	-	0	0
M-1	1.5044	1.0512	1.0512	1.0512	1.0512	1.5577	1.0512	1.6048	1.0512	1.6509	1.5773	1.5190	1.0512	2.5207	2.0068	1.6307	1.5193	1.8201	1.6858	1.7045	1.5801	2.5654	1.5231	1.5482	1.0512	1.5165	1.5509	1.0512	1.0512	1.5002	1.5202	1.0512	1.6324	1.7138	1.8399	1.0512	1.6252	1.5178
round	0.9501	1.0000	1.0000	1.0000	1.0000	0.9443	1.0000	0.9391	1.0000	0.9340	0.9421	0.9485	1.0000	0.8383	0.8948	0.9362	0.9485	0.9154	0.9301	0.9281	0.9418	0.8333	0.9481	0.9453	1.0000	0.9488	0.9450	1.0000	1.0000	0.9506	0.9484	1.0000	0.9360	0.9271	0.9132	1.0000	0.9368	0.9487
s-i/s-n	0.9501	1.2981	1.3274	1.1153	1.0918	0.9443	1.2739	0.9391	1.2739	0.9340	0.9421	0.9485	1.0944	0.8383	0.8948	0.9362	0.9485	0.9154	0.9301	0.9281	0.9418	0.8333	0.9481	0.9453	1.3218	0.9488	0.9450	1.0915	1.1786	0.9506	0.9484	1.1281	0.9360	0.9271	0.9132	1.0855	0.9368	0.9487
n-s	182.83	75.11	68.97	180.38	180	181.35	165.22	182.35	165.22	235.14	233.32	212.88	152.13	247.32	246.91	230.31	187.32	226.18	249.82	201.39	257.34	214.39	192.73	190.69	153.97	231.57	222.91	182.25	181.04	229.49	194.3	194.3	195.56	163.86	208.86	199.98	199.92	208.96
s-i	173.71	97.5	91.55	201.17	196.52	171.24	210.48	171.24	210.48	219.62	219.81	201.92	166.49	207.32	220.94	215.62	177.67	207.04	232.37	186.91	242.36	178.66	182.72	180.26	203.52	219.71	210.65	198.93	213.37	218.15	184.27	219.19	183.05	151.91	190.73	217.07	187.29	198.23
٨	-67.87	-110.12	-109.62	-34.06	-32.97	13.54	27.63	13.54	27.63	4.42	-68.41	-64.97	9.56	-10.41	-45.32	-48.48	-1.75	-56.2	-53.05	-72.21	-61.76	-38.54	41.77	-31.03	23.38	-28.03	-22.2	60.11	-15.2	17.93	-29.24	-52.2	-69.17	73.13	-144.81	10.29	-90.12	39.39
s	165.48	11.45	11.45	212.65	212.65	251.09	251.09	251.09	251.09	269.32	214.05	214.05	214.19	299.54	245.44	231.57	241.23	214.45	241.96	176.79	246.75	241.84	275.06	217.46	256.85	244.52	244.52	192.04	235.01	314.57	209.98	196.81	172.01	283.89	122.94	276	164.05	287.49
I	-8.23	-86.05	-80.1	11.48	16.13	79.85	40.61	79.85	40.61	49.7	-5.76	12.13	47.7	92.22	24.5	15.95	63.56	7.41	9.59	-10.12	4.39	63.18	92.34	37.2	53.33	24.81	33.87	-6.89	21.64	96.42	25.71	-22.38	-11.04	131.98	-67.79	58.93	-23.24	89.26
z	-17.35	-63.66	-57.52	32.27	32.65	69.74	85.87	68.74	85.87	34.18	-19.27	1.17	62.06	52.22	-1.47	1.26	53.91	-11.73	-7.86	-24.6	-10.59	27.45	82.33	26.77	102.88	12.95	21.61	9.79	53.97	85.08	15.68	2.51	-23.55	120.03	-85.92	76.02	-35.87	78.53
Patient	006L	012L	012R	018L	018R	022L	022R	023L	023R	027R	047L	047R	049R	056L	057R	060L	069R	070R	075R	082L	086L	094R	095R	098R	124R	133L	133R	163R	181L	184L	190L	197R	199L	200R	203R	204R	209R	210L

Table C.2: Distance measurements on Grade 1.

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																																						
Nite N I x site wint Nit i wite Nit i wite Nit	D3	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	n-i	-1.359	-2.282	1.972	-1.7	1.824	1.22	3.874	1.483	-1.218	2.311	-1.292	5.319	4.785	2.051	-1.121	-1.383	7.936	-2.688	2.425	-0.463	-1.431	2.29	2.265	-1.317	-1.302	6.244	4.912	4.847	1.982	3.429	3.942	4.446	2.619	4.42	3.438	2.912	4.059
	p2	10	0	0	0	-	-	-	-	0	-	0	-	-	-	0	0	-	0	-	0	0	-	-	0	0	0	-	-	1	-	-	-	-	-	-	-	-
Pattert N s vs si-bs round M-1 pt ivv n-v/v r2 2719 7574 7573 21373 21393 21393 21393 21394 2175 21735 21735 21745 2177 2175 2175 2177 2175 2175 2177 2177 2175 2175 2175 2175 21775 2177 2100 2	M-2	1.8271	2.0163	1.5431	2.1884	0.9531	0.9531	0.9531	0.9531	1.8199	0.9531	1.9039	0.9531	0.9531	0.9531	1.9013	1.8373	0.9531	2.3103	0.9531	2.2257	2.1041	0.9531	0.9531	1.7998	1.7255	1.9215	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531	0.9531
Patient N si si <th< td=""><td>12</td><td>0.7778</td><td>0.7297</td><td>0.8500</td><td>0.6859</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>0.7796</td><td>1.0000</td><td>0.7583</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>0.7589</td><td>0.7752</td><td>1.0000</td><td>0.6549</td><td>1.0000</td><td>0.6765</td><td>0.7074</td><td>1.0000</td><td>1.0000</td><td>0.7847</td><td>0.8036</td><td>0.7538</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td><td>1.0000</td></th<>	12	0.7778	0.7297	0.8500	0.6859	1.0000	1.0000	1.0000	1.0000	0.7796	1.0000	0.7583	1.0000	1.0000	1.0000	0.7589	0.7752	1.0000	0.6549	1.0000	0.6765	0.7074	1.0000	1.0000	0.7847	0.8036	0.7538	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
	n-v/j-v	0.7778	0.7297	0.8500	0.6859	1.3763	1.3298	2.3494	1.0835	0.7796	1.5238	0.7583	2.1762	1.9397	1.6421	0.7589	0.7752	2.4878	0.6549	1.7785	0.6765	0.7074	1.7044	1.7375	0.7847	0.8036	0.7538	2.6308	3.1774	1.4614	2.3866	3.4244	3.8318	1.9947	3.5520	2.2457	1.6738	2.8994
	i-v	61.16	84.42	-131.46	54.13	48.47	36.99	28.71	177.68	55.27	44.12	53.45	45.22	50.92	31.94	46.5	61.52	53.34	<i>0.17</i>	31.15	14.31	48.9	32.51	30.71	61.18	66.3	-253.6	30.12	22.26	42.96	24.73	16.26	15.7	26.33	17.32	27.6	43.22	21.37
	n-v	47.57	61.6	-111.74	37.13	66.71	49.19	67.45	192.51	43.09	67.23	40.53	98.41	98.77	52.45	35.29	47.69	132.7	51.02	55.4	9.68	34.59	55.41	53.36	48.01	53.28	-191.16	79.24	70.73	62.78	59.02	55.68	60.16	52.52	61.52	61.98	72.34	61.96
Patient N I s v si s-n s-i/s-n round $M-1$ 219L -7.94 -65.81 143.52 -126.97 20933 20330 16651 507L -7.06 15.76 203.71 668.81 73.52 210.77 0.8917 20349 16651 507R -20.05 15.76 203.71 6.68.81 19.35 20.9453 16971 20343 507R -193.43 17.53 -23.056 293.96 19.669 1.0501 10512 511R 230.36 -114.88 25.63 -145.51 201.74 393.12 14.91 19.000 10512 511R -76.06 -114.88 25.63 -145.51 201.74 31.64 1.0000 10512 511R -21.93 201.06 53.54 19.401 109.65 1.0000 10512 511R -21.93 107.61 166.75 106.75 1.0000 10512 511R	1d	10	0	-	0	-	-	-	-	0	-	0	-	-	-	0	0	-	0	-	1	0	-	-	0	0	-		-	1	-	-	-	-	-	-	-	-
Patient N I s v si-b s-b-n round 219L -79.4 -65.81 143.52 -12.697 209.33 222.92 0.9390 0.9390 507L -70.6 15.76 203.71 9.666 187.95 210.77 0.8917 0.8917 507R -20.05 -39.71 203.71 9.169 210.77 0.8917 0.8917 507R -20.05 -39.71 203.71 91.66 239.46 10.855 10.000 501R 200.73 210.143 91.75 230.36 239.46 10.851 10.000 514L -76.06 -114.8 92.65 -143.51 207.10 0.9453 10.000 514L -76.06 -114.8 92.65 -143.51 207.10 0.9453 10.000 516L -21.93 45.04 201.65 53.96 181.83 94.01 0.953 0.9453 516L -21.93 175.9 97.05 1086.76<	M-1	1.6051	2.0349	1.0512	1.5479	1.0512	1.0512	1.0512	1.0512	1.6216	1.0512	1.5510	1.0512	1.0512	1.0512	1.5967	1.5156	1.0512	2.1820	1.0512	1.2717	1.6602	1.0512	1.0512	1.6679	1.7649	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512	1.0512
PatientNIsvs-is-i/s-n $219L$ -7.06 15.76 203.71 68.06 187.95 207.71 0.8817 $507L$ -7.06 15.76 203.71 68.06 187.95 209.33 222.92 0.9390 $507R$ -2003 -39.77 209.37 10.66 187.95 209.453 10.881 $507R$ -2005 -39.77 209.31 210.66 187.95 210.77 0.8817 $509R$ -190.45 393.12 15.4 110.65 110.05 120.97 $514R$ -76.06 -114.8 92.63 -143.51 207.32 10.90 $515R$ -70.06 -114.8 92.63 -143.51 207.32 10.005 $516R$ -33.06 -20.14 201.83 89.16 246.87 223.76 110.037 $517L$ -7.11 -60.29 183.9 -100.551 244.92 21.2797 248.99 $517L$ -7.11 -60.29 183.9 -100.551 244.87 223.76 110.0372 $517L$ -7.11 -60.29 183.9 -100.551 237.82 294.00 12571 $571R$ -291.93 -201.42 210.83 -73.59 273.49 100.70 107.86 $517R$ -291.93 -201.42 210.83 -73.59 210.97 270.66 094.05 $571R$ -291.92 201.42 210.86 127.72 257.77 256.77 <	round	0.9390	0.8917	1.0000	0.9453	1.0000	1.0000	1.0000	1.0000	0.9372	1.0000	0.9450	1.0000	1.0000	1.0000	0.9400	0.9489	1.0000	0.8755	1.0000	0.9757	0.9330	1.0000	1.0000	0.9321	0.9215	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Patient N I s v s-i s-n 219L -79.4 -65.81 143.52 -126.97 209.33 222.92 507R -20.05 -39.77 203.71 -68.66 187.95 210.77 507R -20.05 -39.77 203.71 -68.66 187.95 210.77 507R -20.05 -39.77 203.71 -68.66 187.95 210.77 511R 220.71 203.71 -68.66 187.95 210.74 515L 70.06 -114.8 92.63 -143.51 210.96 72.48 515R 97.05 109.23 291.06 72.35 188.07 109.65 516R -33.06 -20.14 201.83 39.91.0 72.43 186.07 516R -33.05 -20.14 201.83 39.51.6 233.44 191 517R -7.11 -60.29 183.9 -100.96 51.94 106 516R -73.58	s-i/s-n	0.9390	0.8917	1.0881	0.9453	1.1058	1.0659	1.2297	1.0868	0.9372	1.1033	0.9450	1.2785	1.2571	1.1234	0.9400	0.9489	1.6502	0.8755	1.1156	0.9757	0.9330	1.1341	1.1079	0.9321	0.9215	1.1609	1.3358	1.2939	1.1094	1.1881	1.1805	1.2703	1.1492	1.2370	1.1823	1.1548	1.2357
PatientNIsvsi219L -79.4 -65.81 143.52 -126.97 209.33 507L -7.06 15.76 203.71 -68.66 187.95 507R -20.05 -39.77 203.71 -68.66 187.95 507R -20.05 -39.77 203.71 -68.66 187.95 507R -20.05 -39.77 203.71 -68.66 187.95 511R 220.711 202.47 393.12 154 190.65 512L -76.06 -114.8 92.63 -143.51 207.43 515L -710.66 -114.8 92.63 -143.51 207.43 516L -710.66 -114.8 92.63 -143.51 207.43 515L -710.66 -114.8 92.63 -143.51 207.43 516L -71.166 -102.08 93.99 -100.96 233.94 517R -2.119 -50.04 183.9 -105.51 244.19 517R -2.119 -50.04 183.9 -105.56 244.19 517R -2.119 -50.04 183.9 -105.56 246.76 527R 25.92 37.13 212.62 293.74 256.77 5211L -77.138 -39.05 -112.42 214.43 296.67 5234L -119.78 -241.46 183.9 -105.56 246.79 527R 25.92 310.51 43.52 256.77 291.42 527R 256.92 <td>S-n</td> <td>222.92</td> <td>210.77</td> <td>223.76</td> <td>310.96</td> <td>172.41</td> <td>185.06</td> <td>168.69</td> <td>170.9</td> <td>194.01</td> <td>223.76</td> <td>234.89</td> <td>191</td> <td>186.09</td> <td>166.25</td> <td>186.7</td> <td>270.6</td> <td>122.06</td> <td>215.97</td> <td>209.85</td> <td>190.8</td> <td>213.5</td> <td>170.74</td> <td>209.97</td> <td>194.03</td> <td>165.76</td> <td>388.06</td> <td>146.27</td> <td>164.92</td> <td>181.2</td> <td>182.26</td> <td>218.45</td> <td>164.51</td> <td>175.58</td> <td>186.47</td> <td>188.58</td> <td>188.11</td> <td>172.2</td>	S-n	222.92	210.77	223.76	310.96	172.41	185.06	168.69	170.9	194.01	223.76	234.89	191	186.09	166.25	186.7	270.6	122.06	215.97	209.85	190.8	213.5	170.74	209.97	194.03	165.76	388.06	146.27	164.92	181.2	182.26	218.45	164.51	175.58	186.47	188.58	188.11	172.2
Patient N I s v 219L -794 -65.81 143.52 -126.97 507L -7.06 15.76 203.71 68.66 507R -20.05 -39.77 203.71 91.69 508R -193.43 -176.43 117.53 -230.56 511R 220.71 202.47 393.12 154 515L 120.16 105.33 291.06 53.96 515L 120.16 105.33 291.06 53.66 516L -7.19 -60.29 183.9 -105.51 517R -2.19 -50.04 183.9 -100.96 527R 98.45 -73.55 193.96 -101.55 527R 25.92 37.13 212.62 -93.75 <td< th=""><th>S-1:</th><th>209.33</th><th>187.95</th><th>243.48</th><th>293.96</th><th>190.65</th><th>197.26</th><th>207.43</th><th>185.73</th><th>181.83</th><th>246.87</th><th>221.97</th><th>244.19</th><th>233.94</th><th>186.76</th><th>175.49</th><th>256.77</th><th>201.42</th><th>189.09</th><th>234.1</th><th>186.17</th><th>199.19</th><th>193.64</th><th>232.62</th><th>180.86</th><th>152.74</th><th>450.5</th><th>195.39</th><th>213.39</th><th>201.02</th><th>216.55</th><th>257.87</th><th>208.97</th><th>201.77</th><th>230.67</th><th>222.96</th><th>217.23</th><th>212.79</th></td<>	S-1:	209.33	187.95	243.48	293.96	190.65	197.26	207.43	185.73	181.83	246.87	221.97	244.19	233.94	186.76	175.49	256.77	201.42	189.09	234.1	186.17	199.19	193.64	232.62	180.86	152.74	450.5	195.39	213.39	201.02	216.55	257.87	208.97	201.77	230.67	222.96	217.23	212.79
PatientNIs219L -79.4 -65.81 143.52 507L -7.06 15.76 203.71 507R -20.05 -39.77 203.71 507R -20.05 -39.77 203.71 507R -20.05 -39.77 203.71 507R -20.05 -39.77 203.71 508R -193.43 -176.43 117.53 514L -76.06 -114.8 92.63 515L 270.16 102.23 291.06 515R -33.06 -114.8 92.63 516L -21.93 -45.04 183.9 517L -7.1 -60.29 183.9 517R -2.19 -50.04 183.9 517R -2.19 -50.04 183.9 527R -73.13 -201.42 201.83 527R -73.13 -201.42 201.83 527R -73.13 -21.03 210.61 527R -73.13 -21.46 183.9 527R -73.13 212.62 527R -50.04 183.9 527R -73.58 -99.75 528 -59.75 204.94 541L -19.56 -42.46 151.18 541R -58.79 $-81.44.03$ 210.51 541R -58.79 $-81.44.03$ 200.75 541R -58.79 $-81.44.63$ 27.67 571R -57.67 -72.11 130.64 573R -73.67 -72.46 151.18 57	Λ	-126.97	-68.66	91.69	-230.56	154	-139.07	-143.51	-72.35	53.96	-89.16	-73.59	-105.51	-100.96	-130.86	-9.37	-121.27	55.75	43.52	-175.18	40.75	-43.15	-74.97	-112.15	-111.4	-88.4	118.47	36.44	26.3	-18.31	80.96	23.72	-33.35	56.69	-3.1	26.9	17.01	23.87
Patient N I 219L -79.4 -65.81 507R -70.6 15.76 507R -20.05 -39.77 507R -20.05 -39.77 507R -20.05 -39.77 507R -103.43 -176.43 514L -76.06 -114.8 515R -70.05 -30.77 516L -21.93 -47.64 515L -21.93 -40.20 516L -71.1 -60.29 517R -2.19 -50.04 517R -2.19 -50.14 517R -2.19 -50.04 5218 -73.58 -50.14 5218 -73.58 -50.14 5217 -73.58 -50.04 5218 -73.58 -50.02 5214 -73.58 -50.14 5215 -73.58 -50.14 5214 -73.58 -50.14 5214 -73.58 -50.14 5	s	143.52	203.71	203.71	117.53	393.12	95.18	92.63	291.06	291.06	201.83	201.83	183.9	183.9	87.84	212.62	197.02	310.51	310.51	90.07	241.23	204.94	151.18	151.18	130.64	130.64	315.37	261.95	261.95	225.67	322.24	297.85	191.32	284.79	244.89	277.46	277.46	258.03
Patient N 219L -79.4 507L -70.6 507R -20.05 509R -193.43 511R 220.71 512R -20.05 514L -76.06 515L 120.16 515L -193.43 515L -79.05 515L -70.05 515L -70.05 515L -70.05 515L -70.05 517L -71.1 517R -2.193 517R -2.193 5217L -7.11 517R -2.193 5217R -2.193 5217R -2.193 5217R -2.193 5217R -7.11 5217R -7.119.78 5221L -7.119.78 5234L -119.78 5234L -119.78 5241L -19.56 691R 115.68 691R 115.68	I	-65.81	15.76	-39.77	-176.43	202.47	-102.08	-114.8	105.33	109.23	-45.04	-20.14	-60.29	-50.04	-98.92	37.13	-59.75	109.09	121.42	-144.03	55.06	5.75	-42.46	-81.44	-50.22	-22.1	-135.13	66.56	48.56	24.65	105.69	39.98	-17.65	83.02	14.22	54.5	60.23	45.24
Patient 219L 507L 507R 507R 507R 511R 513L 513L 513L 513L 513L 513L 513L 513L	Z	-79.4	-7.06	-20.05	-193.43	220.71	-89.88	-76.06	120.16	97.05	-21.93	-33.06	-7.1	-2.19	-78.41	25.92	-73.58	188.45	94.54	-119.78	50.43	-8.56	-19.56	-58.79	-63.39	-35.12	-72.69	115.68	97.03	44.47	139.98	79.4	26.81	109.21	58.42	88.88	89.35	85.83
	Patient	219L	507L	507R	509R	511R	512R	514L	515L	515R	516L	516R	517L	517R	521L	522R	523R	527L	527R	534L	539R	540L	541L	541R	543L	543R	574R	691L	691R	699R	700L	703R	704L	710R	711L	713L	713R	717R

Table C.3: Distance measurements on Grade 1 (continued).

p3	10	0	б	1	0	0	0	0	6	0	0	0	0	0	0	e	б	0	0	e	6	0	б	0	0	0	0	0	0	0	0	0	1	0	0
n-i	-2.57	-1.368	-3.433	-0.981	-2.644	-2.327	-1.415	1.471	-1.181	1.786	-1.615	-1.881	-1.391	3.253	4.094	-3.245	-3.596	-1.584	-2.365	-3.721	-1.775	-1.212	-3.095	-1.488	2.144	2.701	3.276	1.647	-1.459	-1.181	-1.787	2.554	-0.989	2.579	5.634
p2	ε	0	e	0	0	0	0	1	0	-	0	0	0	-	-	ŝ	e	0	0	ŝ	0	0	Э	0	-	-	-	1	0	0	0	1	0	-	-
M-2	2.8571	2.2671	2.5886	1.8379	2.4356	2.4695	1.7272	0.9531	1.6929	0.9531	1.9897	2.1495	1.7123	0.9531	0.9531	2.7938	2.6562	2.2356	1.9977	2.5678	1.8668	1.8878	3.1884	1.6959	0.9531	0.9531	0.9531	0.9531	1.8558	1.7407	2.3332	0.9531	1.6445	0.9531	0.9531
r2	0.5159	0.6659	0.5842	0.7751	0.6231	0.6145	0.8032	1.0000	0.8119	1.0000	0.7365	0.6958	0.8070	1.0000	1.0000	0.5320	0.5670	0.6739	0.7344	0.5895	0.7677	0.7624	0.4317	0.8111	1.0000	1.0000	1.0000	1.0000	0.7705	0.7998	0.6491	1.0000	0.8242	1.0000	1.0000
n-v/i-v	0.5159	0.6659	0.5842	0.7751	0.6231	0.6145	0.8032	1.3368	0.8119	1.5497	0.7365	0.6958	0.8070	2.6160	3.2744	0.5320	0.5670	0.6739	0.7344	0.5895	0.7677	0.7624	0.4317	0.8111	1.5134	1.8902	2.6290	1.4714	0.7705	0.7998	0.6491	1.8614	0.8242	2.0675	3.1479
i-v	53.09	40.95	82.56	43.61	70.15	60.36	71.9	43.68	62.79	32.49	61.28	61.84	72.07	20.13	18	69.34	83.05	48.58	89.05	90.64	76.41	51	54.46	78.79	41.76	30.34	20.11	34.94	63.57	58.98	50.93	29.65	56.26	24.16	26.23
v-n	27.39	27.27	48.23	33.8	43.71	37.09	57.75	58.39	50.98	50.35	45.13	43.03	58.16	52.66	58.94	36.89	47.09	32.74	65.4	53.43	58.66	38.88	23.51	63.91	63.2	57.35	52.87	51.41	48.98	47.17	33.06	55.19	46.37	49.95	82.57
pl	2	0	0	0	0	0	0	1	0	-	0	0	0	-	-	0	0	0	0	0	0	0	0	0	-	-	-	1	0	0	0	1	0	-	1
M-1	1.9646	1.5157	2.2239	1.5302	1.9663	1.9400	1.6931	1.0512	1.5296	1.0512	1.6620	1.8054	1.5398	1.0512	1.0512	2.1882	2.3607	1.7628	1.7772	2.3285	1.7061	1.5131	2.1268	1.6798	1.0512	1.0512	1.0512	1.0512	1.7248	1.6128	1.7896	1.0512	1.5330	1.0512	1.0512
round	0.8995	0.9489	0.8709	0.9473	0.8993	0.9022	0.9294	1.0000	0.9473	1.0000	0.9328	0.9170	0.9462	1.0000	1.0000	0.8749	0.8559	0.9217	0.9201	0.8594	0.9279	0.9492	0.8816	0.9308	1.0000	1.0000	1.0000	1.0000	0.9259	0.9382	0.9187	1.0000	0.9470	1.0000	1.0000
s-i/s-n	0.8995	0.9489	0.8709	0.9473	0.8993	0.9022	0.9294	1.0719	0.9473	1.1011	0.9328	0.9170	0.9462	1.2015	1.2412	0.8749	0.8559	0.9217	0.9201	0.8594	0.9279	0.9492	0.8816	0.9308	1.0902	1.1433	1.1587	1.1051	0.9259	0.9382	0.9187	1.1212	0.9470	1.1696	1.2926
u-s	255.65	267.61	265.99	186.07	262.52	237.87	200.3	204.67	224.28	176.66	240.23	226.6	258.69	161.41	169.76	259.31	249.51	202.24	295.96	264.68	246.27	238.39	261.44	215.08	237.77	188.45	206.47	156.77	196.81	191.08	219.9	210.65	186.51	152.02	192.58
s-i	229.95	253.93	231.66	176.26	236.08	214.6	186.15	219.38	212.47	194.52	224.08	207.79	244.78	193.94	210.7	226.86	213.55	186.4	272.31	227.47	228.52	226.27	230.49	200.2	259.21	215.46	239.23	173.24	182.22	179.27	202.03	236.19	176.62	177.81	248.92
>	-113	-131.05	-77.66	-37.15	-85.93	11.2	-5.38	-99.01	-90.87	-69.62	-141.84	-152.31	-199.32	-109.23	-123.86	-196.24	-196.64	-22.36	-110.12	-188.5	-192.05	-7.1	-14.78	-139.74	-161.72	-139.35	-152.89	56.29	-4.56	10.24	-4.47	-44.87	33.45	7.45	36.05
s	170.04	163.83	236.56	182.72	220.3	286.16	252.67	164.05	184.39	157.39	143.52	117.32	117.53	104.84	104.84	96.66	96.66	212.62	251.24	129.61	112.88	270.17	270.17	139.25	139.25	106.45	106.45	264.47	241.23	248.49	248.49	220.97	266.33	209.42	311.2
Ι	-59.91	-90.1	4.9	6.46	-15.78	71.56	66.52	-55.33	-28.08	-37.13	-80.56	-90.47	-127.25	-89.1	-105.86	-126.9	-113.59	26.22	-21.07	-97.86	-115.64	43.9	39.68	-60.95	-119.96	-109.01	-132.78	91.23	59.01	69.22	46.46	-15.22	89.71	31.61	62.28
z	-85.61	-103.78	-29.43	-3.35	-42.22	48.29	52.37	-40.62	-39.89	-19.27	-96.71	-109.28	-141.16	-56.57	-64.92	-159.35	-149.55	10.38	-44.72	-135.07	-133.39	31.78	8.73	-75.83	-98.52	-82	-100.02	107.7	44.42	57.41	28.59	10.32	79.82	57.4	118.62
Patient	002L	010L	026L	029L	065L	066L	189L	208L	214R	216L	219R	506L	509L	518L	518R	520L	520R	522L	525L	526R	530R	532L	532R	533L	533R	536L	536R	537R	539L	546L	546R	689R	692L	694L	701R

Table C.4: Distance measurements on Grade 2.

p3	0	0	e	б	б	1	1	б	0	ы	0	0	б	ы	n	0	1	1	б	n	1	6
n-i	-1.827	-1.073	-3.29	-6.651	-3.149	-0.314	-0.032	-3.083	-1.997	-1.545	-1.274	6.94	-11.227	-2.814	-3.133	1.739	-0.12	-0.672	-5.587	-4.661	-0.775	-1.046
p2	10	-	0	б	0	-	-	0	0	0	0	-	б	0	0	-	-	0	ŝ	e	-	0
M-2	2.1436	1.4940	2.3504	5.1746	2.3547	1.3745	0.9887	2.1343	2.2495	2.1663	2.1428	0.9531	4.7997	2.4953	2.4629	0.9531	1.0714	1.5596	3.6541	3.4690	1.4642	2.1242
r2	0.6973	0.8625	0.6447	-0.0733	0.6437	0.8929	0.9909	0.6997	0.6704	0.6916	0.6975	1.0000	0.0220	0.6079	0.6161	1.0000	0.9699	0.8458	0.3133	0.3604	0.8701	0.7022
n-v/i-v	0.6973	0.8625	0.6447	-0.0733	0.6437	0.8929	0.9909	0.6997	0.6704	0.6916	0.6975	1.4931	0.0220	0.6079	0.6161	2.0917	0.9699	0.8458	0.3133	0.3604	0.8701	0.7022
i-v	60.36	78.02	92.61	61.97	88.37	29.31	35.32	102.66	60.59	50.09	42.12	140.74	114.8	71.77	81.62	15.93	39.9	43.58	81.36	72.87	59.64	35.13
n-v	42.09	67.29	59.71	-4.54	56.88	26.17	35	71.83	40.62	34.64	29.38	210.14	2.53	43.63	50.29	33.32	38.7	36.86	25.49	26.26	51.89	24.67
p1	10	-	0	e	0	-	-	0	0	0	0	-	б	0	0	-	-	-	ŝ	ŝ	-	1
M-1	1.7640	1.4906	2.2146	3.4445	2.3746	1.1831	1.0655	2.0608	1.8264	1.7198	1.5883	1.0512	3.6349	2.0626	2.1800	1.0512	1.1014	1.3412	3.0457	2.5361	1.2962	1.4135
round	0.9215	0.9516	0.8719	0.7366	0.8543	0.9855	0.9984	0.8889	0.9147	0.9264	0.9409	1.0000	0.7156	0.8887	0.8758	1.0000	0.9945	0.9681	0.7805	0.8366	0.9730	0.9601
s-i/s-n	0.9215	0.9516	0.8719	0.7366	0.8543	0.9855	0.9984	0.8889	0.9147	0.9264	0.9409	1.4660	0.7156	0.8887	0.8758	1.0687	0.9945	0.9681	0.7805	0.8366	0.9730	0.9601
u-s	232.87	221.88	256.93	252.5	216.19	216.27	203.98	277.44	234.07	209.94	215.51	148.94	394.8	252.8	252.18	253.27	217.16	210.53	254.51	285.19	287.45	262.3
s-i	214.6	211.15	224.03	185.99	184.7	213.13	203.66	246.61	214.1	194.49	202.77	218.34	282.53	224.66	220.85	270.66	215.96	203.81	198.64	238.58	279.7	251.84
>	11.2	-3.01	-71.81	-48.4	-153.87	-105.1	-101.64	-220.95	-146.37	-210.87	-211.18	-229.47	-99.76	-206.36	20.38	36.26	-149.91	-141.44	-79.07	-98.94	-128.49	-78
s	286.16	286.16	244.83	199.56	119.2	137.34	137.34	128.32	128.32	33.71	33.71	129.61	297.57	90.07	322.85	322.85	105.95	105.95	200.93	212.51	210.85	208.97
I	71.56	75.01	20.8	13.57	-65.5	-75.79	-66.32	-118.29	-85.78	-160.78	-169.06	-88.73	15.04	-134.59	102	52.19	-110.01	-97.86	2.29	-26.07	-68.85	-42.87
z	53.29	64.28	-12.1	-52.94	-96.99	-78.93	-66.64	-149.12	-105.75	-176.23	-181.8	-19.33	-97.23	-162.73	70.67	69.58	-111.21	-104.58	-53.58	-72.68	-76.6	-53.33
Patient	177L	177R	206L	207L	212L	215L	215R	513L	513R	519L	519R	526L	52R	534R	538L	538R	547L	547R	549R	62R	697L	712L

Grade 3.
on
Distance measurements
2:
Ü
Table

M2	1.0000	1.0000	1.0000	1.0000	1.0000	0.7184	1.0000	1.0000	0.6213	1.0000	1.0000	1.0000	0.6010	0.4637	1.0000	1.0000	1.0000	1.0000	1.0000	0.9135	0.7835	0.8248	0.9005	0.8787	0.8563	0.8446	0.7491	0.7348	0.8272	0.8288	0.7278
n-v/i-v	4.3277	4.6672	18.5948	45.7771	1.5272	0.7184	1.6197	1.5585	0.6213	1.7526	1.1805	1.0103	0.6010	0.4637	0.9618	1.4203	1.5338	2.2327	3.1841	0.9135	0.7835	0.8248	0.9005	0.8787	0.8563	0.8446	0.7491	0.7348	0.8272	0.8288	0.7278
i-v	28.41	25.15	4.22	1.75	49.11	60.08	40.94	45.91	40.51	37.19	31.19	39	24.51	36.08	-23.04	-1.38	106.51	40.74	26.24	-20.24	44.33	32.3	13.02	38.98	-20.18	-26.67	11.88	17.78	37.5	25.55	9.04
n-v	122.95	117.38	78.47	80.11	75	43.16	66.31	71.55	25.17	65.18	36.82	39.4	14.73	16.73	-22.16	0.58	163.36	90.96	83.55	-35.26	-13.59	-7.87	-11.63	10.37	-50.28	-60.2	-17.12	-13.73	-2.02	-11.63	-32.94
M1	1.0000	1.0000	1.0000	1.0000	1.0000	0.8880	1.0000	1.0000	0.9266	1.0000	1.0000	1.0000	0.9499	0.9078	1.0000	1.0000	1.0000	1.0000	1.0000	0.9413	0.7597	0.8464	0.8966	0.8787	0.8899	0.8760	0.8998	0.8908	0.8382	0.8506	0.8413
s-i/s-n	1.1646	1.8828	1.8962	1.9649	1.1382	0.8880	1.1429	1.1608	0.9266	1.1603	1.0334	1.0025	0.9499	0.9078	1.0034	1.0101	1.5812	1.4544	1.3495	0.9413	0.7597	0.8464	0.8966	0.8787	0.8899	0.8760	0.8998	0.8908	0.8382	0.8506	0.8413
n-s	164	104.48	82.85	81.21	187.36	151.09	177.58	159.42	208.92	174.63	168.55	163.2	195.22	209.86	257.31	193.72	97.81	110.53	163.99	256	241.02	261.44	238.36	235.77	273.3	270.37	289.4	288.65	244.25	248.91	264.46
S-i	191	196.71	157.1	159.57	213.25	134.17	202.95	185.06	193.58	202.62	174.18	163.6	185.44	190.51	258.19	195.68	154.66	160.75	221.3	240.98	183.1	221.27	213.71	207.16	243.2	236.84	260.4	257.14	204.73	211.73	222.48
٧	120.36	120.36	-20.11	-20.11	8.14	-2.16	5.05	17.97	-14.09	-39.52	13.74	16.51	8.13	-8.51	-45.94	24.14	-61.83	-59.24	-53.68	-6.2	23.17	-2.97	34.66	-3.08	29.65	42.5	-96.31	-98.95	-8.8	-8.4	-54.84
s	342.22	342.22	141.21	141.21	270.5	192.09	248.94	248.94	220	200.29	219.11	219.11	218.08	218.08	189.21	218.44	199.34	142.25	193.86	214.54	250.6	250.6	261.39	243.06	252.67	252.67	175.97	175.97	233.43	228.88	176.68
.1	148.77	145.51	-15.89	-18.36	57.25	57.92	45.99	63.88	26.42	-2.33	44.93	55.51	32.64	27.57	-68.98	22.76	44.68	-18.5	-27.44	-26.44	67.5	29.33	47.68	35.9	9.47	15.83	-84.43	-81.17	28.7	17.15	-45.8
n	243.31	237.74	58.36	60	83.14	41	71.36	89.52	11.08	25.66	50.56	55.91	22.86	8.22	-68.1	24.72	101.53	31.72	29.87	-41.46	9.58	-10.84	23.03	7.29	-20.63	-17.7	-113.43	-112.68	-10.82	-20.03	-87.78
Patient	kit-r	kit-l	model-03 r	model-03 l	p134-r	p140-1	p148-r	p148-1	p161-r	p156-l	p173-r	p173-l	p126-r	p126-1	p145-1	p146-1	model-01-l	model-02-l	model-04-r	p117-r	p119-1	p119-r	p120-r	p125-r	p127-1	p127-r	p128-1	p128-r	p104-r	p105-r	p110-1
Grade	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

Table C.6: Distance measurements.

M2	0.7316	0.6635	0.8180	0.7284	0.6849	0.6683	0.6904	0.8918	1.0000	1.0000	1.0000	1.0000	0.8534	0.8793	0.9456	0.9254	0.4071
n-v/i-v	0.7316	0.6635	0.8180	0.7284	0.6849	0.6683	0.6904	0.8918	1.8614	1.2350	1.0460	3.1479	0.8534	0.8793	0.9456	0.9254	0.4071
i-v	45.47	88.53	16.55	63.72	-183.47	58.52	90.8	66.47	29.65	13.87	50.4	26.23	82.71	47.11	27.21	43.19	95.28
n-v	-4.7	13.53	-25.24	-0.85	0.71	-12.4	17.96	51.75	55.19	17.13	52.72	82.57	44.7	24.75	18.08	29.06	38.78
M1	0.8060	0.7033	0.8153	0.7527	0.7464	0.7605	0.7595	0.9505	1.0000	1.0000	1.0000	1.0000	0.8169	0.9054	0.9502	0.9353	0.6385
s-i/s-n	0.8060	0.7033	0.8153	0.7527	0.7464	0.7605	0.7595	0.9505	1.1212	1.0136	1.0170	1.2926	0.8169	0.9054	0.9502	0.9353	0.6385
u-s	258.61	252.81	226.26	261.09	282.98	296.09	302.91	297.24	210.65	239.6	136.6	192.58	207.54	236.42	183.41	218.48	356.25
s-i	208.44	177.81	184.47	196.52	211.21	225.17	230.07	282.52	236.19	242.86	138.92	248.92	169.53	214.06	174.28	204.35	227.45
v	-58.53	-65.66	13.09	-25.94	-44.74	-55.54	-14.47	-130.44	-44.87	65.7	7.45	36.05	-23.36	-61.83	-59.24	-53.68	-78.04
s	195.38	200.68	214.11	234.3	238.95	238.95	265.33	218.55	220.97	322.43	196.77	311.2	228.88	199.34	142.25	193.86	244.69
.1	-13.06	22.87	29.64	37.78	27.74	13.78	35.26	-63.97	-15.22	79.57	57.85	62.28	59.35	-14.72	-32.03	-10.49	17.24
u	-63.23	-52.13	-12.15	-26.79	-44.03	-57.14	-37.58	-78.69	10.32	82.83	60.17	118.62	21.34	-37.08	-41.16	-24.62	-111.56
Patient	107-1	155-r	157-I	158-1	176-1	176-r	179-r	525-1	689-r	692-1	694-1	701-r	105-1	model01-r	model02-r	model04-1	108-1
Grade	2	7	7	7	7	0	7	7	7	0	0	7	7	7	0	7	e

Table C.7: Distance measurements (continued).

Appendix D

Patient Information

Patient	Age	Race	Ethnicity	BMI
	Age	NdUU		
2	n.a.	White	Not_Hispanic_Latino	28
3	55	White	n.a.	22.5
5	53	White	n.a.	32.5
6	39	White	n.a.	n.a.
7	54	White	n.a.	21.5
8	56	White	n.a.	27.5
9	38	White	n.a.	24.3
10	53	White	n.a.	37.1
12	56	White	Hispanic_Latino	27.3
13	40	White	n.a.	20.4
16	47	White	n.a.	20.7
18	64	White	Hispanic_Latino	25.1
22	51	Black_AfricanAmerican	n.a.	29.5
23	40	Asian	n.a.	26.1
25	41	White	n.a.	22.2
26	53	White	n.a.	30.5
27	47	White	n.a.	33.6
29	42	White	n.a.	22.7
37	56	White	NotHispanic_Latino	27.3
46	36	White	NotHispanic_Latino	24.7
47	53	White	NotHispanic_Latino	35.3
49	42	White	Hispanic_Latino	27.5
52	n.a.	n.a.	n.a.	21.5
53	53	White	NotHispanic_Latino	23.1
55	53	White	NotHispanic_Latino	22
56	54	White	NotHispanic_Latino	25.9
57	63	White	NotHispanic_Latino	24.8
60	54	White	NotHispanic_Latino	32.1
62	n.a.	n.a.	n.a.	n.a.
65	53	White	Not_Hispanic_Latino	31
66	66	White	Not_Hispanic_Latino	27.6
67	50	White	Hispanic_Latino	23.4
69	50	White	NotHispanic_Latino	25.5
70	52	White	NotHispanic_Latino	39.6
73	41	White	NotHispanic_Latino	20.5
75	68	White	NotHispanic_Latino	33.5
76	43	White	Hispanic_Latino	20.6
78	40	White	NotHispanic_Latino	21.9
79	73	White	NotHispanic_Latino	28.9
82	59	White	NotHispanic_Latino	31.6
84	27	White	NotHispanic_Latino	23.4
86	53	White	NotHispanic_Latino	32.9
88	38	White	NotHispanic_Latino	33.1
89	66	White	NotHispanic_Latino	21.9
93	51	White	NotHispanic_Latino	22.2
94	48	White	NotHispanic_Latino	27.5
95	46	White	NotHispanic Latino	25.2
96	37	Black_AfricanAmerican	NotHispanic_Latino	31.4
98	55	White	NotHispanic_Latino	30.6

Table D.1: Patient information.

Patient	Age	Race	Ethnicity	BMI
113	54	White	NotHispanic_Latino	35.2
124	54	n.a.	n.a.	36.4
131	51	n.a.	NotHispanic_Latino	20.4
133	46	White	NotHispanic_Latino	34.4
135	51	White	NotHispanic_Latino	20.6
154	55	White	NotHispanic_Latino	30
160	n.a.	n.a.	n.a.	27.3
163	37	White	NotHispanic_Latino	26.2
175	37	White	NotHispanic_Latino	24.9
177	n.a.	n.a.	n.a.	n.a.
181	47	White	Hispanic Latino	28.5
183	42	White	Hispanic Latino	23.2
184	59	White	NotHispanic Latino	28.7
186	48	Black African American	n a	35.3
188	56	White	NotHispanic Latino	34.5
100	50	White	Hispanic Latino	27.9
109	n.a.	White White		27.0
190	53	white	NotHispanic_Latino	27.6
192	46	White	NotHispanic_Latino	32.4
197	52	White	Hispanic_Latino	33.6
199	41	n.a.	n.a.	24.8
200	51	White	NotHispanic_Latino	21.7
201	38	n.a.	NotHispanic_Latino	19
203	55	White	NotHispanic_Latino	30.8
204	50	White	NotHispanic_Latino	25.9
205	57	White	NotHispanic_Latino	29
206	58	White	NotHispanic_Latino	n.a.
207	42	White	NotHispanic_Latino	n.a.
208	n.a.	n.a.	n.a.	n.a.
209	34	White	NotHispanic_Latino	n.a.
210	52	n.a.	n.a.	n.a.
211	53	Black_AfricanAmerican	NotHispanic Latino	25.7
212	52	Black African American	n a	38.4
212	40	White	Not Hispanic Latino	33.1
217	40	n a	Hispanic Latino	55.1 n o
215	49	n.a.		11.a.
210	11.a. 40	II.a. White	II.d. NotHismonia Latina	11.a.
217	49	winte	Not Lioparie Let	2ð.2
219	50	wnite	NotHispanic_Latino	n.a.
220	52	White	NotH1spanic_Latino	22.5
505	n.a.	n.a.	n.a.	24.2
506	n.a.	n.a.	n.a.	26
507	n.a.	n.a.	n.a.	n.a.
508	n.a.	n.a.	n.a.	n.a.
509	n.a.	n.a.	n.a.	n.a.
511	n.a.	n.a.	n.a.	n.a.
512	n.a.	n.a.	n.a.	n.a.
513	n.a.	n.a.	n.a.	n.a.
514	n.a.	n.a.	n.a.	n.a.
515	n.a.	n.a.	n.a.	n.a.
516	n.a.	n.a.	n.a.	n.a.
517	n.a.	n.a.	n.a.	n.a.
518	n a	n a	n a	31.2
510	n.a.	n.a.	n.a.	n 9
520	n.a.	11.a.	n.a.	11.a. 20-1
520	n.a.	n.a.	n.a.	58.1
521	n.a.	n.a.	n.a.	n.a.
/ / 3/ -			10.0	n 0

Table D.1: Patient information (continuted).

Patient	Age	Race	Ethnicity	BMI
523	n.a.	n.a.	n.a.	n.a.
525	n.a.	n.a.	n.a.	n.a.
526	n.a.	n.a.	n.a.	32.4
527	n.a.	n.a.	n.a.	n.a.
528	n.a.	n.a.	n.a.	22.4
529	n.a.	n.a.	n.a.	22.3
530	n.a.	n.a.	n.a.	30.6
532	n.a.	n.a.	n.a.	30.9
533	n.a.	n.a.	n.a.	31.8
534	n.a.	n.a.	n.a.	n.a.
535	n.a.	n.a.	n.a.	n.a.
536	n.a.	n.a.	n.a.	25.9
537	n.a.	n.a.	n.a.	34.6
538	n.a.	n.a.	n.a.	n.a.
539	n.a.	n.a.	n.a.	n.a.
540	n.a.	n.a.	n.a.	n.a.
541	n.a.	n.a.	n.a.	n.a.
542	n.a.	n.a.	n.a.	n.a.
543	n.a.	n.a.	n.a.	n.a.
546	n.a.	n.a.	n.a.	26.9
547	n.a.	n.a.	n.a.	n.a.
549	n.a.	n.a.	n.a.	40.3
554	n.a.	n.a.	n.a.	n.a.
574	n.a.	n.a.	n.a.	n.a.
689	n.a.	n.a.	n.a.	n.a.
691	n.a.	n.a.	n.a.	n.a.
692	n.a.	n.a.	n.a.	20.3
694	n.a.	n.a.	n.a.	28.2
697	n.a.	n.a.	n.a.	n.a.
699	n.a.	n.a.	n.a.	n.a.
700	n.a.	n.a.	n.a.	20.9
701	n.a.	n.a.	n.a.	n.a.
702	n.a.	n.a.	n.a.	n.a.
703	n.a.	n.a.	n.a.	n.a.
704	n.a.	n.a.	n.a.	n.a.
705	n.a.	n.a.	n.a.	n.a.
710	n.a.	n.a.	n.a.	n.a.
711	n.a.	n.a.	n.a.	n.a.
712	n.a.	n.a.	n.a.	n.a.
713	n.a.	n.a.	n.a.	n.a.
717	n.a.	n.a.	n.a.	n.a.

Table D.1: Patient information (continuted).